

Unit II Internal Combustion Engine

I.C Engine :-

Combustion of fuel take place inside the cylinder that engine called as I.C Engine

Heat Engine :-

Any engine that Converts the heat energy released due to Combustion of fuel into useful Mechanical work is Known as heat engine.

It has two type

- (1) External Combustion engine
- (2) Internal Combustion engine

E.C Engine :

External Combustion engines, the Combustion of fuel take place outside the cylinder.

The fuel is not mixed with air in external Combustion engine

Classification :-

(1) No. of stroke

2. stroke

4 - stroke

(2) According to the thermodynamic

Otto

Diesel

Duel

Brayton

Ignition :- i Spark Ignition  
ii Compression Ignition

Fuel :- Petrol diesel gas

Speed :- Slow Speed, Medium Speed, High Speed

Cylinder :- Inline engine Radial Engine, Opposed engine<sup>(cylinder)</sup>  
V-engines Rotary Engine, Delta engine  
Opposed Piston engine Vertical horizontal Engine.

Cooling :- Air Cooled, Water Cooled

Fuel Injection :- Carburettor engines, Air Injection Engines  
Airless or Solid Injection engines.

No. of Cylinder :- Single Cylinder Multi Cylinder

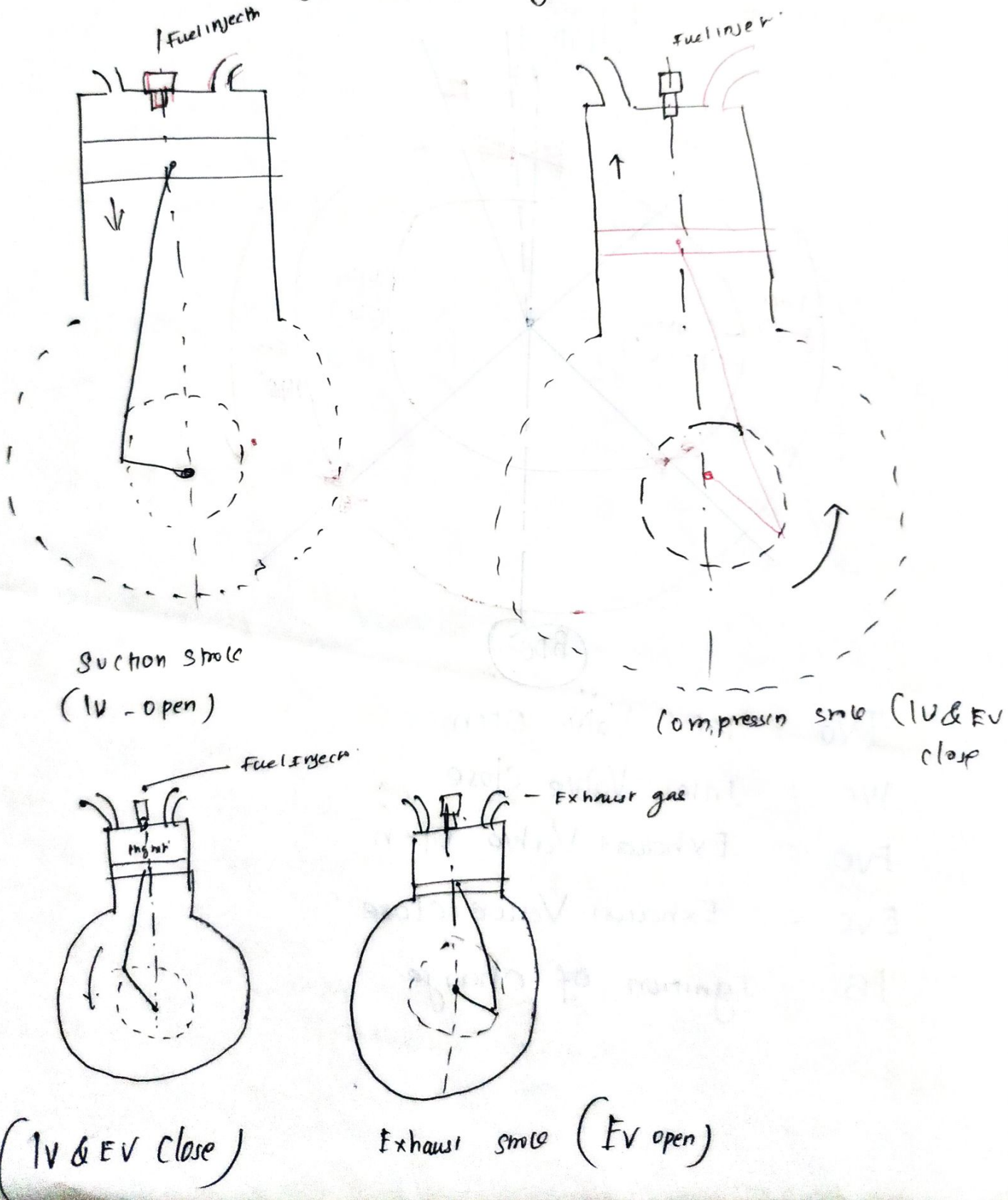
Governing :- Hit and Miss governed engine  
Quality Governed Engines  
Quantity Governed Engines

