



SNS COLLEGE OF TECHNOLOGY

An Autonomous Institution
Coimbatore-35



Accredited by NBA – AICTE and Accredited by NAAC – UGC with 'A+' Grade
Approved by AICTE, New Delhi & Affiliated to Anna University, Chennai

DEPARTMENT OF ELECTRONICS & COMMUNICATION ENGINEERING

19ECB212 – DIGITAL SIGNAL PROCESSING

II YEAR/ IV SEMESTER

UNIT 3 – FIR FILTER DESIGN

TOPIC – FIR Filter Design using Windowing Techniques



WINDOWING TECHNIQUES OF FIR FILTERS



- The windows are finite duration sequences used to modify the impulse response of the FIR filters in order to reduce the ripples in the pass band and stop band and also to achieve the desired transition from pass band and stop band
- The FIR filter design starts with desired frequency response $H_d(e^{j\omega})$. The desired impulse response $h_d(n)$ is obtained by taking inverse Fourier transform of $H_d(e^{j\omega})$. The desired impulse response will be an infinite duration sequence
- On multiplying finite duration window sequence with infinite duration impulse response with modified sample, which is used to design FIR filter
- **Types of Windowing Techniques: Rectangular Window, Hanning Window, Hamming Window and Blackman Window**



HANNING AND HAMMING WINDOW



Features of Hamming Window spectrum:

1. The main-lobe width is equal to $8\pi / N$
2. The maximum side-lobe magnitude is -41dB
3. The side-lobe magnitude remains constant with increasing ω

$$w_H(n) = 0.54 + 0.46 \cos \frac{2\pi n}{N-1} \quad ; \quad \text{for } n = -\frac{N-1}{2} \text{ to } +\frac{N-1}{2}$$
$$= 0 \quad ; \quad \text{other } n$$

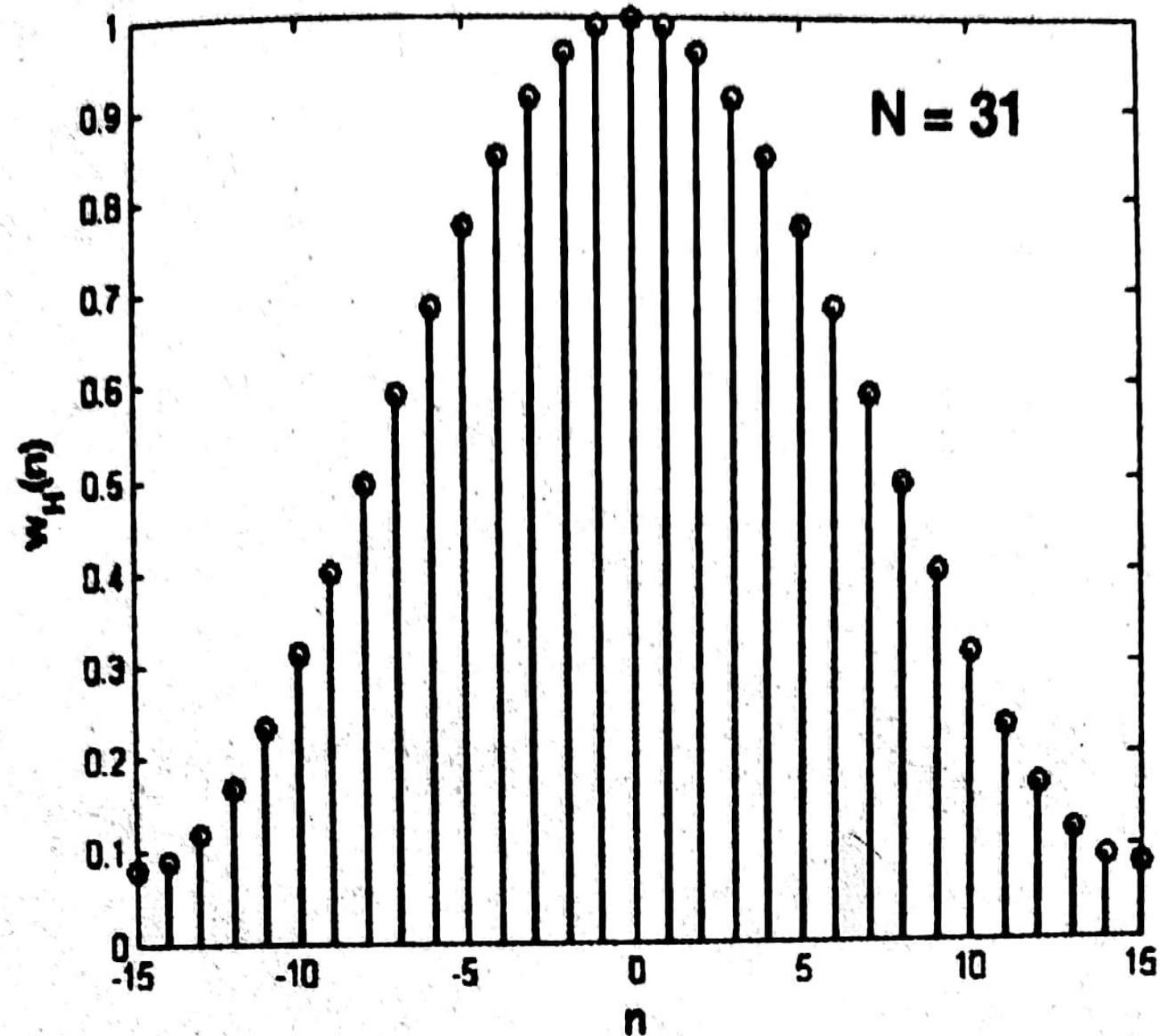
$$w_H(n) = 0.54 - 0.46 \cos \frac{2\pi n}{N-1} \quad ; \quad \text{for } n = 0 \text{ to } N-1$$
$$= 0 \quad ; \quad \text{other } n$$



