

19.11. RANKINE'S FORMULA

In Art. 19.10, we have learnt that Euler's formula gives correct results only for very long columns. But what happens when the column is a short or the column is not a very long. On the basis of results of experiments performed by Rankine, he established an empirical formula which is applicable to all columns whether they are short or long. The empirical formula given by Rankine is known as Rankine's formula, which is given as

$$\frac{1}{P} = \frac{1}{P_C} + \frac{1}{P_E} \quad \dots(i)$$

where P = Crippling load by Rankine's formula
 P_C = Crushing load = $\sigma_c \times A$
 σ_c = Ultimate crushing stress
 A = Area of cross-section
 P_E = Crippling load by Euler's formula
 $= \frac{\pi^2 EI}{L_e^2}$, in which L_e = Effective length

For a given column material the crushing stress σ_c is a constant. Hence the crushing load P_C (which is equal to $\sigma_c \times A$) will also be constant for a given cross-sectional area of the column. In equation (i), P_C is constant and hence value of P depends upon the value of P_E . But for a given column material and given cross-sectional area, the value of P_E depends upon the effective length of the column.

(i) If the column is a short, which means the value of L_e is small, then the value of P_E will be large. Hence the value of $\frac{1}{P_E}$ will be small enough and is negligible as compared to the value of $\frac{1}{P_C}$. Neglecting the value of $\frac{1}{P_E}$ in equation (i), we get

$$\frac{1}{P} \rightarrow \frac{1}{P_C} \quad \text{or} \quad P \rightarrow P_C$$

Hence the crippling load by Rankine's formula for a short column is approximately equal to crushing load. In Art. 19.2.1 also we have seen that short columns fail due to crushing.

(ii) If the column is long, which means the value of L_e is large. Then the value of P_E will be small and the value of $\frac{1}{P_E}$ will be large enough compared with $\frac{1}{P_C}$. Hence the value of $\frac{1}{P_C}$ may be neglected in equation (i).

$$\frac{1}{P} = \frac{1}{P_E} \quad \text{or} \quad P \rightarrow P_E$$

Hence the crippling load by Rankine's formula for long columns is approximately equal to crippling load given by Euler's formula.

Hence the Rankine's formula $\frac{1}{P} = \frac{1}{P_C} + \frac{1}{P_E}$ gives satisfactory results for all lengths of columns, ranging from short to long columns.

$$\text{Now the Rankine's formula is } \frac{1}{P} = \frac{1}{P_C} + \frac{1}{P_E} = \frac{P_E + P_C}{P_C \cdot P_E}$$

Taking reciprocal to both sides, we have

$$P = \frac{P_C \cdot P_E}{P_E + P_C} = \frac{P_C}{1 + \frac{P_C}{P_E}}$$

(Dividing the numerator and denominator by P_E)

$$= \frac{\sigma_c \times A}{1 + \frac{\sigma_c \cdot A}{\left(\frac{\pi^2 EI}{L_c^2}\right)}} \quad \left(\because P_c = \sigma_c \cdot A \text{ and } P_E = \frac{\pi^2 EI}{L_c^2} \right)$$

But $I = Ak^2$, where k = least radius of gyration

\therefore The above equation becomes as

$$\begin{aligned} P &= \frac{\sigma_c \cdot A}{1 + \frac{\sigma_c \cdot A \cdot L_c^2}{\pi^2 E \cdot Ak^2}} = \frac{\sigma_c \cdot A}{1 + \frac{\sigma_c}{\pi^2 E} \cdot \left(\frac{L_c}{k}\right)^2} \\ &= \frac{\sigma_c \cdot A}{1 + \alpha \cdot \left(\frac{L_c}{k}\right)^2} \quad \dots(19.9) \end{aligned}$$

where $\alpha = \frac{\sigma_c}{\pi^2 E}$ and is known as Rankine's constant.

The equation (19.9) gives crippling load by Rankine's formula. As the Rankine formula is empirical formula, the value of ' α ' is taken from the results of the experiments and is not calculated from the values of σ_c and E .

The values of σ_c and α for different columns material are given below in Table 19.2.

