



# **SNS COLLEGE OF TECHNOLOGY**

## **AN AUTONOMOUS INSTITUTION**



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### **DEPARTMENT OF AGRICULTURAL ENGINEERING**

**COURSE CODE & NAME: 19AGT301 & HEAT POWER ENGINEERING**

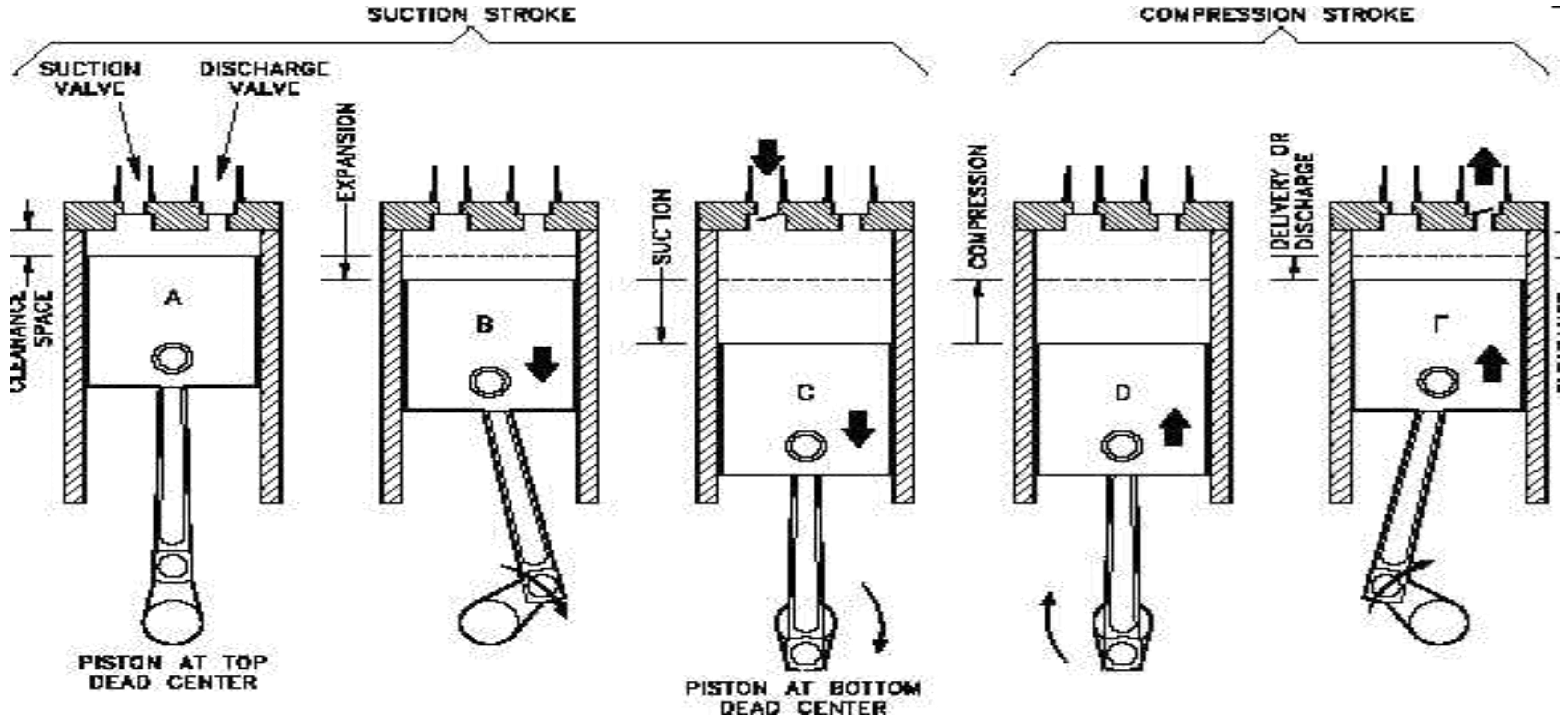
**III YEAR / V SEMESTER**

**UNIT : IV IC ENGINE PERFORMANCE AND AIR COMPRESSORS**

**TOPIC 7 :Air Compressors**

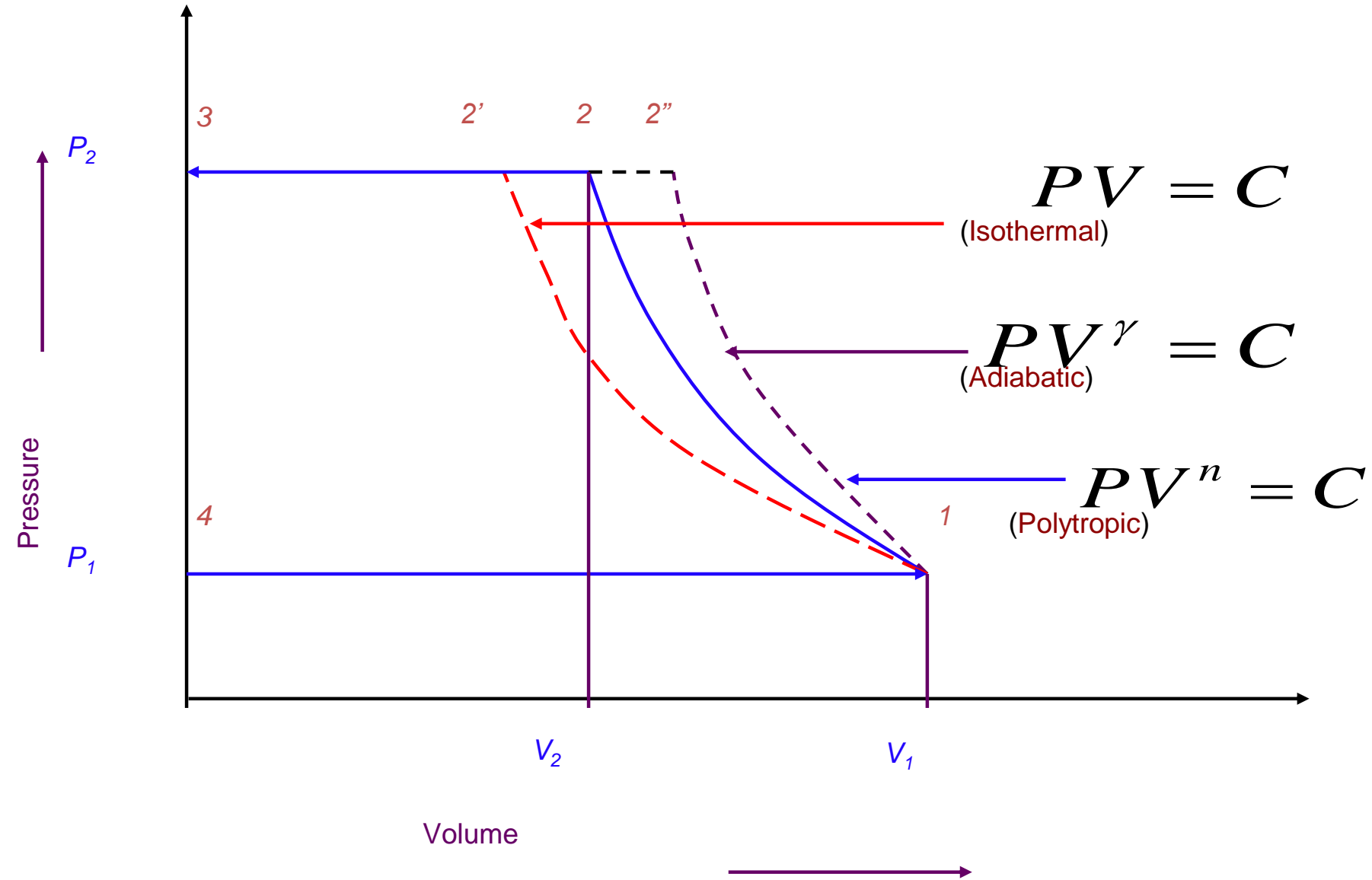


# Reciprocating Compressor - Working





# Reciprocating Compressor – Equation for Work



Operations : 4 – 1 : Volume  $V_1$  of air aspirated into Compressor, at  $P_1$  and  $T_1$ .  
 1 – 2 : Air compressed according to  $PV^n = \text{Const.}$  from  $P_1$  to  $P_2$ .

→ Temp increase from  $T_1$  to  $T_2$ .