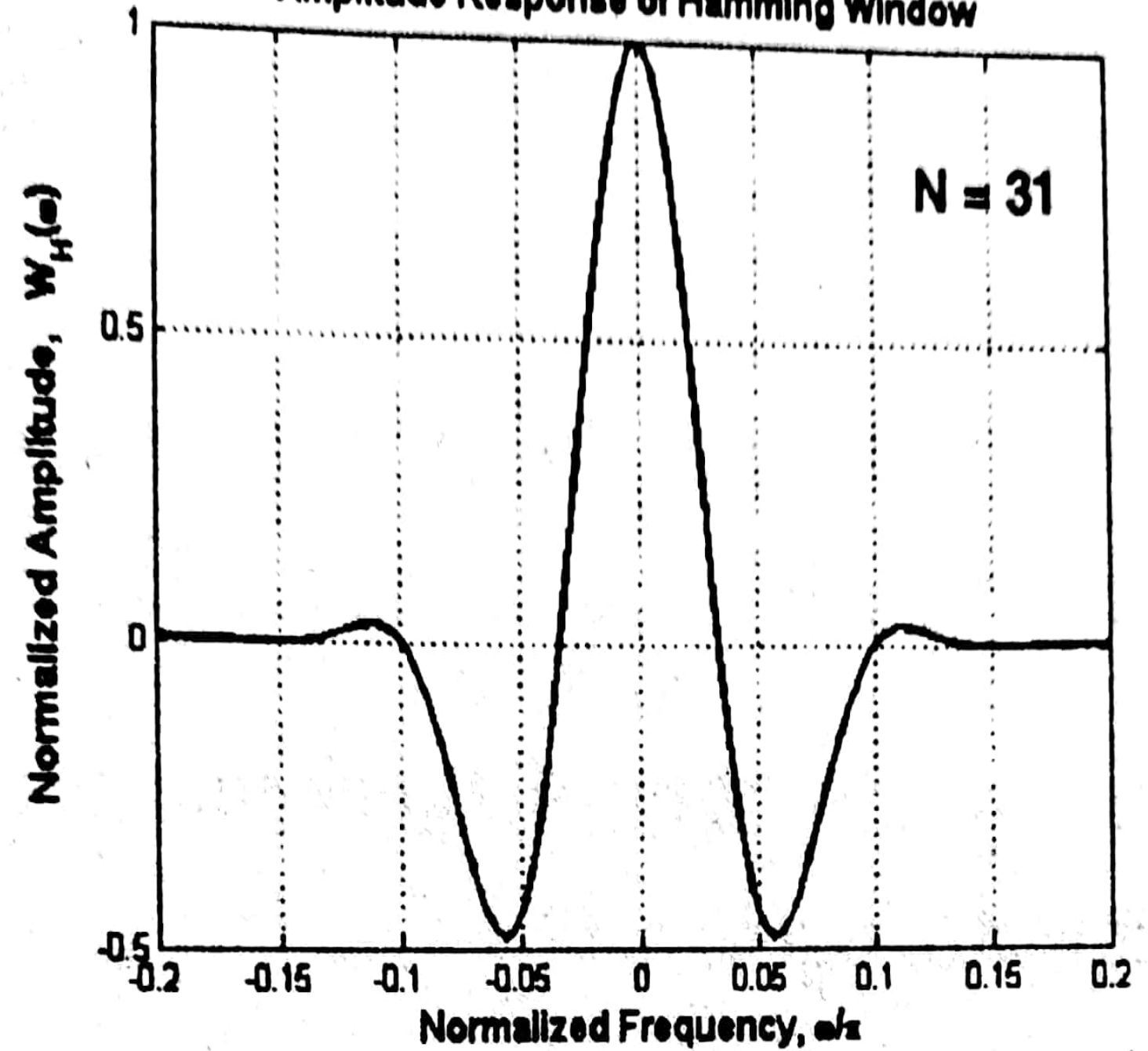
HAMMING WINDOW



Hamming Window Sequence

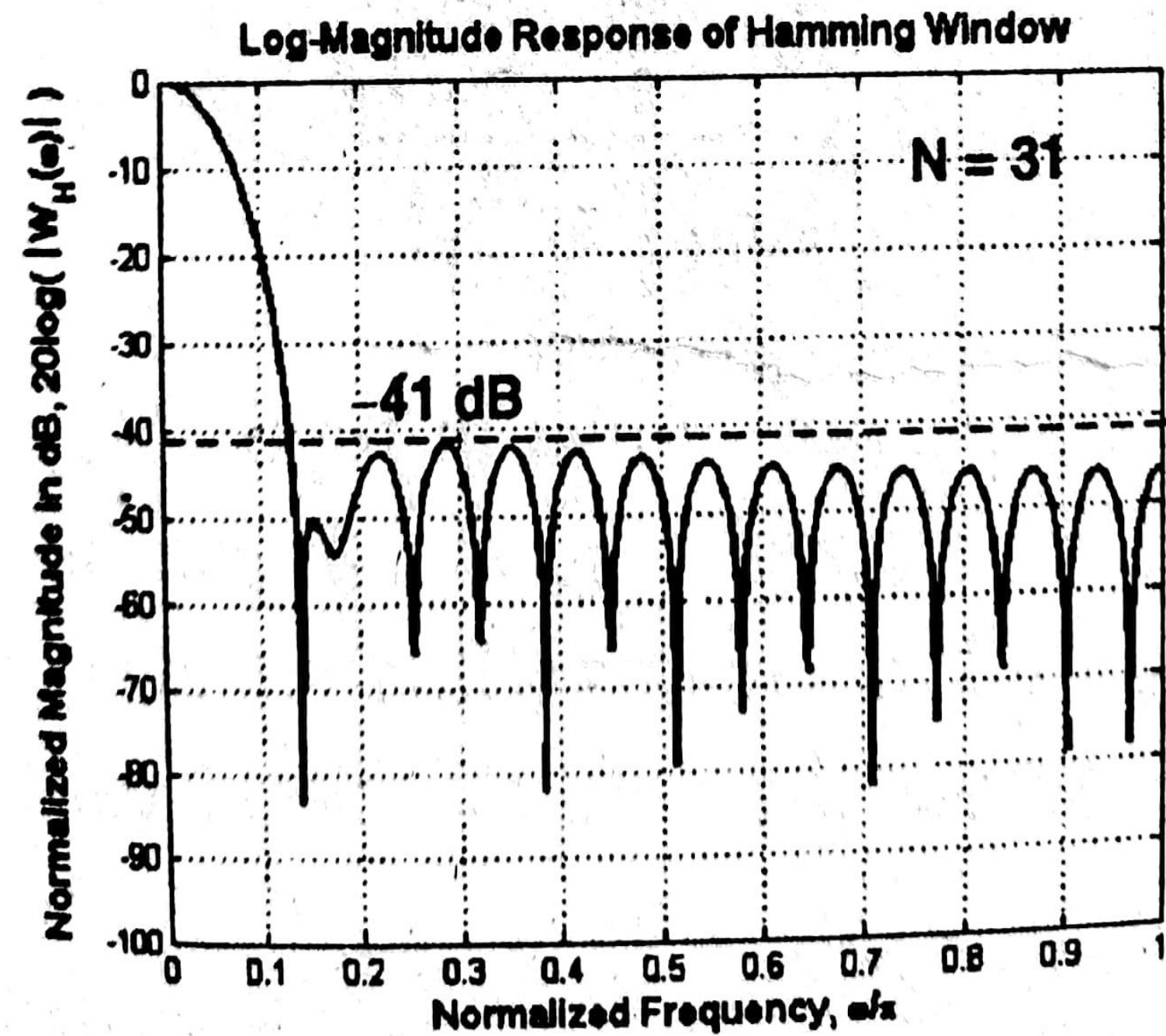
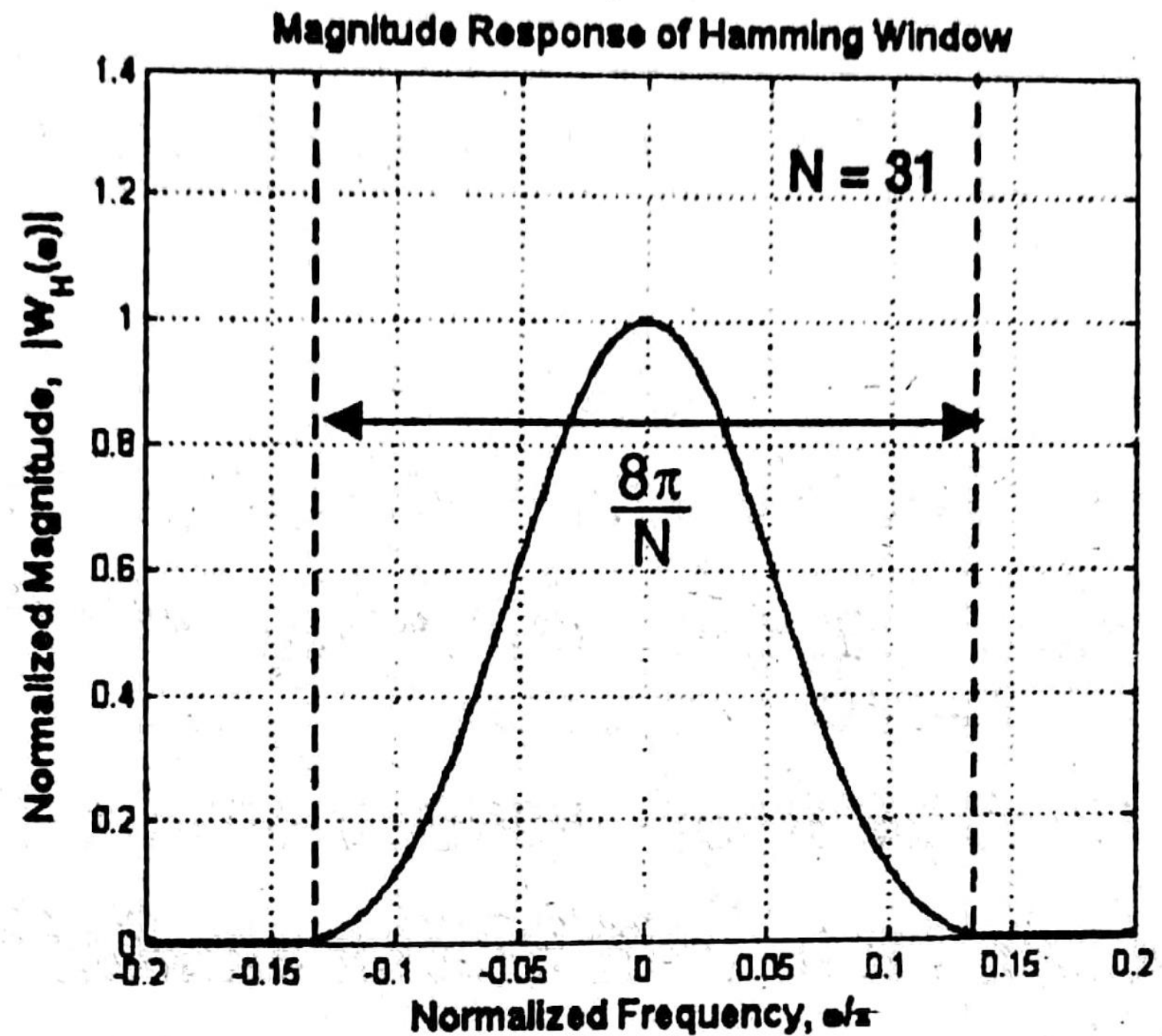