TABLE 19.2

S. No.	Material	σ_c in N/mm^2	α
1.	Wrought Iron	250	$\frac{1}{9000}$
2.	Cast Iron	550	$\frac{1}{1600}$
3.	Mild Steel	320	$\frac{1}{7500}$
4.	Timber	50	$\frac{1}{750}$

Problem 19.13. The external and internal diameter of a hollow cast iron column are 5 cm and 4 cm respectively. If the length of this column is 3 m and both of its ends are fixed, determine the crippling load using Rankine's formula. Take the values of $\sigma_c = 550 N/mm^2$ and

$\alpha = \frac{1}{1600}$ in Rankine's formula.

Sol. Given :

External dia., $D = 5$ cm

Internal dia., $d = 4$ cm

$$\therefore \text{Area, } A = \frac{\pi}{4} (5^2 - 4^2) = 2.25\pi \text{ cm}^2 = 2.25\pi \times 10^2 \text{ mm}^2 = 225\pi \text{ mm}^2$$

$$\begin{aligned} \text{Moment of Inertia, } I &= \frac{\pi}{64} [5^4 - 4^4] = 5.7656 \pi \text{ cm}^4 \\ &= 5.7656\pi \times 10^4 \text{ mm}^4 = 57656\pi \text{ mm}^4 \end{aligned}$$

∴ Least radius of gyration,

$$k = \sqrt{\frac{I}{A}} = \sqrt{\frac{57656\pi}{225\pi}} = 25.625 \text{ mm}$$

Length of column, $l = 3 \text{ m} = 3000 \text{ mm}$

As both the ends are fixed,

∴ Effective length, $L_e = \frac{l}{2} = \frac{3000}{2} = 1500 \text{ mm}$

Crushing stress, $\sigma_c = 550 \text{ N/mm}^2$

Rankine's constant, $a = \frac{1}{1600}$

Let P = Crippling load by Rankine's formula

Using equation (19.9), we have

$$\begin{aligned} P &= \frac{\sigma_c \cdot A}{1 + \left(\frac{L_e}{k}\right)^2} = \frac{550 \times 225\pi}{1 + \frac{1}{1600} \times \left(\frac{1500}{25.625}\right)^2} \\ &= \frac{550 \times 225\pi}{3.1415} = 123750 \text{ N. Ans.} \end{aligned}$$

Problem 19.14. A hollow cylindrical cast iron column is 4 m long with both ends fixed. Determine the minimum diameter of the column if it has to carry a safe load of 250 kN with a factor of safety of 5. Take the internal diameter as 0.8 times the external diameter. Take $\sigma_c = 550 \text{ N/mm}^2$ and $a = \frac{1}{1600}$ in Rankine's formula. (AMIE, Winter 1983)

Sol. Given :

Length of column, $l = 4 \text{ m} = 4000 \text{ mm}$

End conditions = Both ends fixed

∴ Effective length, $L_e = \frac{l}{2} = \frac{4000}{2} = 2000 \text{ mm}$

Safe load, = 250 kN

Factor of safety, = 5

Let External dia., = D

Internal dia., = $0.8 \times D$

Crushing stress, $\sigma_c = 550 \text{ N/mm}^2$

Value of 'a' = $\frac{1}{1600}$ in Rankine's formula

Now factor of safety = $\frac{\text{Crippling load}}{\text{Safe load}}$ or $5 = \frac{\text{Crippling load}}{250}$

∴ Crippling load, $P = 5 \times 250 = 1250 \text{ kN} = 1250000 \text{ N}$

Area of column, $A = \frac{\pi}{4} [D^2 - (0.8D)^2]$
 $= \frac{\pi}{4} [D^2 - 0.64D^2] = \frac{\pi}{4} \times 0.36D^2 = \pi \times 0.09D^2$

Moment of Inertia, $I = \frac{\pi}{64} [D^4 - (0.8D)^4] = \frac{\pi}{64} [D^4 - 0.4096D^4]$

$$= \frac{\pi}{64} \times 0.5904 \times D^4 = 0.009225 \times \pi \times D^4$$

But $I = A \times k^2$, where k is radius of gyration

$$\therefore k = \sqrt{\frac{I}{A}} = \sqrt{\frac{0.009225 \times \pi D^4}{\pi \times 0.09 \times D^2}} = 0.32D$$