Valve :- Over head Valve, Side Valve, L-head Valve  
T-head type h-head type

Application :- Stationary, Automobile, Locomotive  
Aero, Marine

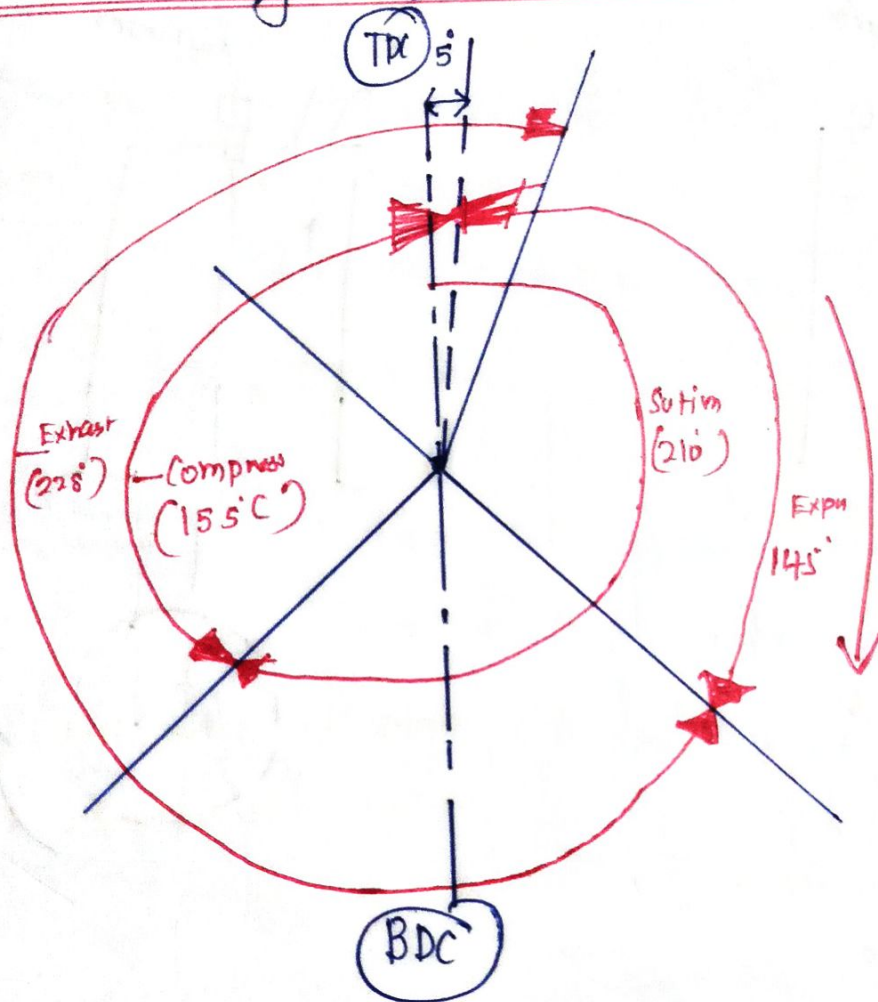
# Four stroke Engine [Diesel]

Diesel engines are also known as Compression Ignition engine as Combustion takes place due to high pressure and temperature generated during Compression stroke.