Amplitude Response of Hamming Window





HAMMING WINDOW

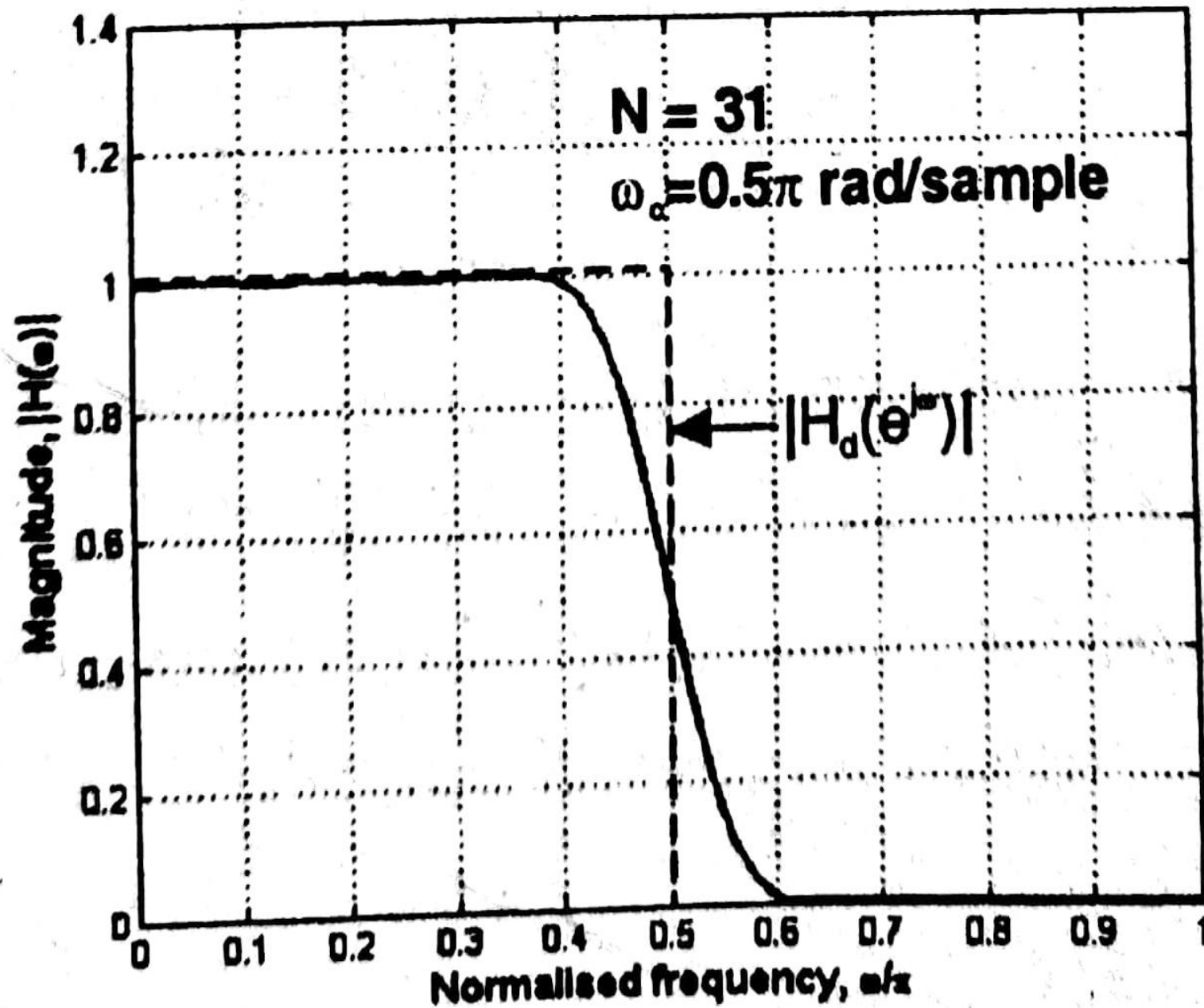




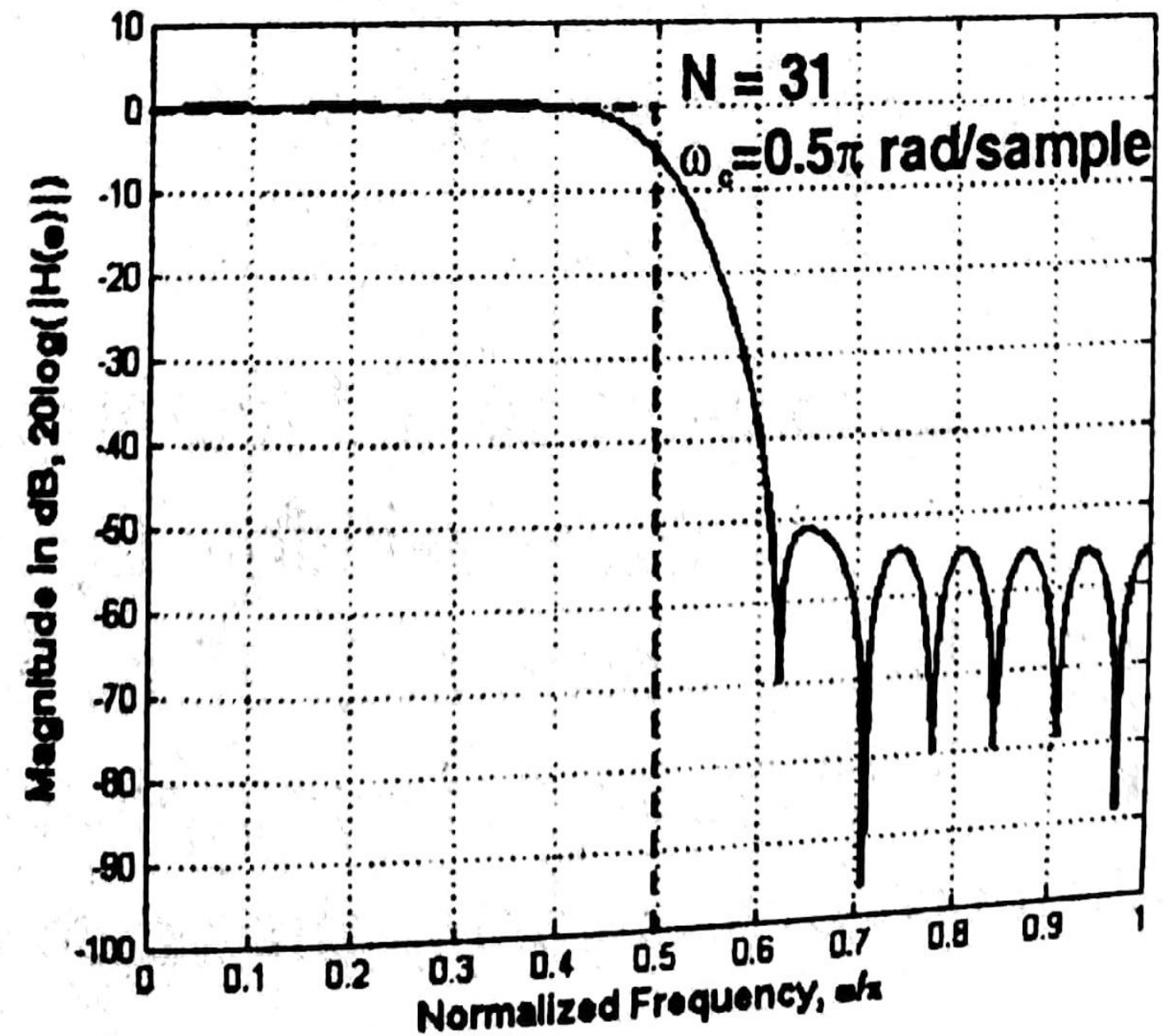
HAMMING WINDOW



Magnitude Response of Lowpass FIR Filter using $w_H(n)$



Log-Magnitude Response of Lowpass FIR Filter using $w_H(n)$





BLACKMAN WINDOW



Features of Blackman Window spectrum:

1. The main-lobe width is equal to $12\pi/N$
2. The maximum side-lobe magnitude is -58dB