2 – 3 : Compressed air at  $P_2$  and  $V_2$  with temperature  $T_2$  is delivered.



# Reciprocating Compressor – Equation for Work



During **Compression**, due to the **excess temperature** above surrounding, the air will exchange the heat to the surrounding.

⇒ Compression Index,  $n$  is always less than  $\gamma$ , the **adiabatic** index.

As **Compressor** is a **work consuming device**, every effort is desired to reduce the work.

Work done = Area under  $P$ - $V$  curve

⇒  $1 - 2''$  : Adiabatic Compression = Max. Work.

⇒  $1 - 2$  : Polytropic Compression

⇒  $1 - 2'$  : Isothermal Compression = Min. Work.



# Reciprocating Compressor – Equation for Work

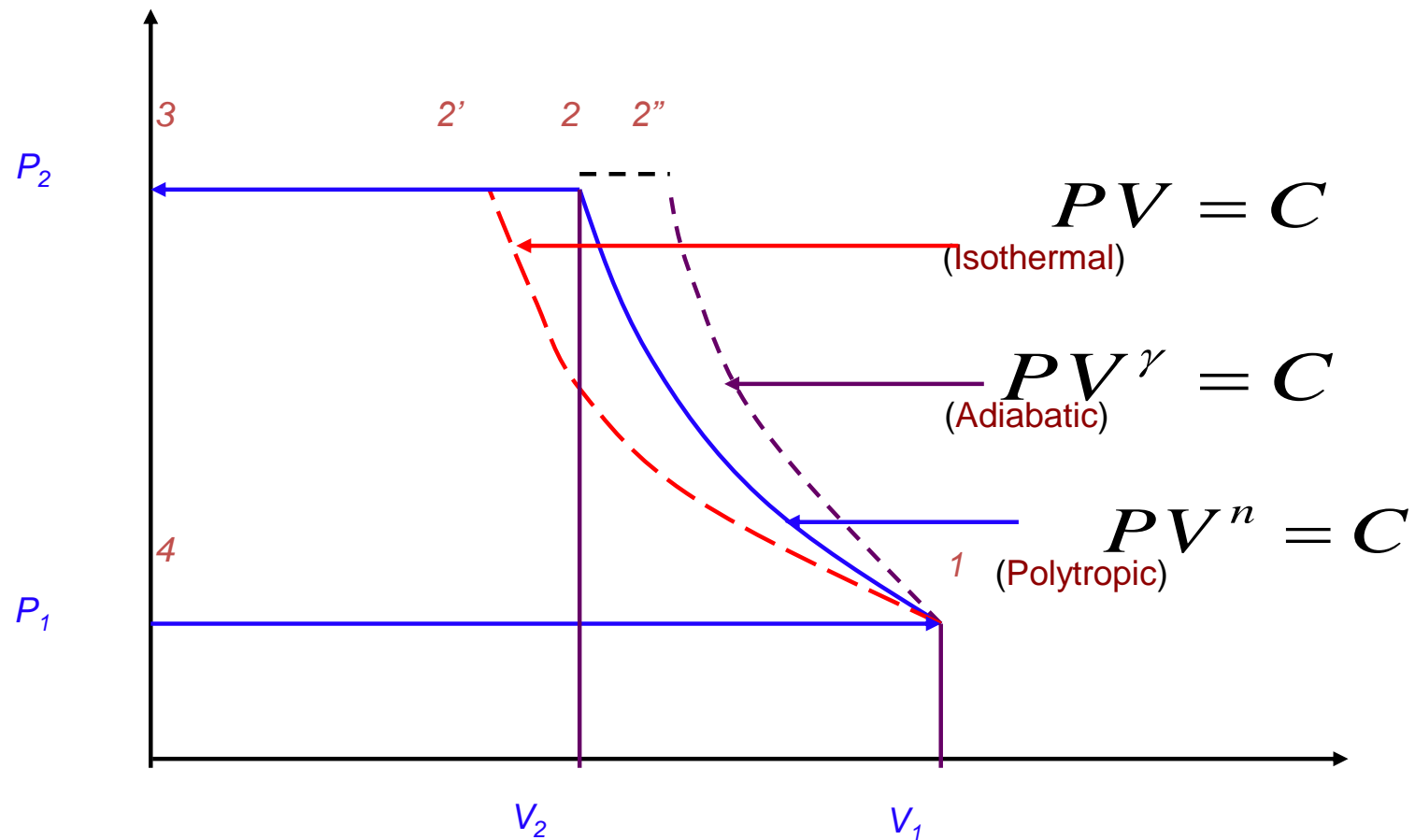


Thus, comparison between the **Isothermal Work** and the **Actual Work** is important.

