

# SNS COLLEGE OF TECHNOLOGY



# Liquid Rocket Propulsion

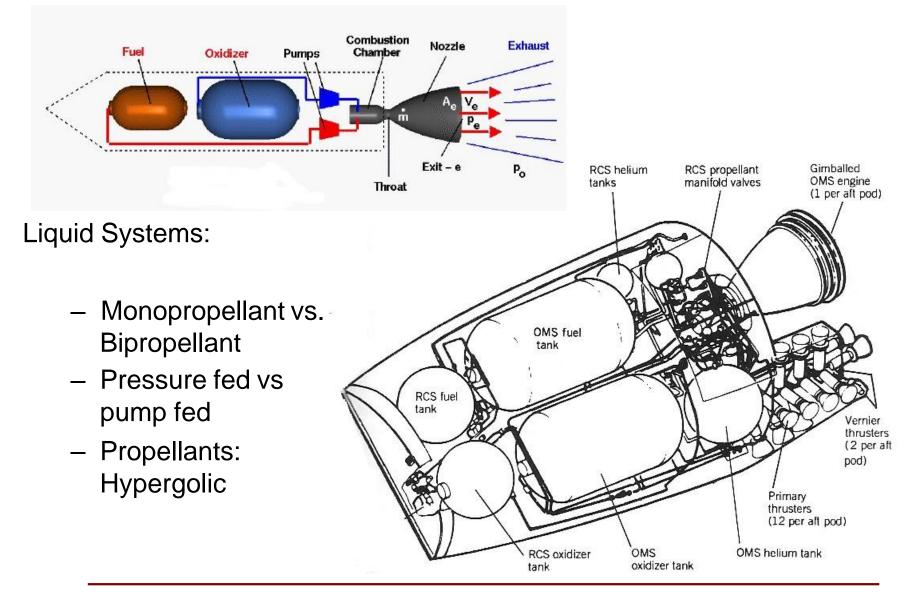
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Courtesy : Stanford University KOC University

Activate Windows

### Liquid Rocket Schematic



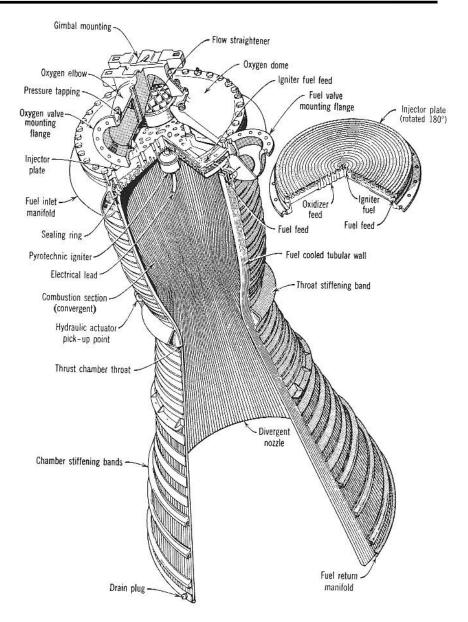
#### Liquid Rocket Types –Based on Propellants

- Monopropellant systems:
  - Single liquid, simpler system
  - Decompose over a catalyst bed
  - Low Isp performance
  - H2O2, hydrazine, N2O
  - Used in satellite propulsion, RCS
- Cryogenic Engines
  - LOX/LH2
  - Expensive, but very high lsp
  - Upper states
- LOX/Kerosene
  - Decent Isp and density
  - Hard to stabilize
  - A lot of launch vehicles use LOX/Kerosene engines
- Storable
  - NTO/Hydrazine or derivative
  - Toxic, not favored in modern systems

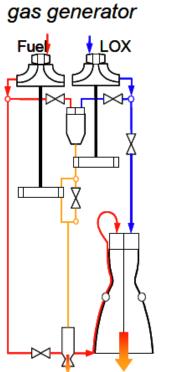
- LOX/Methane
  - Up and coming technology
  - Good compromise between kerosene and H2