3. The side-lobe magnitude decreases with increasing ω

$$w_B(n) = 0.42 + 0.5 \cos \frac{2\pi n}{N-1} + 0.08 \cos \frac{4\pi n}{N-1} \quad ; \quad \text{for } n = -\frac{N-1}{2} \text{ to } +\frac{N-1}{2}$$
$$= 0 \quad ; \quad \text{other } n$$

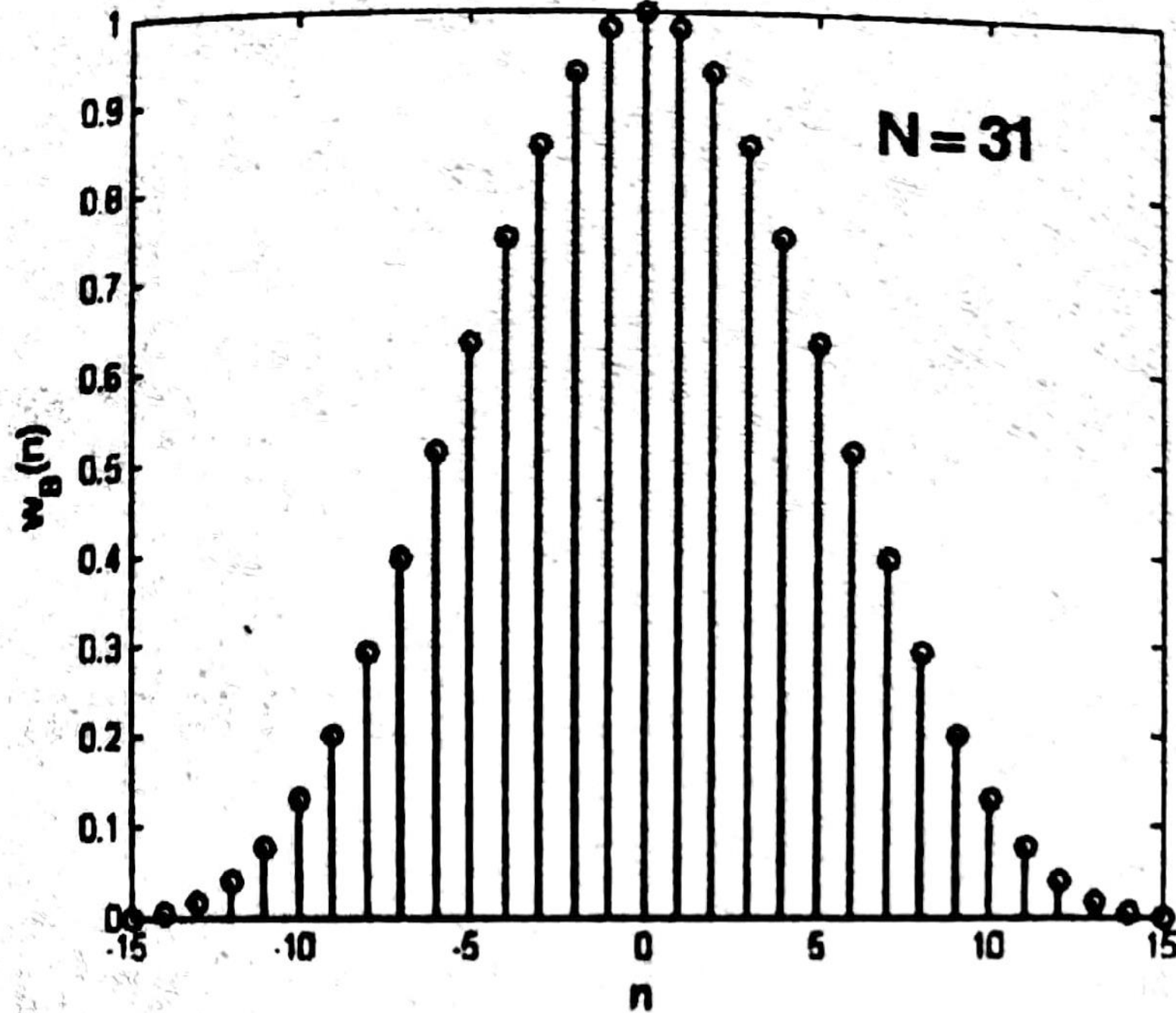
$$w_B(n) = 0.42 - 0.5 \cos \frac{2\pi n}{N-1} + 0.08 \cos \frac{4\pi n}{N-1} \quad ; \quad \text{for } n = 0 \text{ to } N-1$$
$$= 0 \quad ; \quad \text{other } n$$