Isothermal Efficiency,  $\eta_{iso} =$

$$\frac{\text{Isothermal Work}}{\text{Actual Work}}$$

Thus, more the **Isothermal Efficiency**, more the actual compression approaches to the **Isothermal Compression**.



Actual Work =  $W_{act} = \text{Area } 4-1-2-3-4$

$W_{act} = \text{Area } (4-1) - \text{Area } (1-2) - \text{Area } (2-3)$

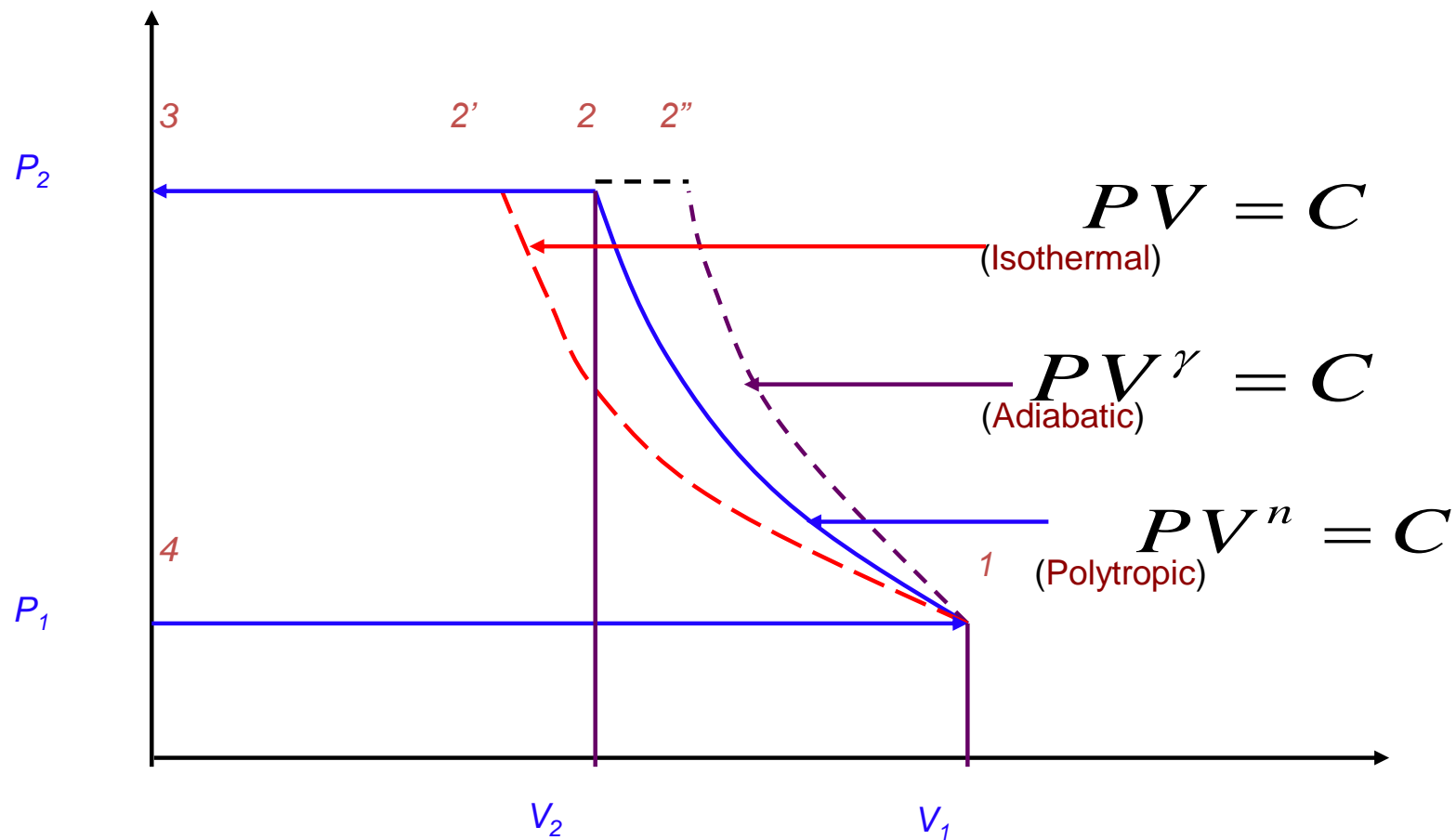
$$= P_1 V_1 - \frac{P_2 V_2 - P_1 V_1}{n-1} - P_2 V_2$$

$$= (P_1 V_1 - P_2 V_2) - \left( \frac{P_2 V_2 - P_1 V_1}{n-1} \right)$$

$$= (P_1 V_1 - P_2 V_2) + \left( \frac{P_1 V_1 - P_2 V_2}{n-1} \right)$$



# Reciprocating Compressor – Equation for Work



Now,

$$W_{iso} = \left( 1 + \frac{1}{n-1} \right) (P_1 V_1 - P_2 V_2)$$

$$= \left( \frac{n}{n-1} \right) (P_1 V_1 - P_2 V_2)$$

$$= \left( \frac{n}{n-1} \right) P_1 V_1 \left( 1 - \frac{P_2 V_2}{P_1 V_1} \right)$$

$$P_1 V_1^n = P_2 V_2^n$$

$$\Rightarrow \frac{V_2}{V_1} = \left( \frac{P_1}{P_2} \right)^{1/n}$$

$$W_{iso} = \left( \frac{n}{n-1} \right) P_1 V_1 \left\{ 1 - \frac{P_2}{P_1} \left( \frac{P_1}{P_2} \right)^{1/n} \right\}$$



# Reciprocating Compressor – Equation for Work



$$W_{iso} = \left( \frac{n}{n-1} \right) P_1 V_1 \left\{ 1 - \frac{P_2}{P_1} \left( \frac{P_1}{P_2} \right)^{1/n} \right\}$$