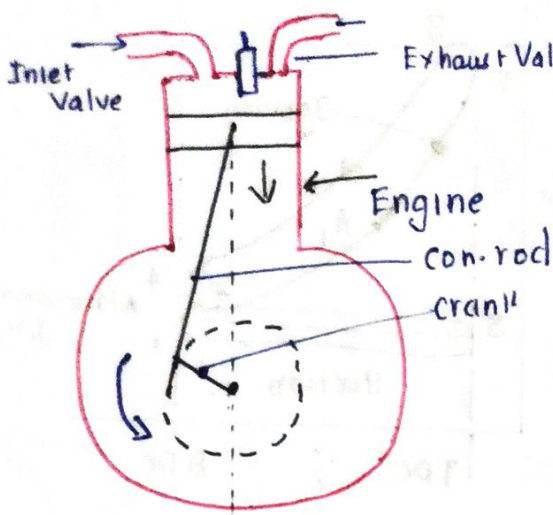
- 5-1 Suction stroke
- 1-2 Compression Stroke
- 3-4 Expansion stroke
- 1-6 Exhaust stroke
- 2-3 Instantaneous Combustion & 4-1 Sudden fall in Pressure

Valve Timing Diagram for 4-stroke Petrol engine

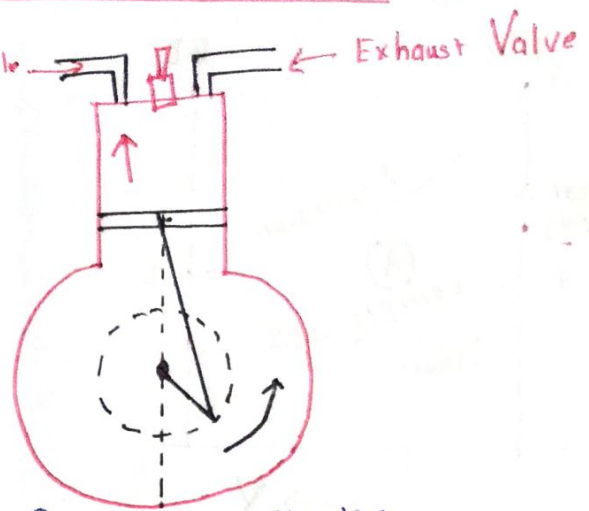


- IVO = Inlet Valve Open
- IVC = Inlet Valve Close
- EVO = Exhaust Valve Open
- EVC = Exhaust Valve Close
- IG = Ignition of charge

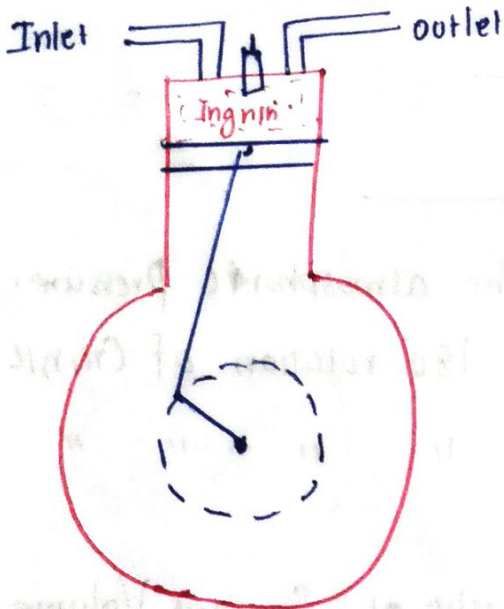
# Four Stroke engine [Petrol]