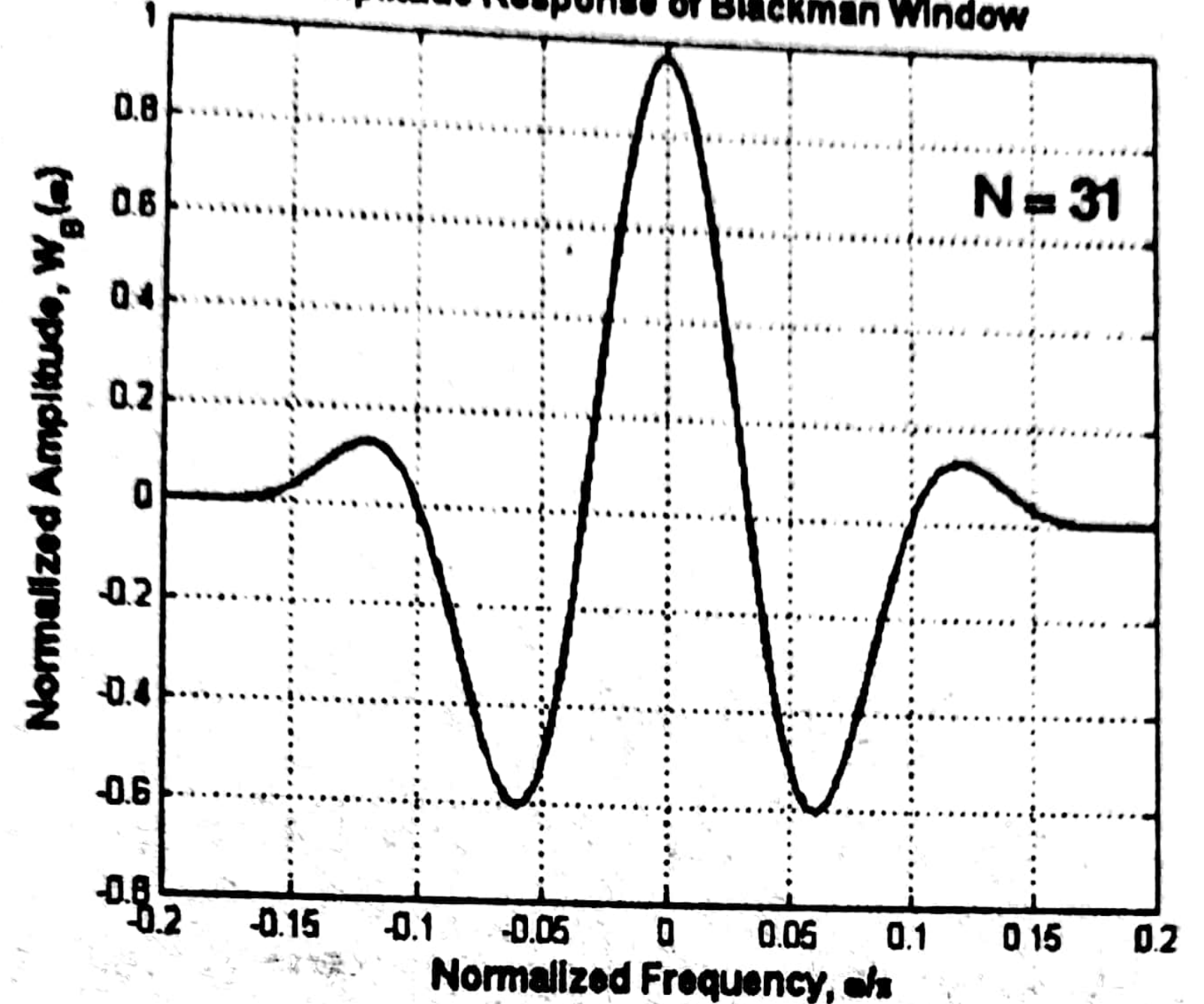
BLACKMAN WINDOW



Blackmann Window Sequence



Amplitude Response of Blackman Window

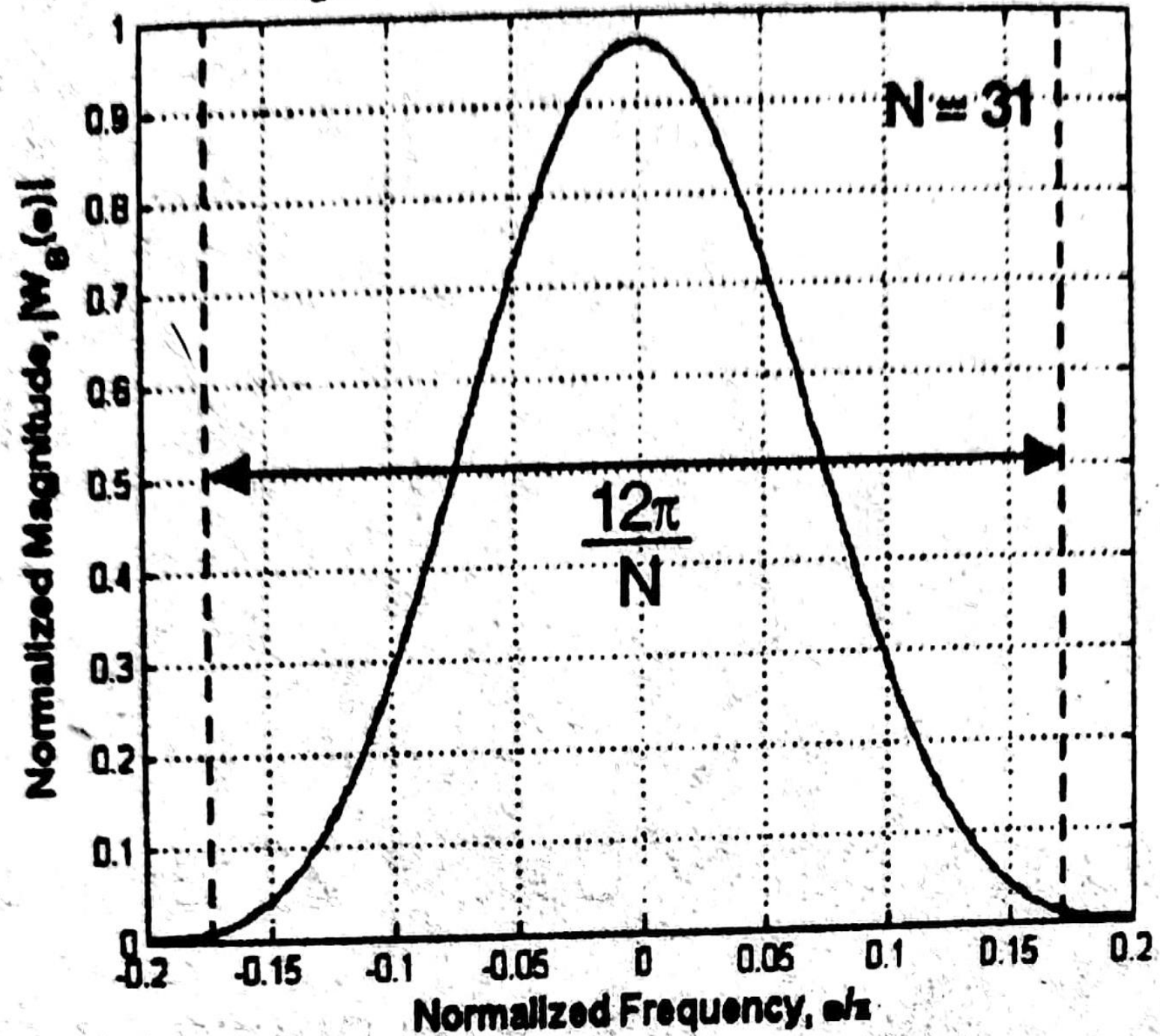




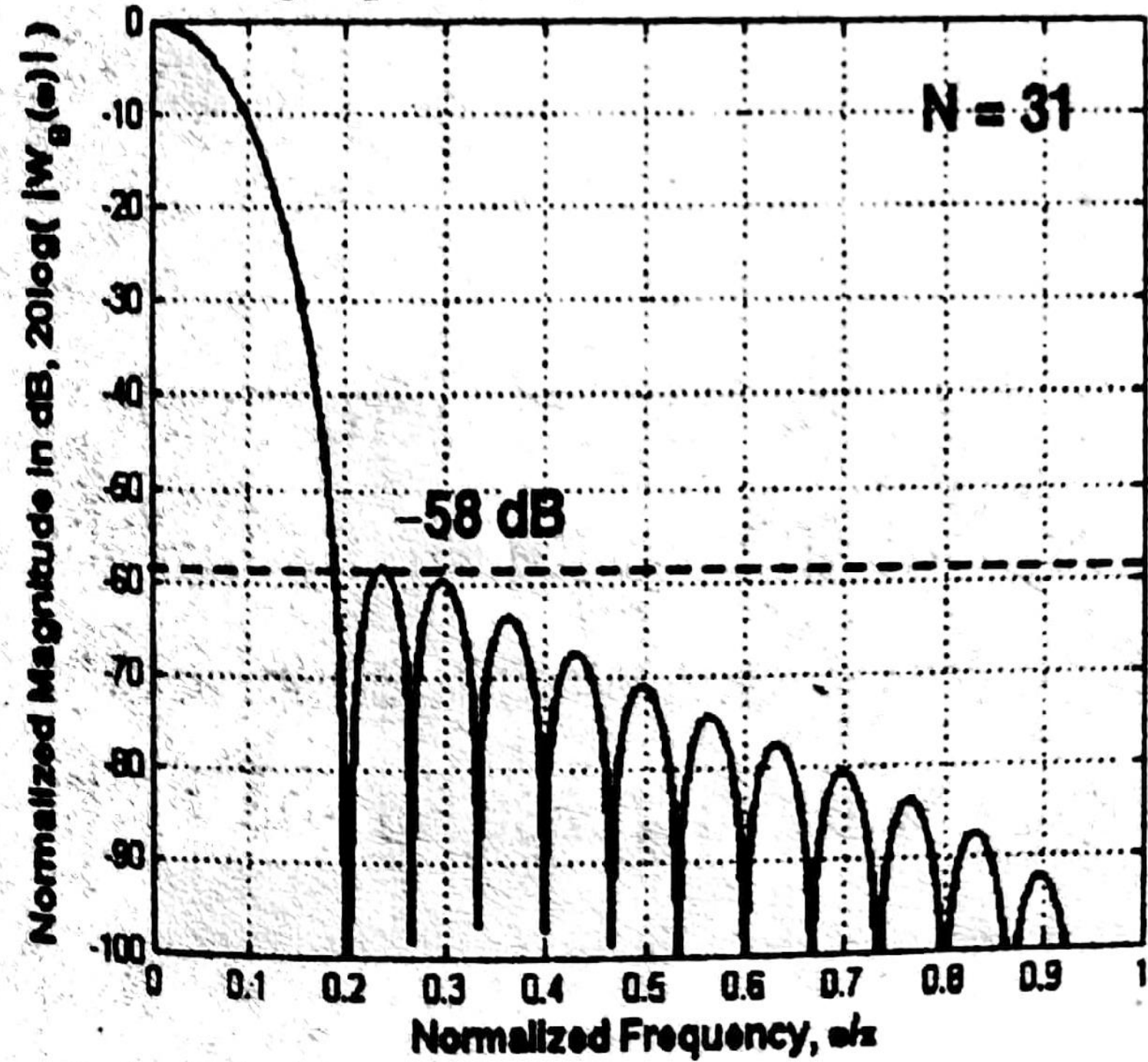
BLACKMAN WINDOW



Magnitude Response of Blackman Window



Log-Magnitude Response of Blackman Window

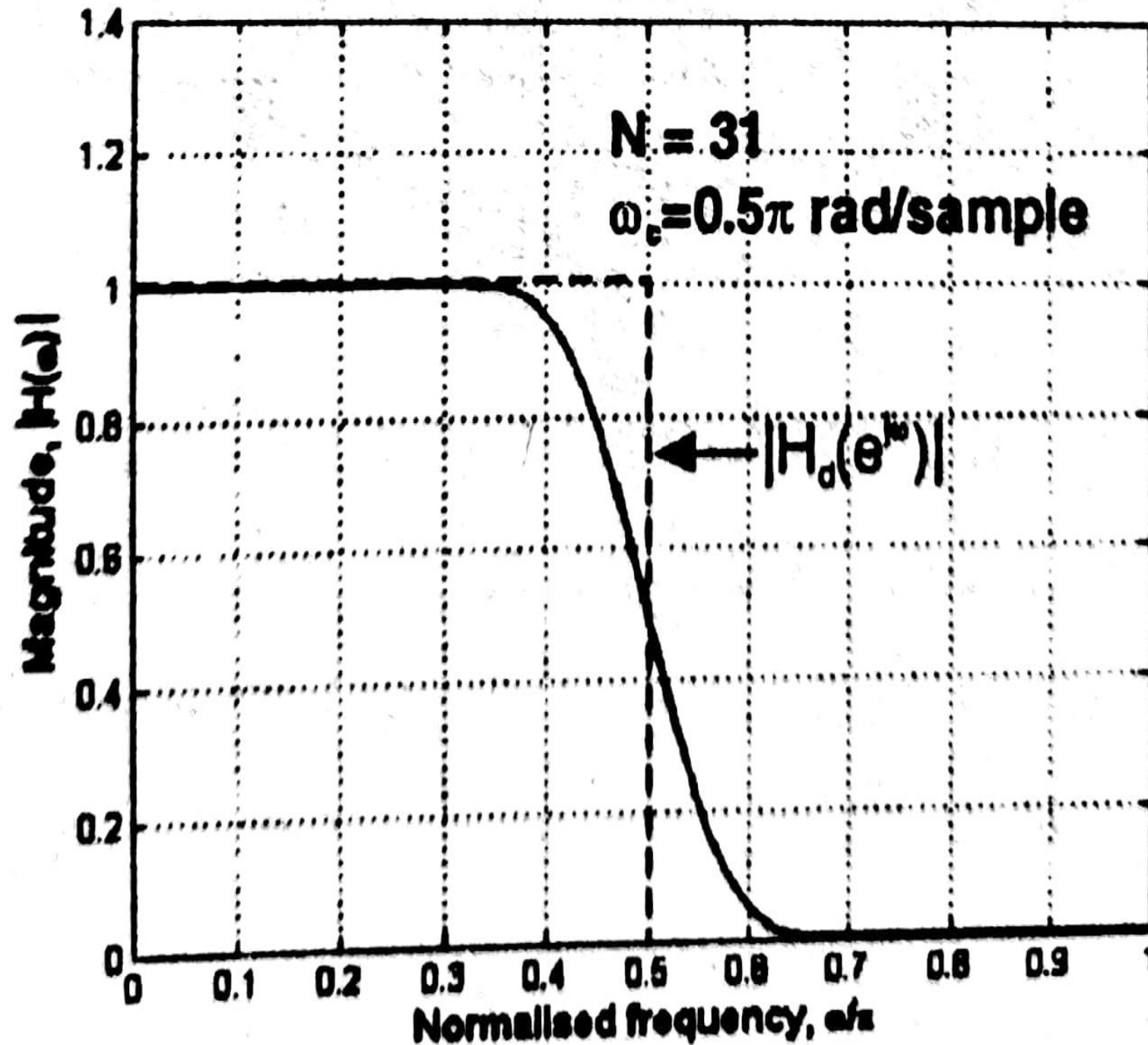




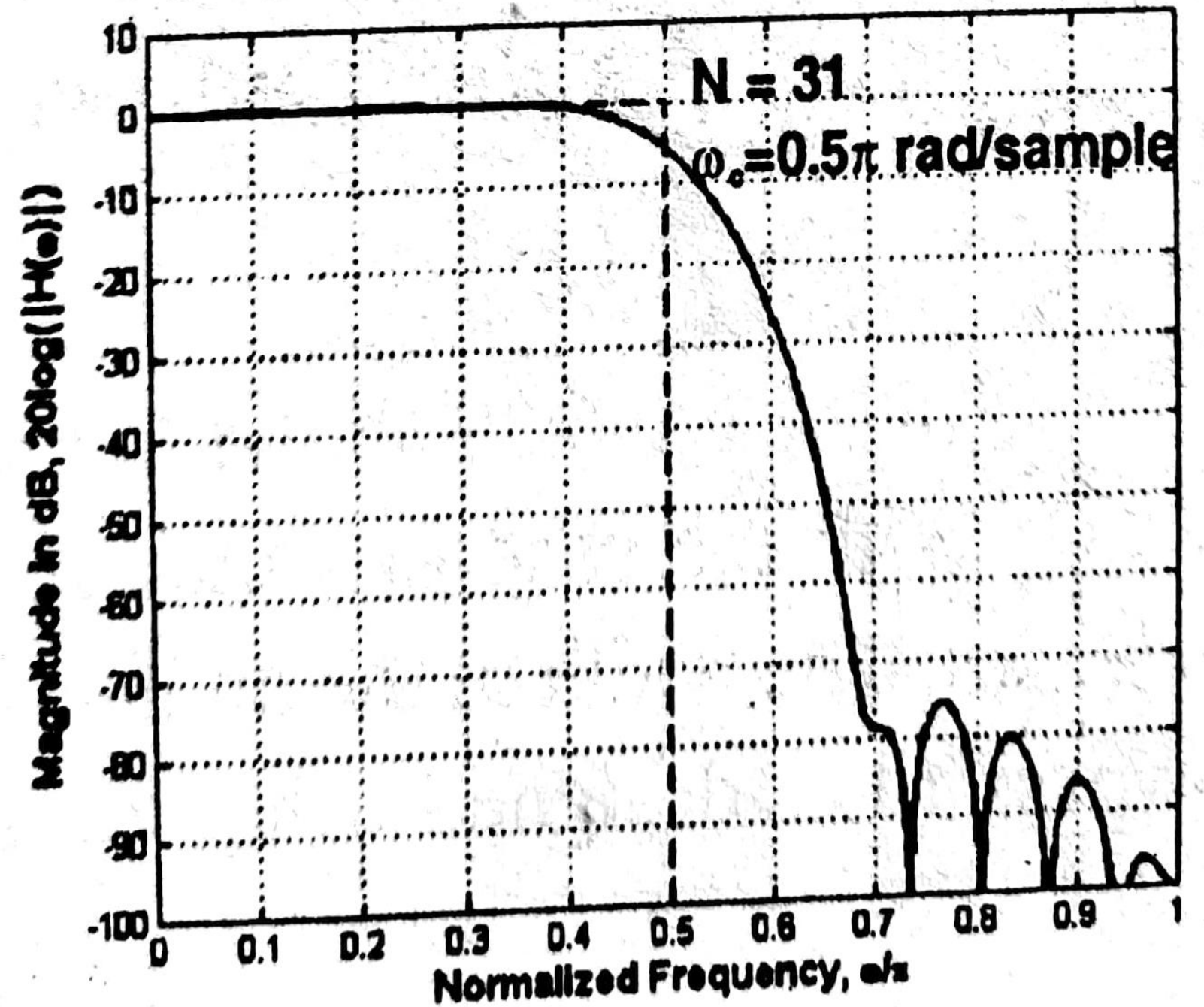
BLACKMAN WINDOW



Magnitude Response of Lowpass FIR Filter using $w_B(n)$



Log-Magnitude Response of Lowpass FIR Filter using $w_B(n)$





FREQUENCY DOMAIN CHARACTERISTICS



S.No.	Type of Window	Approximate width of main-lobe	Magnitude of first side-lobe
1	Rectangular	$4\pi/N$	-13dB
2	Hanning	$8\pi/N$	-31dB
3	Hamming	$8\pi/N$	-41dB
4	Blackman	$12\pi/N$	-58dB



IDEAL FREQUENCY RESPONSE FOR FIR FILTER DESIGN USING WINDOWS



Low Pass

