

SNS COLLEGE OF TECHNOLOGY

Coimbatore-35
An Autonomous Institution



Accredited by NBA – AICTE and Accredited by NAAC – UGC with 'A+' Grade Approved by AICTE, New Delhi & Affiliated to Anna University, Chennai

DEPARTMENT OF AUTOMOBILE ENGINEERING

19AUB303 – Finite Element Methods and Analysis

IV YEAR / VII SEM

UNIT – 3 FORMULATION OF ELEMENT CHARACTERISTIC

MATRICES AND VECTORS FOR THERMAL PROBLEMS

Topic – 1 – Problems on 1D Plate Elements



1D Bar Element - Problem



A thin steel plate of uniform this canes 25 mm is subjected to a point hood of 420 N at mid depth as shown below. The plate is also subjected to self-weight. If young's modulus, E=2010 N/mm = 4 unit Weight density, P=0.8×10-4 N/mm3. Calculate the following (i) displacement at each nodal point (ii) Stress in each element.

100 mm)
2
2
2
200 mm)
420N
200 mm)

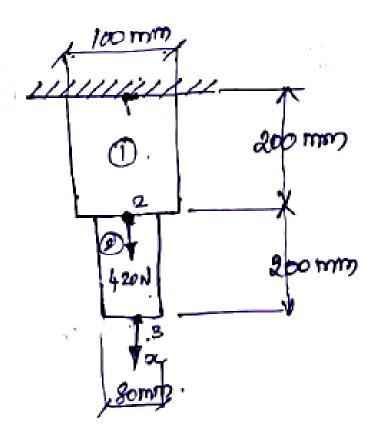
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Thickness,
Unit Weight Donaity,
                                    = 2500 mm
                                   = 2000 mm2
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To_	Find:-		-		١.					_	
	(j)	Displaceme	ent	at	each	noceal	points	ч,	, U2	Ę	Чз
	(ii)	Stress	'n	each	ele	nent.,	J, X	T ₂			





The steel plate is subjected to selfweight, we have Body Force Vector

element
$$\bigcirc$$
, $\begin{cases} f_1 \\ f_2 \end{cases} = 0.8 \times 10^{-1} \times 2500 \times 200 \begin{cases} 1 \\ 1 \end{cases}$

$$\begin{cases} F_1 \\ F_2 \\ \end{cases} = \begin{cases} 20 \\ 20 \\ \end{cases}$$





For element (2)

$$\begin{cases} F_2 \\ F_3 \end{cases} = \begin{cases} 16 \\ 16 \\ 1 \end{cases}$$

Assembling the body force rector,

$$\begin{cases} f_1 \\ f_2 \\ f_3 \end{cases} = \begin{cases} \frac{2.0}{36} \\ \frac{36}{16} \\ \frac{16}{36} \end{cases}$$





A point load is acting at
$$\frac{1}{2}$$
 = $\frac{1}{5}$ = $\frac{20}{36+420}$ mid olyth, nodal print $\frac{1}{2}$ = $\frac{1}{5}$ = $\frac{20}{16}$ =

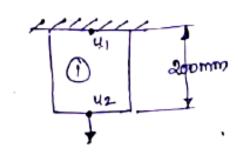




Finite element egn. for one dimensional plate element,

$$[k] = \frac{Ab}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$

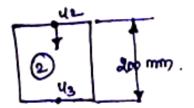
For element (1, Noder (1,2)!-







$$\begin{bmatrix} k_1 \end{bmatrix} = \frac{A_2 E}{b} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix}$$



$$= \frac{1 \times 10^{5}}{1 \times 10^{5}} \begin{bmatrix} \frac{a_{22}}{a_{0}} & \frac{a_{23}}{a_{0}} \\ \frac{a_{32}}{a_{0}} & \frac{a_{33}}{a_{0}} \end{bmatrix} \begin{cases} u_{1} - 2 & = \\ u_{3} & = \\ u_{3} & = \\ u_{3} & = \end{cases} \begin{cases} F_{2} & 2 & \dots > \\ F_{3} & \vdots \end{cases}$$









Applying boundary condition; at node , the displacement 4, = 0 4 Substituting the values of F1, F2 9 F3.

$$\frac{3}{2} \frac{1}{10} = \frac{25}{45} - \frac{25}{45} = \frac{20}{456} = \frac{20}{456} = \frac{20}{456} = \frac{20}{456} = \frac{20}{16} = \frac{20}$$

In the above egn, the first aw & first column is neglected because the nodal point (1) is fixed.



Jub., the value of up = 1.888 x 10 4 in @







(ii) Stocks in Each element

$$\sigma_1 = E\left(\frac{u_2 - u_1}{\ell_1}\right)$$









(i) Displacements at each modal

43=1.988 × 10-4 mm.

01 = 0.1888 N/mm2, 02 = 0.008 N/mm2

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