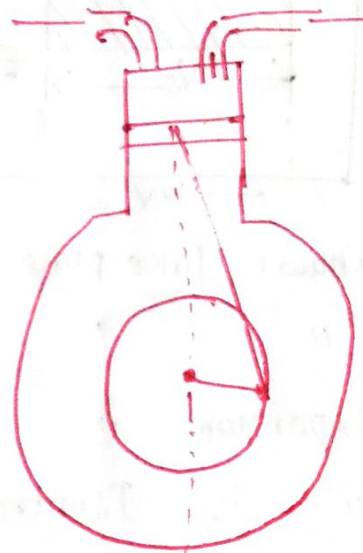
Suction stroke  
(Inlet Valve open)



Compression stroke  
[In. V & Ex. Val closed]

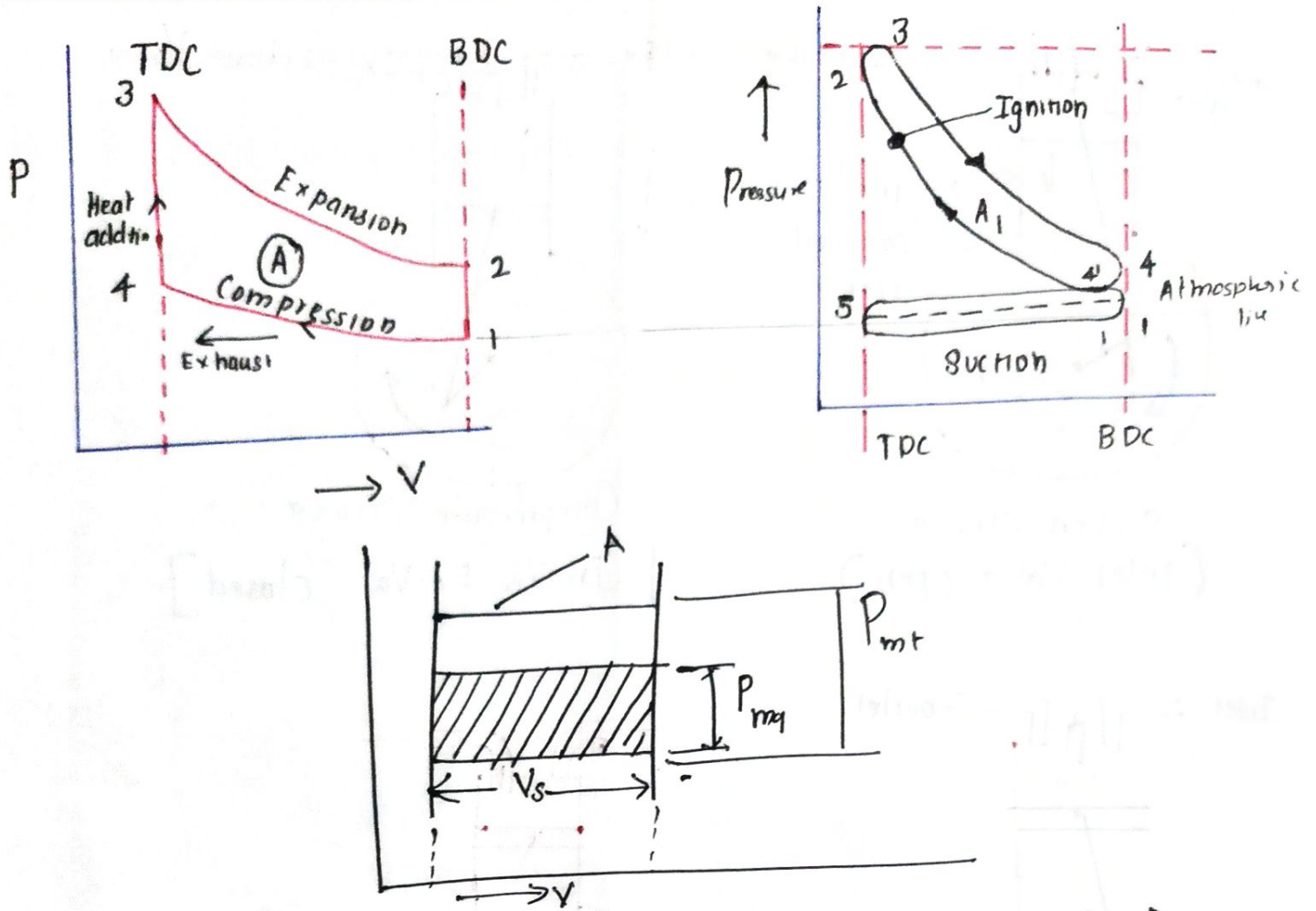


(Knocking stroke)



Exhaust stroke  
outlet Valve open

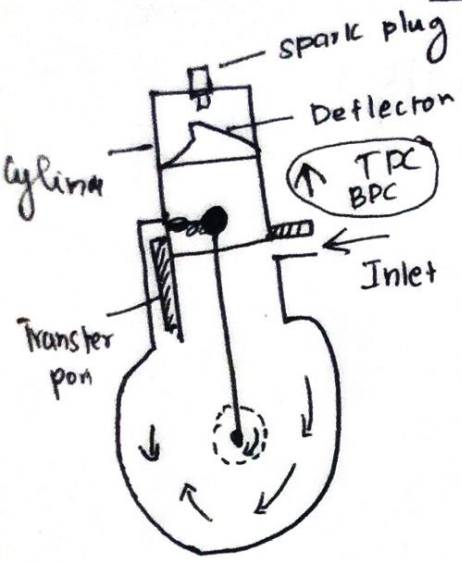
# Theoretical and actual PV diagrams



1. The suction & Exhaust take place outside the atmospheric pressure.
2. " " " " through 180° rotation of Crank
3. Compression & Expansion " " " " " "
4. " " " Isentropic
5. The Combustion take place instantaneously at Constant Volume at the end of Compression stroke.
6. The inlet Valve closes beyond the state [after combustion begins]
7. The Pressure suddenly fall to atmosphere at the end of expansion stroke.