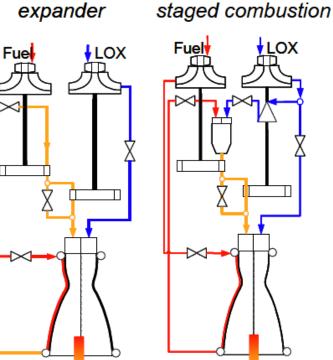
### Liquid Rocket Thrust Chamber

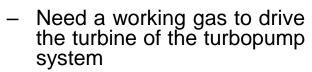
- Thrust chamber includes
  - Injector
  - Combustion chamber
  - Nozzle
  - Ignition system
- Introduce the oxidizer and fuel in liquid or gaseous phase
- Control the mass flow rate of oxidizer and fuel
- Vaporize mix and react the components
- Expel though the nozzle



### Pump Fed Liquid Rocket Cycle Types







- Vaporize the propellant to drive the turbine by
  - Combustion (very lean or very rich to limit temperature)
  - Use the fuel from regenerative cooling
- Turbine inlet temperature is typically around 800-850 K
- Staged combustion cycle is more efficient than the gas generator cycle (older systems such as F1 use the gas generation cycle).

LOX

- Fuel rich pre burners are easier to develop but not as desirable as the oxidizer rich burners
  - Soot deposit on turbine blades
  - Much more oxidizer than fuel (O/F >1)
- Only LOX rich staged combustion systems are Russian engines
- LOX/H2 systems typically utilize fuel rich pre burners

### Liquid Rocket Engines

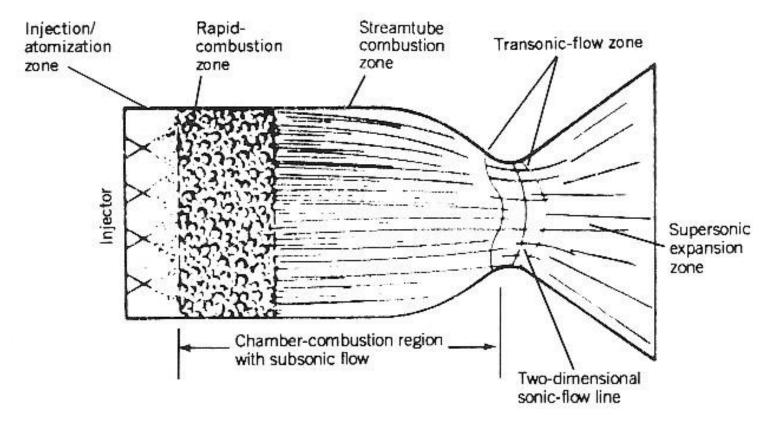
Engine	Thrust, klb	lsp, sec	Propellants	Design Year
F-1	1,500	265	LOX/RP-1	1959
(Saturn V- First Stage)	(SL)	(SL)		
J-2	230	425	LOX/H2	1960
(Saturn V-Upper stages)	(vac)	(vac)		
RS-27A	200	255	LOX/RP-1	1987
(Old Delta Booster)	(SL)	(SL)		
MA-5A	430	265	LOX/RP-1	1988
(Old Atlas Booster)	(SL)	(SL)		
SSME (RS-24)	512	453	LOX/H2	1972
(Space Shuttle Main Engine)	(vac)	(vac)		
SE-10	Max 10.5	305	N2O4/N2H4+	1963
(Lunar Module Descent)	(vac)	(vac)	UDMH	
RD-180	900	311	LOX/Kerosene	Late 1970's
(Atlas V Booster)	(SL)	(SL)		

### A High Performance Engine: RD-180

- High performance LOX/kerosene engine
- Built and marketed by RD AMROSS
  - 50% NPO Energomash (Russian)
  - 50% Pratt and Whitney (US)
- Derived from the Russian engine RD-170 (developed for the Energia/Buran system)
- Used in Atlas III and Atlas V launchers
- Staged combustion cycle Oxidizer rich pre burner
- Vacuum Isp: 337.8 sec
- Nozzle expansion ratio: 36.4
- Chamber pressure: 257 atm
- O/F: 2.71
- Thrust: 0.9 Mlbf
- Throttling range: 47% to 100%