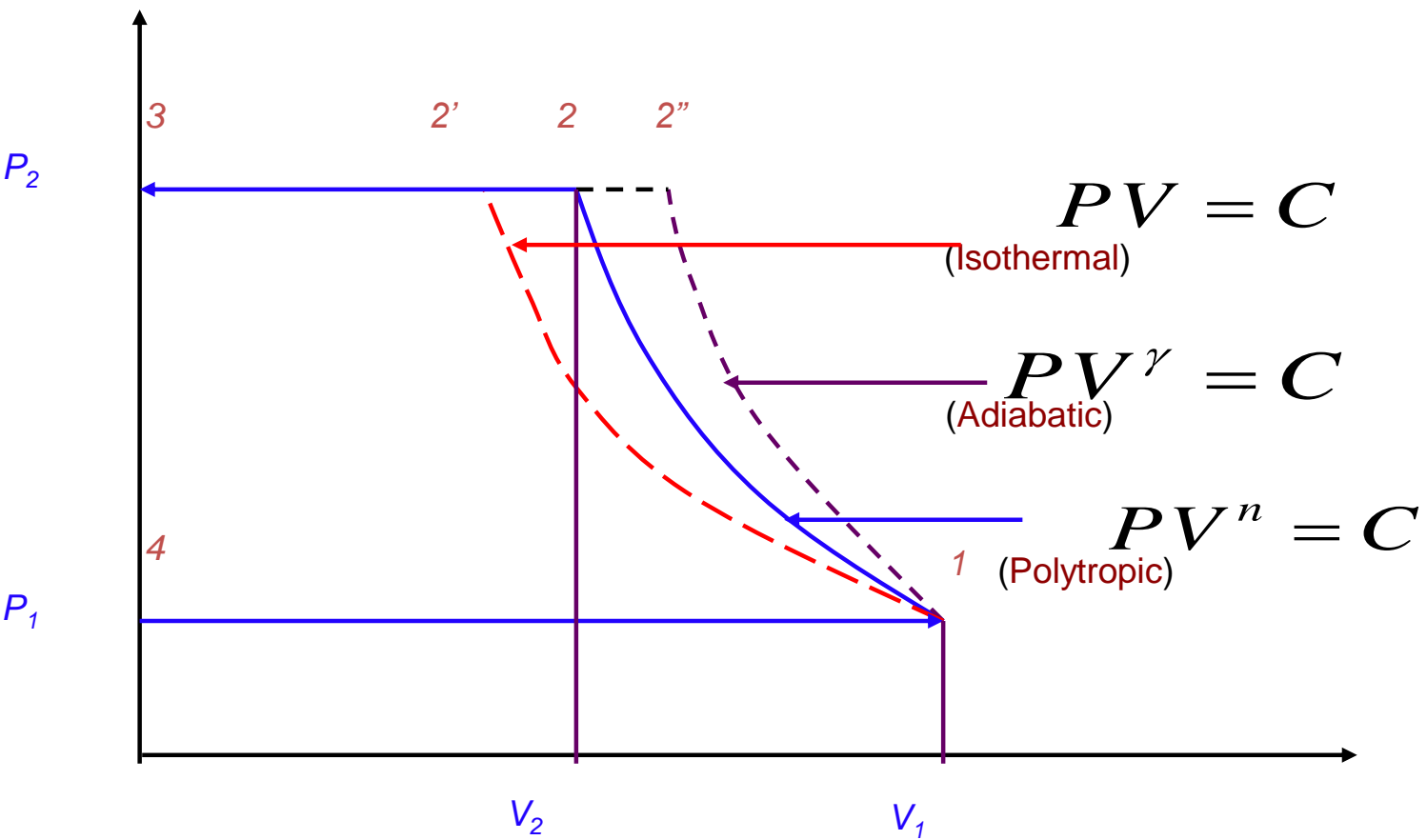
$$= \left( \frac{n}{n-1} \right) P_1 V_1 \left\{ 1 - \frac{P_2}{P_1} \left( \frac{P_2}{P_1} \right)^{-1/n} \right\}$$

$$W_{iso} = \left( \frac{n}{n-1} \right) P_1 V_1 \left\{ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} \right\}$$

$$W_{iso} = \left( \frac{n}{n-1} \right) mRT_1 \left\{ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}} \right\}$$

The solution of this equation is always *negative*.

This shows that Work is done *ON* the Compressor.