Now using equation (19.9), $P = \frac{\sigma_c \cdot A}{1 + \alpha \left(\frac{L_c}{k}\right)^2}$

or $1250000 = \frac{550 \times \pi \times 0.09 D^2}{1 + \frac{1}{1600} \times \left(\frac{2000}{0.32D}\right)^2}$ ($\because A = \pi \times 0.09D^2$)

$$\frac{1250000}{550 \times \pi \times 0.09} = \frac{D^2}{1 + \frac{24414}{D^2}} \quad \text{or} \quad 8038 = \frac{D^2 \times D^2}{D^2 + 24414}$$

or $8038D^2 + 8038 \times 24414 = D^4$ or $D^4 - 8038D^2 - 8038 \times 24414 = 0$

or $D^4 - 8038 D^2 - 196239700 = 0$.

The above equations is a quadratic equation in D^2 . The solution is

$$\therefore D^2 = \frac{8038 \pm \sqrt{8038^2 + 4 \times 1 \times 196239700}}{2}$$

$$\left(\text{Roots} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} \right)$$

$$= \frac{8038 \pm \sqrt{646094 + 784958800}}{2} = \frac{8038 \pm 29147}{2}$$

$$= \frac{8038 + 29147}{2} \quad (\text{The other root is not possible})$$

$$= 18592.5 \text{ mm}^2$$

$$\therefore D = \sqrt{18592.5} = 136.3 \text{ mm}$$

\therefore External diameter = 136.3 mm. Ans.

Internal diameter = $0.8 \times 136.3 = 109 \text{ mm}$. Ans.

Problem 19.18. A hollow cast iron column 200 mm outside diameter and 150 mm inside diameter, 8 m long has both ends fixed. It is subjected to an axial compressive load. Taking a factor of safety as 6, $\sigma_c = 560 \text{ N/mm}^2$, $\alpha = \frac{1}{1600}$, determine the safe Rankine load.

(AMIE, Summer 1990)

Sol. Given :

External dia., $D = 200 \text{ mm}$

Internal dia., $d = 150 \text{ mm}$

Length, $l = 8 \text{ m} = 8000 \text{ mm}$

End conditions = Both the ends are fixed

Crushing stress, $\sigma_c = 560 \text{ N/mm}^2$

Rankine's constant, $\alpha = \frac{1}{1600}$

Safety factor = 6

$$\begin{aligned} \text{Area of cross-section, } A &= \frac{\pi}{4} (D^2 - d^2) = \frac{\pi}{4} (200^2 - 150^2) \\ &= \frac{\pi}{4} (40000 - 22500) = 13744 \text{ mm}^2 \end{aligned}$$

$$\begin{aligned} \text{Moment of inertia, } I &= \frac{\pi}{64} (D^4 - d^4) = \frac{\pi}{64} (200^4 - 150^4) \\ &= \frac{\pi}{64} (1600000000 - 506250000) = 53689000 \text{ mm}^4 \end{aligned}$$

$$\text{Least radius of gyration, } k = \sqrt{\frac{I}{A}} = \sqrt{\frac{53689000}{13744}} = 62.5 \text{ mm}$$

Let P = Crippling load by Rankine formula.

$$\text{Using equation (19.9), } P = \frac{\sigma_c \times A}{1 + \alpha \left(\frac{L_e}{k} \right)^2}$$

$$\text{where } L_e = \text{Effective length} = \frac{l}{2} = \frac{8000}{2} = 4000 \text{ mm}$$

$$\begin{aligned} P &= \frac{560 \times 13744}{1 + \frac{1}{1600} \times \left(\frac{4000}{62.5} \right)^2} \\ &= \frac{7696640}{1 + 2.56} = \frac{7696640}{3.56} = 2161977 \text{ N} = 2161.977 \text{ kN} \end{aligned}$$

$$\therefore \text{ Safe load} = \frac{\text{Crippling load}}{\text{Factor of safety}} = \frac{2161.977}{6} = 360.3295 \text{ kN. Ans.}$$