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\alpha} & ; \quad -\omega_c \leq \omega \leq +\omega_c \\ 0 & ; \quad -\pi \leq \omega < -\omega_c \\ 0 & ; \quad \omega_c < \omega \leq \pi \end{cases}$$

High Pass

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\alpha} & ; \quad -\pi \leq \omega \leq -\omega_c \\ e^{-j\omega\alpha} & ; \quad \omega_c \leq \omega \leq \pi \\ 0 & ; \quad -\omega_c < \omega < +\omega_c \end{cases}$$



IDEAL FREQUENCY RESPONSE FOR FIR FILTER DESIGN USING WINDOWS



Band Pass

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\alpha} & ; & -\omega_{c2} \leq \omega \leq -\omega_{c1} \\ e^{-j\omega\alpha} & ; & \omega_{c1} \leq \omega \leq \omega_{c2} \\ 0 & ; & -\pi \leq \omega < -\omega_{c2} \\ 0 & ; & -\omega_{c1} < \omega < +\omega_{c1} \\ 0 & ; & \omega_{c2} < \omega \leq \pi \end{cases}$$

Band stop

$$H_d(e^{j\omega}) = \begin{cases} e^{-j\omega\alpha} & ; & -\pi \leq \omega \leq -\omega_{c2} \\ e^{-j\omega\alpha} & ; & -\omega_{c1} \leq \omega \leq +\omega_{c1} \\ e^{-j\omega\alpha} & ; & \omega_{c2} \leq \omega \leq \pi \\ 0 & ; & -\omega_{c2} < \omega < -\omega_{c1} \\ 0 & ; & \omega_{c1} < \omega < \omega_{c2} \end{cases}$$



DESIRED IMPULSE RESPONSE FOR FIR FILTER DESIGN USING WINDOWS



Low Pass

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\omega_c}^{\omega_c} e^{-j\omega\alpha} e^{j\omega n} d\omega$$

$$\left[\because H_d(e^{j\omega}) = 0 \text{ in the range } -\pi \leq \omega < -\omega_c \text{ and } +\omega_c < \omega \leq +\pi \right]$$

High Pass

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{+\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\pi}^{-\omega_c} e^{-j\omega\alpha} e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{\omega_c}^{\pi} e^{-j\omega\alpha} e^{j\omega n} d\omega$$

$$\left[\because H_d(e^{j\omega}) = 0 \text{ in the range } -\omega_c < \omega < +\omega_c \right]$$