8. Sudden pressure rises after ignition is not possible. The pressure increases after some crank rotation or increase in volume.
9. Exhaust Valve open little before the end of the expansion stroke.
10. Burned gas can be pushed out into atmosphere only if the pressure of Exhaust gas is above atmospheric level.

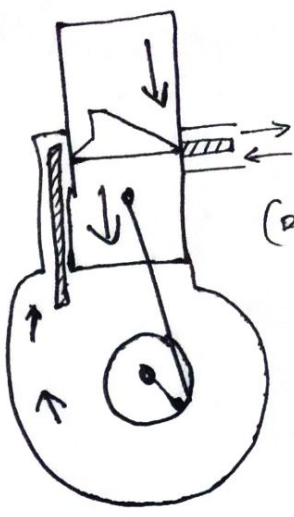
2 Stroke petrol

(1) Suction:-



(a)  
Suction

- piston move TDC to BDC
- Inlet port closed.
- transfer port & Exhaust port open
- Fresh air & fuel enter into cylinder



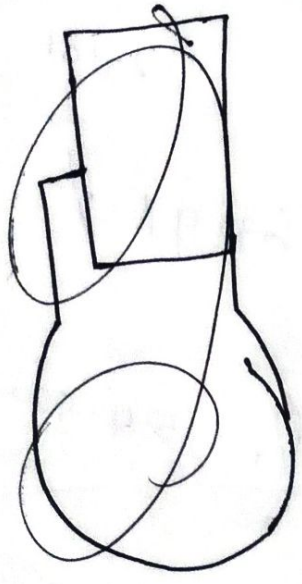
(b)  
both are closed condition

(2) Compression stage:-

- piston move BDC to TDC
- Fresh fuel & air enter into crank case
- close transfer port & Exhaust port.
- After air fuel mixture is compressed piston move upwards
- Pre & temp increased at end of compression