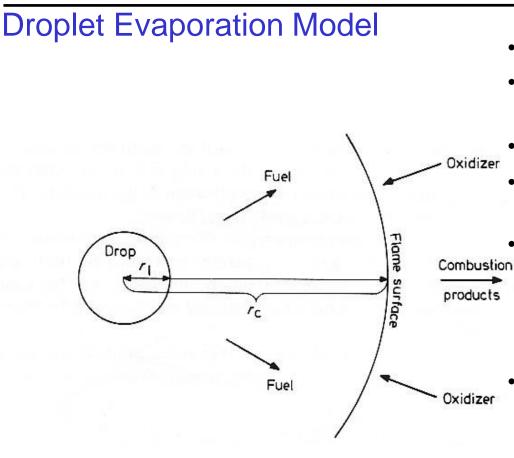
#### Liquid Rocket Combustion



- Monopropellant vs Bipropellant
- Low Residency Times: <10 msec</li>
- High Volumetric Heat Release: 370 Mega-Watt/m<sup>3</sup>

#### Liquid Rocket Combustion

- Combustion Zones:
  - Injection Atomization Zone:
    - Heterogeneous mixture (liquid/gas)
    - Low velocities
    - Relatively cool
    - Main process evaporation of the droplets
  - Rapid Combustion Zone:
    - Intensive fast combustion reactions
    - Large increase in velocity (due to gas/liquid volume increase)
    - Combustion is an inherently unsteady process (small explosions)
  - Stream Tube Combustion Zone:
    - High gas velocity, small residence time
    - Combustion reactions at a slow rate
    - Stream tubes are formed
    - Limited transport across the stream tubes
- Boundaries between zones are fuzzy
- Combustion models and design tools are incomplete



• See "Combustion" by I. Glassman for a rigorous derivation

- Diffusion flame
- Transport through molecular diffusion + convection
- Diffusion flame, O/F stoichiometric
- Evaporation of a burning droplet in quiescent environment
- D<sup>2</sup> law for droplet evaporation

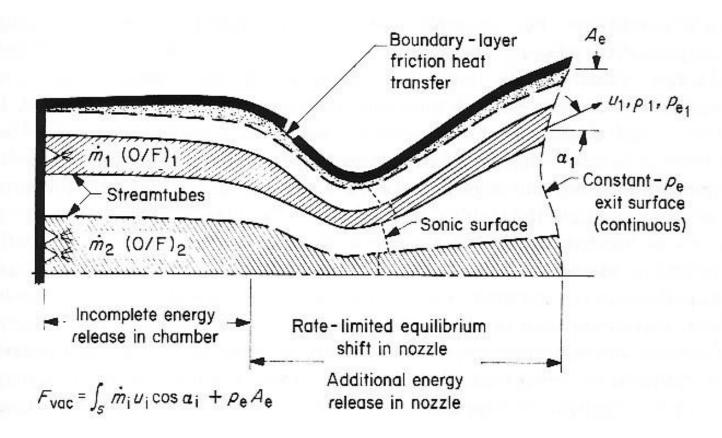
$$\frac{dD^2}{dt} = -K = -\frac{8\lambda}{C_p \rho} \ln(1+B)$$

The Spalding number is

$$B = \frac{1}{h_{v}} \left[ C_{p} \left( T_{\infty} - T_{l} \right) + \frac{Q_{r} Y_{ox,\infty}}{\left( O/F \right)_{stoic}} \right]$$

 As a first order approximation droplet surface temperature can be taken as the boiling temperature

#### Liquid Rocket Combustion-Stream Tube Model



- One dimensional model
- Different steam tubes could be at different O/F ratios. Introduces a loss
- Boundary layer heat transfer can be modeled by this model

#### Liquid Engine Design Issues

- Must consider performance, stability and compatibility simultaneously
- Performance (Isp):
  - Theoretical value (for a given average O/F)
  - Losses:
    - Thermal (heat transfer)
    - Combustion efficiency (mixing/kinetics)
    - Nonuniform propellant distribution (mixing)
    - Boundary layer (friction)
    - Geometry (nozzle divergence)
    - Particle lag (two phase flow)
  - The Isp efficiencies of the modern engines are fairly high: 95-98
    %
  - Operational conditions are critical
    - Low pressures: Kinetics
    - · Low Thrusts: Boundary layer
    - Small Volume: Low combustion efficiency