Delivery Temperature,

$$T_2 = T_1 \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}}$$

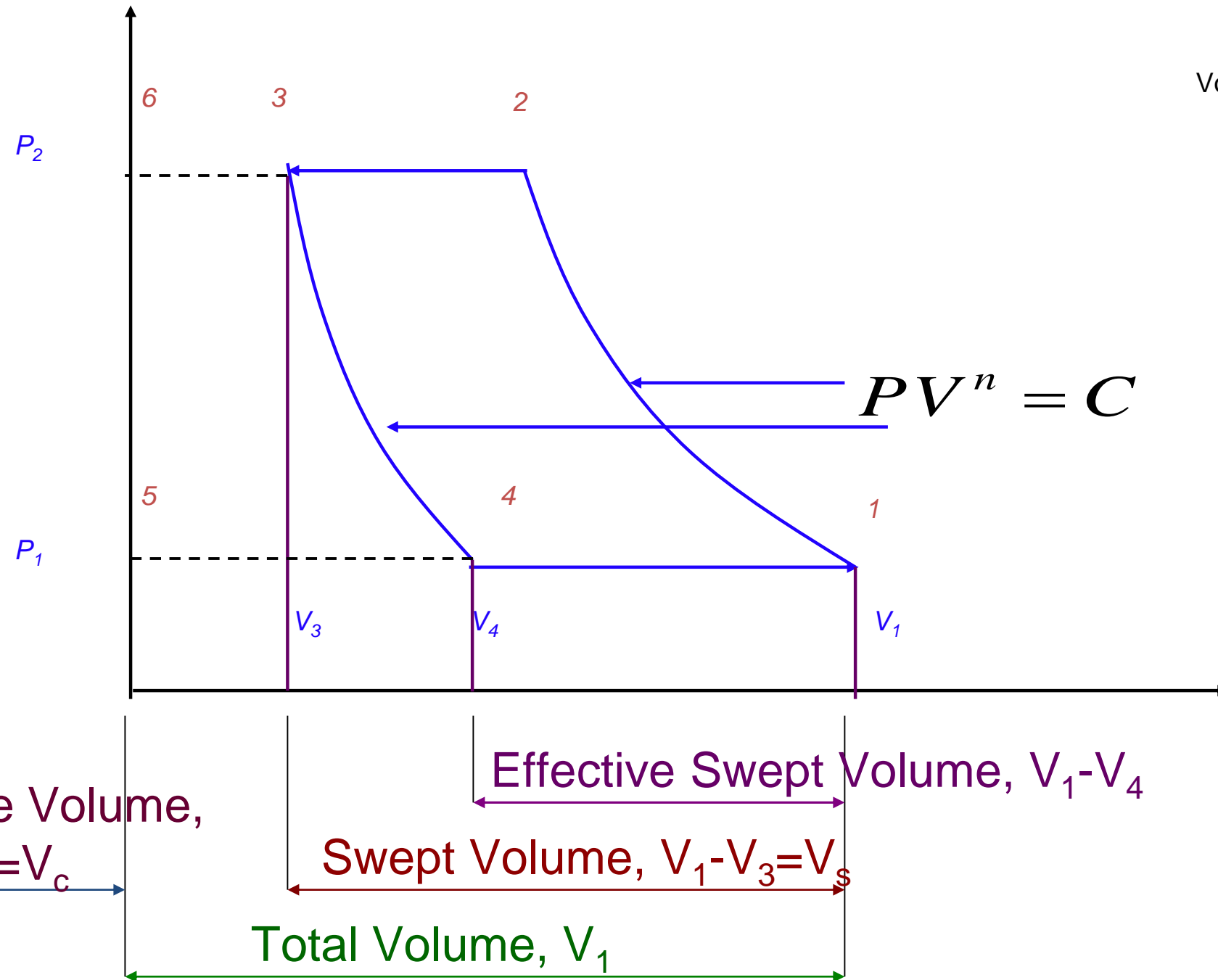


# Reciprocating Compressor – Equation for Work



Clearance Volume :

Volume that remains inside the cylinder after the piston reaches the end of its inward stroke.



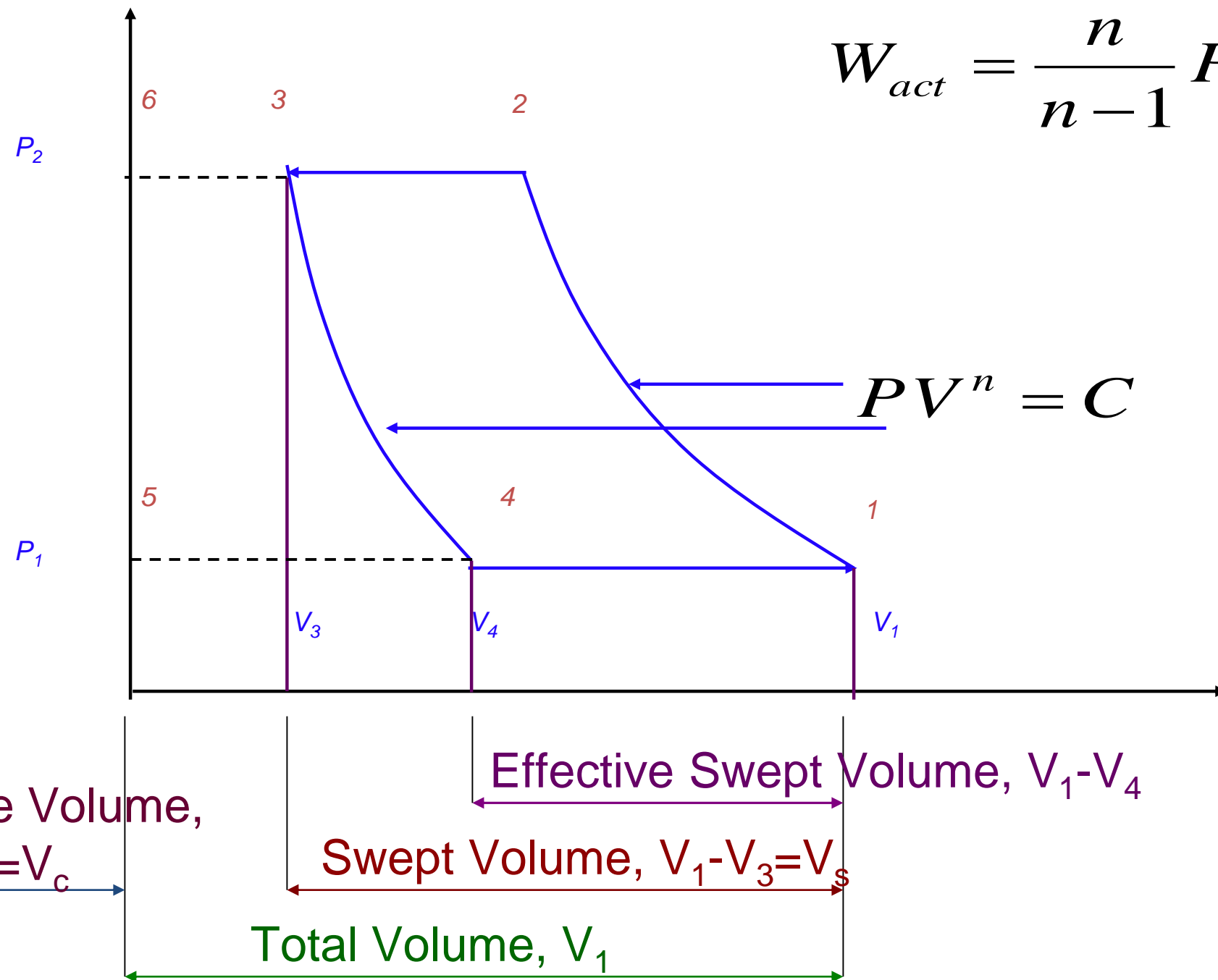
Thus, *Effective Stroke Volume* =  $V_1 - V_4$

Actual Work =  $W_{act} = \text{Area } 1-2-3-4$

$W_{act} = \text{Area } (5-1-2-6) - \text{Area } (5-4-3-6)$



# Reciprocating Compressor – Equation for Work

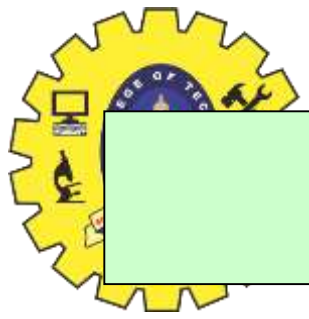


$$W_{act} = \frac{n}{n-1} P_1 V_1 \left\{ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{m-1}{n}} \right\} - \frac{n}{n-1} P_4 V_4 \left\{ 1 - \left( \frac{P_3}{P_4} \right)^{\frac{m-1}{n}} \right\}$$

$$\Rightarrow W_{act} = \frac{n}{n-1} P_1 V_1 \left\{ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{m-1}{n}} \right\} - \frac{n}{n-1} P_1 V_4 \left\{ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{m-1}{n}} \right\}$$

$$W_{act} = \left( \frac{n}{n-1} \right) P_1 (V_1 - V_4) \left\{ 1 - \frac{P_2}{P_1} \left( \frac{P_1}{P_2} \right)^{1/n} \right\}$$