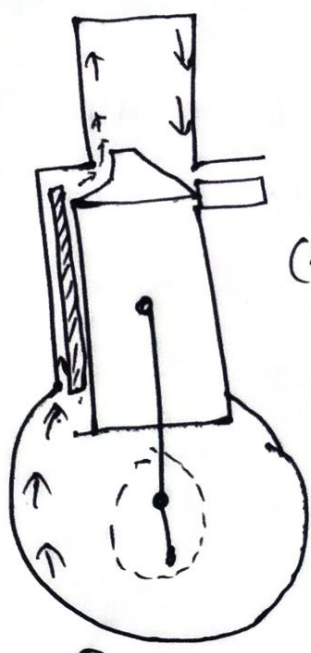
(3) Expansion stage:-

- charge is ignited with help of spark plug
- piston pushed downwards with high force
- hot burnt gases expand due to high speed of piston

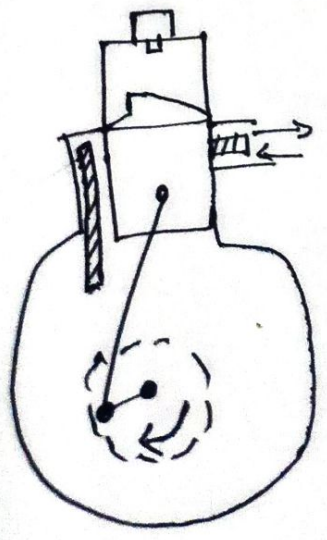


(A) Exhaust stage:-

- Exhaust port is opened as the piston move downwards.
- Burnt gases go out side when port is open
- Complete the cycle and start ready a suction stroke.



(c)  
Transfer port open  
Exhaust port open  
Suction port close.



(d)  
Both are closed

$$\eta_{bth} = \frac{3600}{0.2387 \times 43000}$$

(43 MJ/kg)

$$\boxed{\eta_{bth} \quad 35.069\%}$$

Relative efficiency:

$$\eta_r = \frac{\eta_{bth}}{\eta_{air}}$$

$$\eta_{air} = 1 - \frac{1}{(\gamma_r)^{\gamma-1}} \quad V_s = \frac{\pi d^2 \times l}{4}$$

$$\frac{\pi}{4} 100^2 \times 12 = 942.478 \text{ cm}^3$$

$$\gamma_r = \frac{V_s + V_c}{V_c} = \frac{942.478 + 80}{80} = 12.781$$

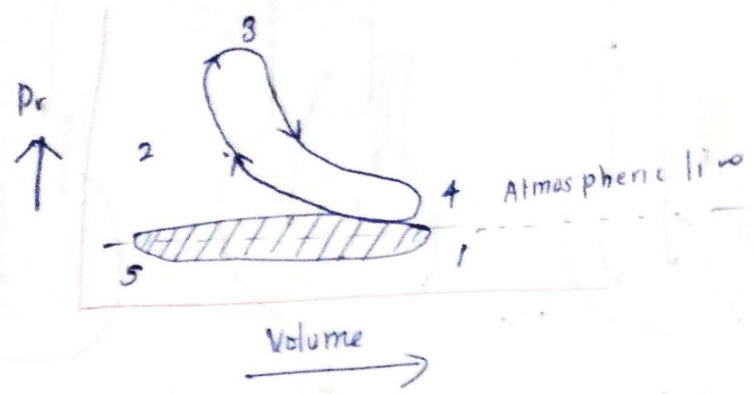
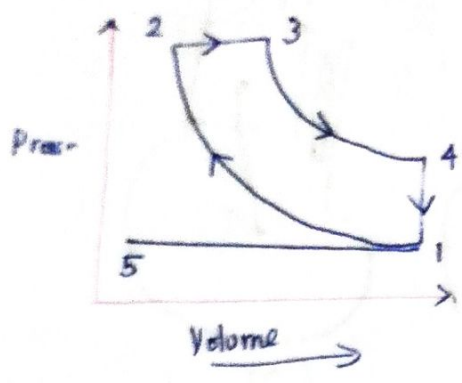
$$\eta_{air} = 1 - \frac{1}{(12.781)^{1.4-1}} = 63.91\%$$