#### Liquid Engine Design Issues

- Stability:
  - Liquid engine combustion is an inherently unstable process
  - Metastable (minimize the amplitude of the fluctuations)
  - Stability fixes:
    - Chemical
    - Aerodynamic
    - Mechanical
- Compatibility
  - Environmental components
    - Thermal (Heat Transfer)
    - Chemical (Reactions)
    - Gas dynamic (Erosion)

### Liquid Engine Design Issues

- Control Variables:
  - Feed system dynamics
  - Injector design, injector pressure drop
  - Combustion chamber geometry
    - Combustion chamber volume, Vc (includes the convergent part of the nozzle). Define L\*

$$L^* = V_c / A_t$$

• Residence time in the chamber is

$$\tau = L^* / c^*$$

- Efficiency increases with L\*. More time for atomization, vaporization, mixing and reacting
- For typical liquid systems L\* ranges 0.8-3 meters
- Baffles
- Absorption cavities
- Propellant additive selection (i.e. Hypergolic propellants)

### Liquid Engine Design Issues

- Combustion chamber and nozzle walls must be cooled
  - Regenerative cooling
    - Cooling jacket, some of the heat is used to warm the fuel
  - Ablative cooling
    - Carbon graphite, phenolic
  - Film cooling
    - Injector face cooling
  - Radiation cooling
    - Used in small engines and monopropellant systems
    - Niobium, Rhenium coated Inconel
  - Combination
- As the combustion chamber size reduces
  - Heating intensity increases
  - Surface area decreases
- Nozzle throat has the maximum heat transfer
- Total pressure loss in the chamber
  - Ac/At must be high to minimize the total pressure loss

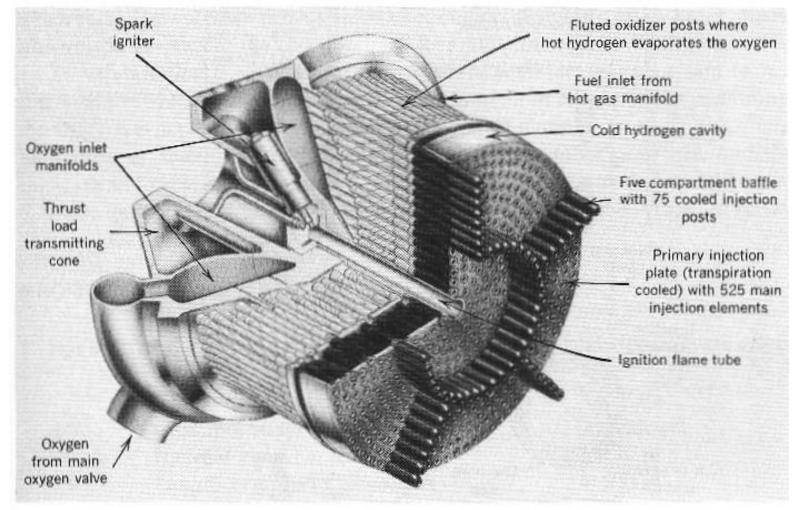
### Liquid Engine Injector Design

- Injector design is critical for stable and efficient operation
  - Meter the oxidizer and fuel flow rates
  - Atomize the liquids
- Types
  - Impinging stream: doublet, triplet, self impinging
  - Shower head (V2 rocket injector)
  - Hollow post sleeve element
  - Splash plate
  - Pintle
- Flow rate expression

$$nh = C_d A_i \sqrt{2\rho_l \Delta P}$$

- Typically Cd varies from 0.60 to 0.84 (0.61 for square edge orifice)
- Large injector pressure drop is important for stability and efficiency
  - Increasing Delta P increases the tank weight or pump requirements
- Momentum matching for the oxidizer and fuel streams. Makes the throttling more difficult

#### Liquid Rocket Injector Design - SSME Injector



Liquid rocket injectors are very complex devices

## Liquid Rockets Summary

#### Summary

- Complicated design
- Expensive manufacturing
  - Exotic materials
  - Complex parts with tight tolerance requirements
- Very good Isp performance
- Multiple liquids in the system
- Fire hazard
- Mature technology

#### Challenges

- Cost effective systems
- LOX/RP-1: Oxygen rich pre-burner
- Replacement for hydrazine and its derivatives