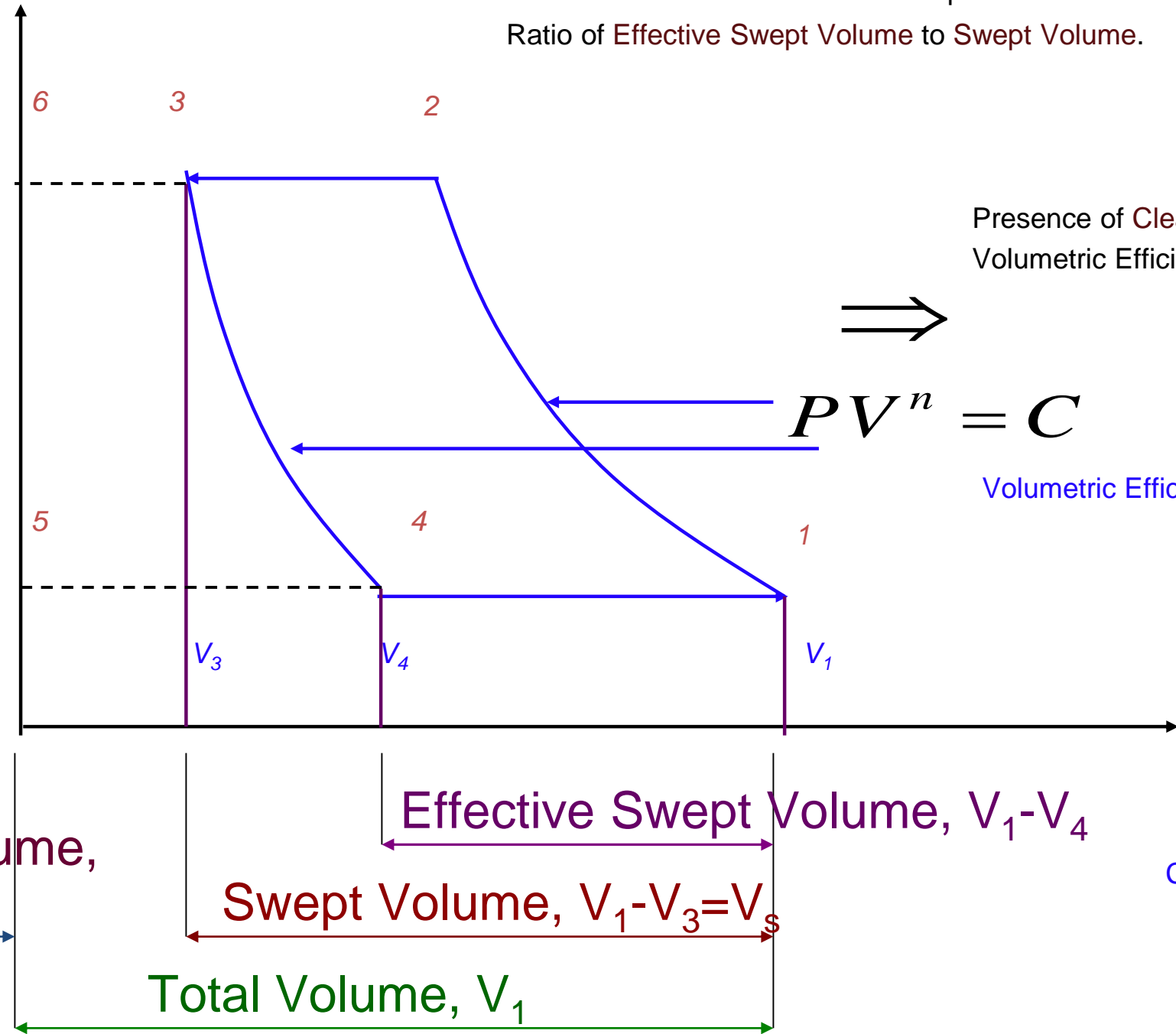
But,  $P_4 = P_1$  and  $P_3 = P_2$



# Reciprocating Compressor – Volumetric Efficiency

Volumetric Efficiency :

Ratio of free air delivered to the displacement of the compressor.  
 Ratio of Effective Swept Volume to Swept Volume.



Presence of Clearance Volume  
 Volumetric Efficiency *less than* 1. ( 60 – 85 % )

$$PV^n = C$$

Volumetric Efficiency =

Clearance Volume,  
 $V_3 = V_c$

Effective Swept Volume,  $V_1 - V_4$   
 Swept Volume,  $V_1 - V_3 = V_s$   
 Total Volume,  $V_1$

Clearance Ratio =

Effective Swept Volume

Swept Volume

$$V_1 - V_4$$

=

$$V_1 - V_3$$

Clearance Volume

Swept Volume

$$V_c$$

=

$$V_s$$

=  $\gamma$

( 4 – 10 % )