DESIRED IMPULSE RESPONSE FOR FIR FILTER DESIGN USING WINDOWS



Band Pass

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{+\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\omega_{c2}}^{-\omega_{c1}} e^{-j\omega\alpha} e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{\omega_{c1}}^{\omega_{c2}} e^{-j\omega\alpha} e^{j\omega n} d\omega$$

$$\left[\because H_d(e^{j\omega}) = 0 \text{ in the range } -\pi \leq \omega < -\omega_{c2} ; -\omega_{c1} < \omega < +\omega_{c1} \text{ and } +\omega_{c2} < \omega \leq +\pi \right]$$

Band Stop

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{+\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-\pi}^{-\omega_{c2}} e^{j\omega\alpha} e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{-\omega_{c1}}^{+\omega_{c1}} e^{-j\omega\alpha} e^{j\omega n} d\omega + \frac{1}{2\pi} \int_{\omega_{c2}}^{\pi} e^{-j\omega\alpha} e^{j\omega n} d\omega$$

$$\left[\because H_d(e^{j\omega}) = 0 \text{ in the range } -\omega_{c2} < \omega < -\omega_{c1} \text{ and } +\omega_{c1} < \omega < +\omega_{c2} \right]$$



FIR FILTER DESIGN USING WINDOWS

Symmetry Condition $h(N-1-n) = h(n)$



1. The specifications of digital FIR filter are,

(i) The desired frequency response $H_d(e^{j\omega}) = C e^{-j\alpha\omega}$

Where $C = \text{Constant}$ and $\alpha = N-1/2$

(i) The cutoff frequency ω_c for lowpass and high pass ω_{c1} and ω_{c2} for bandpass and bandstop filters.

(ii) The number of samples of impulse response N

2. Determine the desired impulse response $h_d(n)$ by taking inverse Fourier transform of the desired frequency response $H_d(e^{j\omega})$

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$



FIR FILTER DESIGN USING WINDOWS



3. Choose the desired window sequence $w(n)$ defined for $n= 0$ to $N-1$. Multiply $h_d(n)$ with $w(n)$ to get the impulse response $h(n)$ of the filter. Calculate N -samples of the impulse response for $n=0$ to $N-1$

Impulse Response

$$h(n) = h_d(n) \times w(n) \text{ for } n=0 \text{ to } N-1$$

- The impulse response is symmetric with centre of symmetry at $(N-1)/2$ and so $h(N-1-n) = h(n)$. It is sufficient if we calculate $h(n)$ for $n=0$ to $(N-1)/2$
4. Take Z transform of the impulse response $h(n)$ to get the transfer function $H(z)$ of

FIR Filter

$$H(z) = \mathcal{Z}\{h(n)\} = \sum_{n=0}^{N-1} h(n) z^{-n}$$

5. Draw a suitable structure for realization of FIR filter.



FIR FILTER DESIGN USING WINDOWS



Symmetry Condition $h(-n) = h(n)$

1. The specifications of digital FIR filter are,

(i) The desired frequency response $H_d(e^{j\omega}) = C$

Where $C = \text{Constant}$ ($C=1=\text{Normalized Magnitude}$)

(i) The cutoff frequency ω_c for lowpass and high pass ω_{c1} and ω_{c2} for bandpass and bandstop filters.

(ii) The number of samples of impulse response N

2. Determine the desired impulse response $h_d(n)$ by taking inverse Fourier transform of the desired frequency response $H_d(e^{j\omega})$

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega$$



FIR FILTER DESIGN USING WINDOWS



3. Choose the desired window sequence $w(n)$ defined for $n = -\frac{(N-1)}{2}$ to $\frac{(N-1)}{2}$. Multiply $h_d(n)$ with $w(n)$ to get the impulse response $h(n)$ of the filter. Calculate N -samples of the impulse response for $n = -\frac{(N-1)}{2}$ to $\frac{(N-1)}{2}$

Impulse Response

$$h(n) = h_d(n) \times w(n) \text{ for } n = -\frac{(N-1)}{2} \text{ to } \frac{(N-1)}{2}$$

- The impulse response is symmetric with centre of symmetry at $n=0$ and so $h(-n) = h(n)$. It is sufficient if we calculate $h(n)$ for $n=0$ to $\frac{(N-1)}{2}$
4. Take Z transform of the impulse response $h(n)$ to get the transfer function $H(z)$ of FIR Filter, $H_N(z)$

$$H_N(z) = \mathcal{Z}\{h(n)\} = \sum_{n = -\frac{N-1}{2}}^{+\frac{N-1}{2}} h(n) z^{-n}$$



PROCEDURE FOR DIGITAL FIR FILTER BY FOURIER SERIES METHOD



5. Convert the noncausal transfer function, $H_N(z)$ to causal transfer function, $H(z)$ by multiplying $H_N(z) Z^{-(N-1)/2}$

$$H(z) = z^{-\frac{N-1}{2}} \sum_{n=-\frac{N-1}{2}}^{+\frac{N-1}{2}} h(n) z^{-n}$$

Transfer Function

$$H(z) = z^{-\frac{N-1}{2}} \left[h(0) + \sum_{n=1}^{\frac{N-1}{2}} h(n) \left[z^n + z^{-n} \right] \right]$$

6. Draw a suitable structure for realization of FIR filter



COMPARISON OF RECTANGULAR & HAMMING WINDOW



S.No.	Rectangular Window	Hamming Window
1	The width of the main-lobe in window spectrum is $4\pi/N$	The width of the main-lobe in window spectrum is $8\pi/N$
2	The maximum side-lobe magnitude in window spectrum is -13dB	The maximum side-lobe magnitude in window spectrum is -41dB
3	In window spectrum the side-lobe magnitude slightly decreases with increasing ω	In window spectrum the side - lobe magnitude remains constant
4	In FIR filter designed using rectangular window, the minimum stopband attenuation is 22dB	In FIR filter designed using hamming window, the minimum stopband attenuation is 51dB



COMPARISON OF HAMMING & HANNING WINDOW



S.No.	Hamming Window	Hanning Window
1	The width of the main-lobe in window spectrum is $8\pi/N$	The width of the main-lobe in window spectrum is $8\pi/N$
2	The maximum side-lobe magnitude in window spectrum is -41dB	The maximum side-lobe magnitude in window spectrum is -31dB
3	In window spectrum the side - lobe magnitude remains constant	In window spectrum the side - lobe magnitude decreases with increasing ω
4	In FIR filter designed using hamming window, the minimum stopband attenuation is 51dB	In FIR filter designed using hanning window, the minimum stopband attenuation is 44dB



COMPARISON OF HAMMING & BLACKMAN WINDOW



S.No.	Hamming Window	Blackman Window
1	The width of the main-lobe in window spectrum is $8\pi/N$	The width of the main-lobe in window spectrum is $12\pi/N$
2	The maximum side-lobe magnitude in window spectrum is -41dB	The maximum side-lobe magnitude in window spectrum is -58dB
3	In window spectrum the side - lobe magnitude remains constant with increasing ω	In window spectrum the side - lobe magnitude decreases rapidly with increasing ω
4	In FIR filter designed using hamming window, the minimum stopband attenuation is 51dB	In FIR filter designed using blackman window, the minimum stopband attenuation is 78dB



ASSESSMENT



1. The FIR filter design starts with desired frequency response $H_d(e^{j\omega})$.

The desired impulse response $h_d(n)$ is obtained by taking -----

2. List the types of windowing techniques.

3. How to calculate desired impulse response $h_d(n)$

4. Compare rectangular window and hamming window.

5. Define Blackman window.

6. Summarize the features of hamming window spectrum.

7. The transfer function $H(z)$ of FIR filter is defined as -----



THANK YOU