# Reciprocating Compressor – Volumetric Efficiency



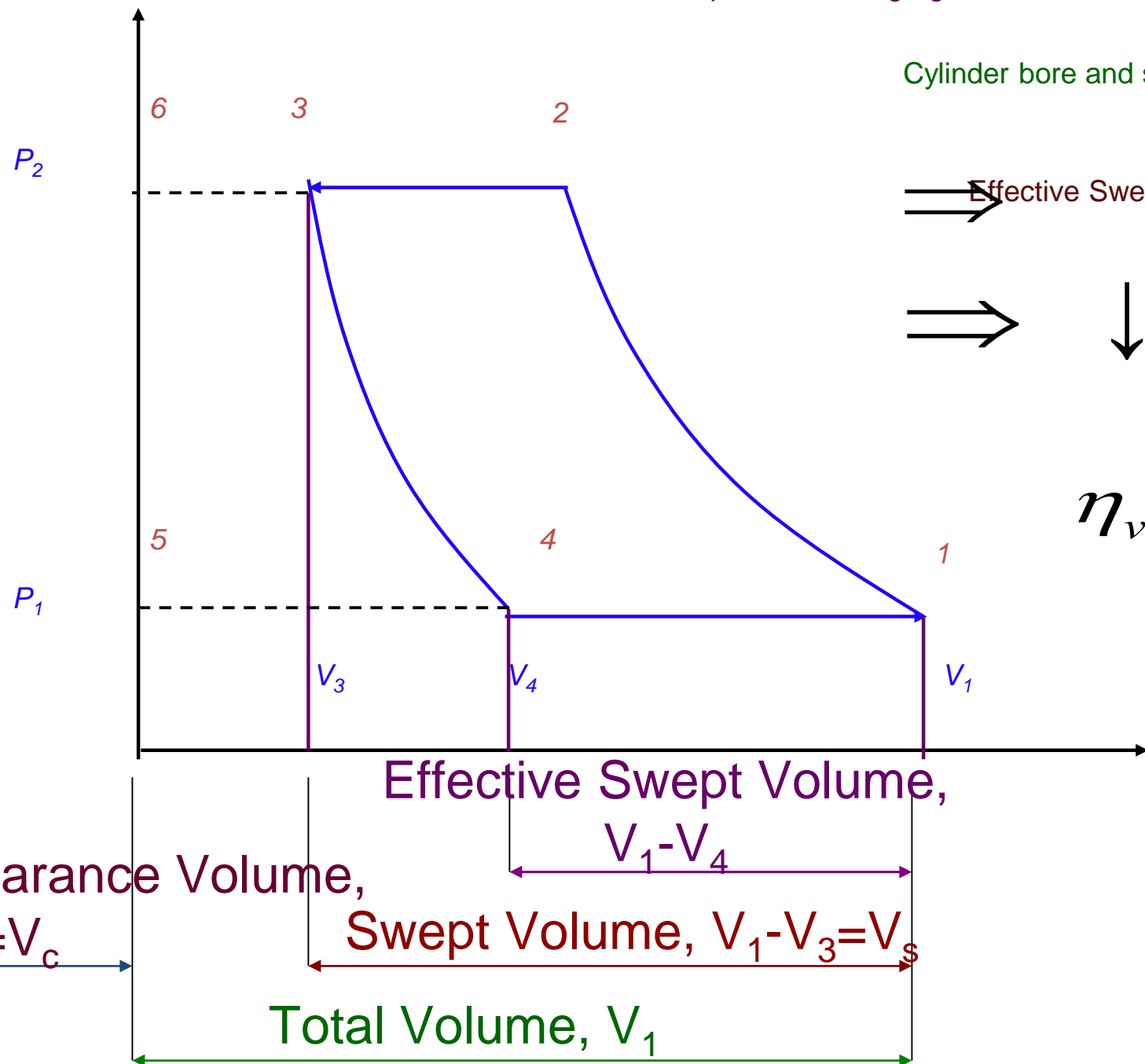
↑ Pr. Ratio    ↑ Effect of Clearance Volume

...Clearance air expansion through greater volume before intake

Cylinder bore and stroke is fixed.

⇒ Effective Swept Volume ( $V_1 - V_4$ ) ↓ with ↑ Pr. Ratio

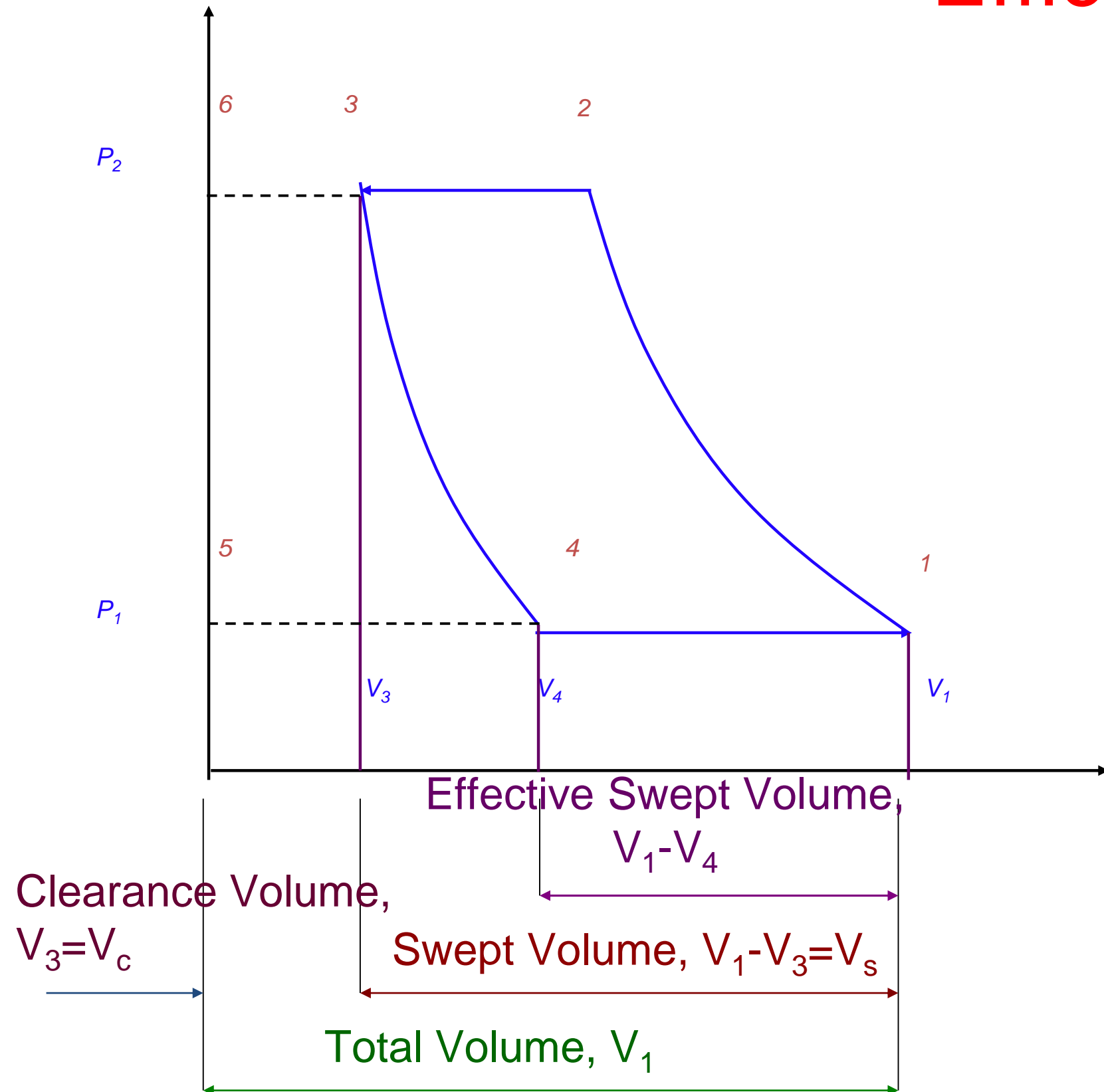
⇒ ↓ Volumetric Efficiency



$$\begin{aligned}
 \eta_{vol} &= \frac{V_1 - V_4}{V_1 - V_3} \\
 &= \frac{(V_1 - V_3) + (V_3 - V_4)}{(V_1 - V_3)} = 1 + \frac{V_3}{(V_1 - V_3)} - \frac{V_4}{(V_1 - V_3)} \\
 &= 1 + \frac{V_3}{(V_1 - V_3)} - \frac{V_4}{(V_1 - V_3)} \cdot \frac{V_3}{V_3} \\
 &= 1 + \frac{V_3}{(V_1 - V_3)} - \frac{V_3}{(V_1 - V_3)} \cdot \frac{V_4}{V_3}
 \end{aligned}$$



# Reciprocating Compressor – Volumetric Efficiency



$$\eta_{vol} = 1 + \frac{V_3}{V_1 - V_3} \left( 1 - \frac{V_3}{V_4} \right)$$

$$\eta_{vol} = 1 - \frac{V_3}{V_1 - V_3} \left( \frac{V_3}{V_4} - 1 \right)$$

$$\eta_{vol} = 1 - \frac{V_3}{V_1 - V_3} \left( \left( \frac{P_3}{P_4} \right)^{1/n} - 1 \right)$$

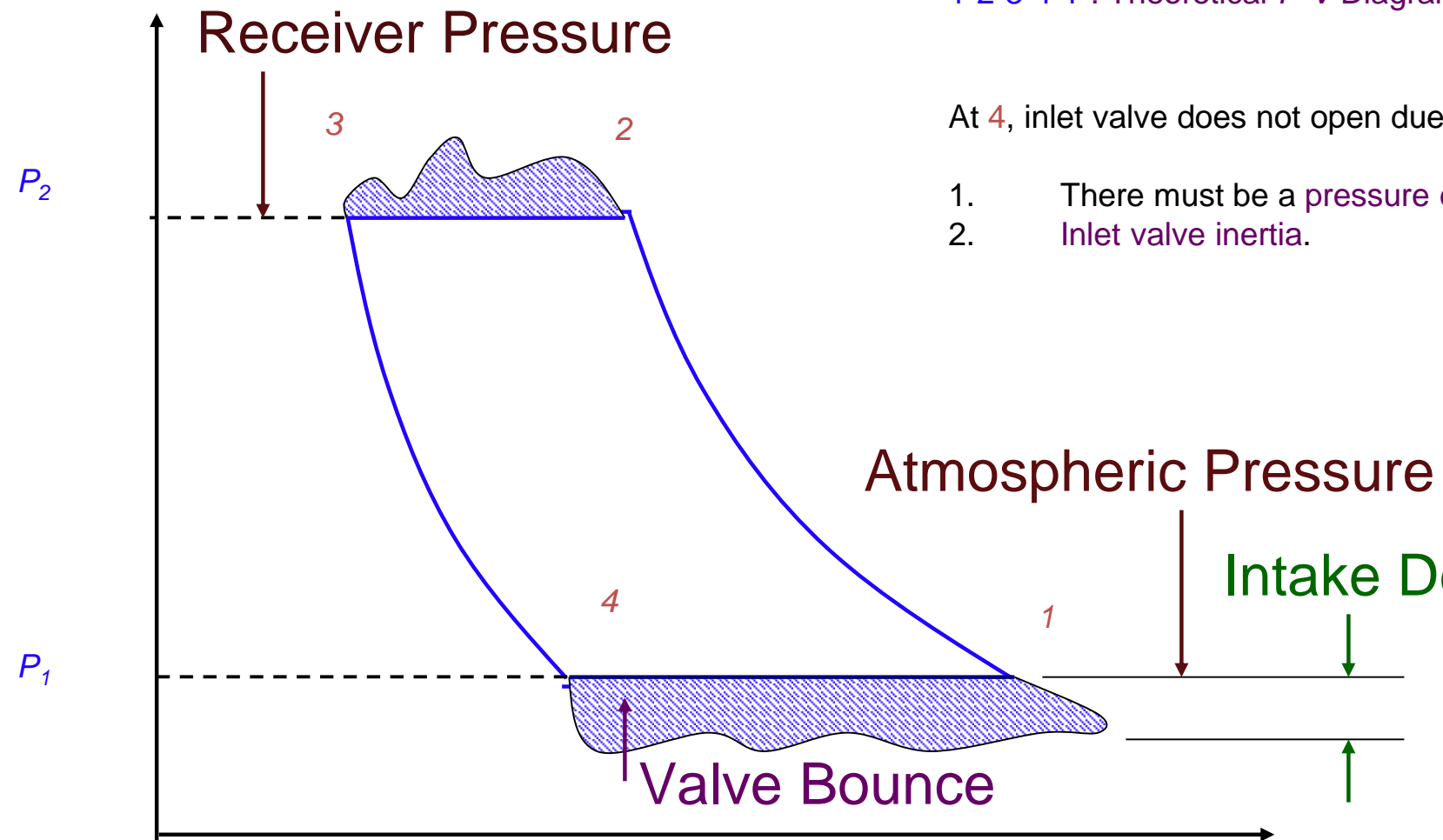
$$\eta_{vol} = 1 - \gamma \cdot \left( \left( \frac{P_3}{P_4} \right)^{1/n} - 1 \right)$$



# Reciprocating Compressor – Actual $P$ - $V$ Diagram



1-2-3-4-1 : Theoretical  $P$ - $V$  Diagram.



At 4, inlet valve does not open due to :

1. There must be a pressure difference across the valve to open.
2. Inlet valve inertia.

Pr. Drop continues till sufficient level for valve to force its seat.

Some valve bounce is set (wavy line).

Eventually, the pressure sets down at a level *lower than* atmospheric pressure. This negative pressure difference is known as *Intake Depression*.

Similar situation appears at 2, i.e. at the start of the delivery.

Pressure rise, followed by valve bounce and then pressure settles at a level *higher than* the delivery pressure level.

Air delivery to a tank / receiver, hence, generally known as *Receiver Pressure*.