$$\eta_r = \frac{0.35069}{0.63911}$$

$$\boxed{\eta_r = 54.872\%}$$

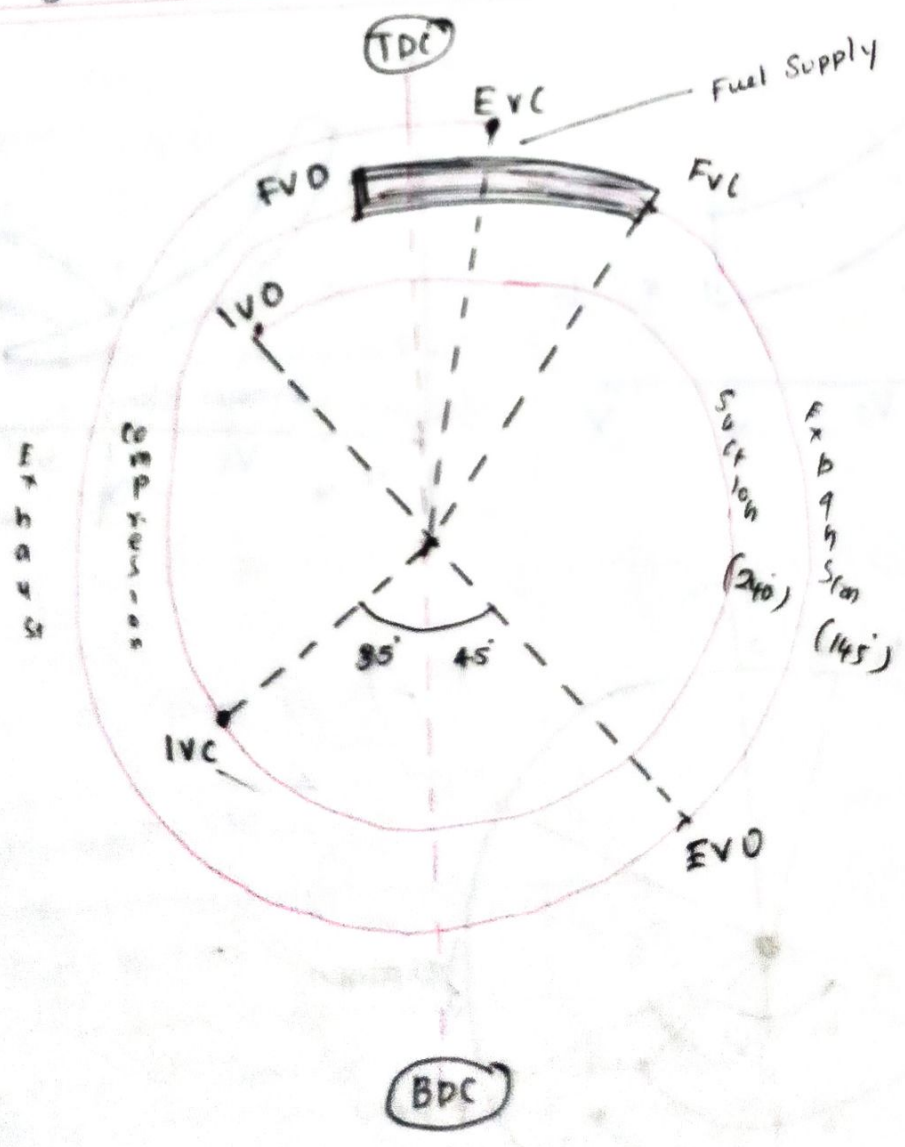


Theoretical and actual P.V diagram

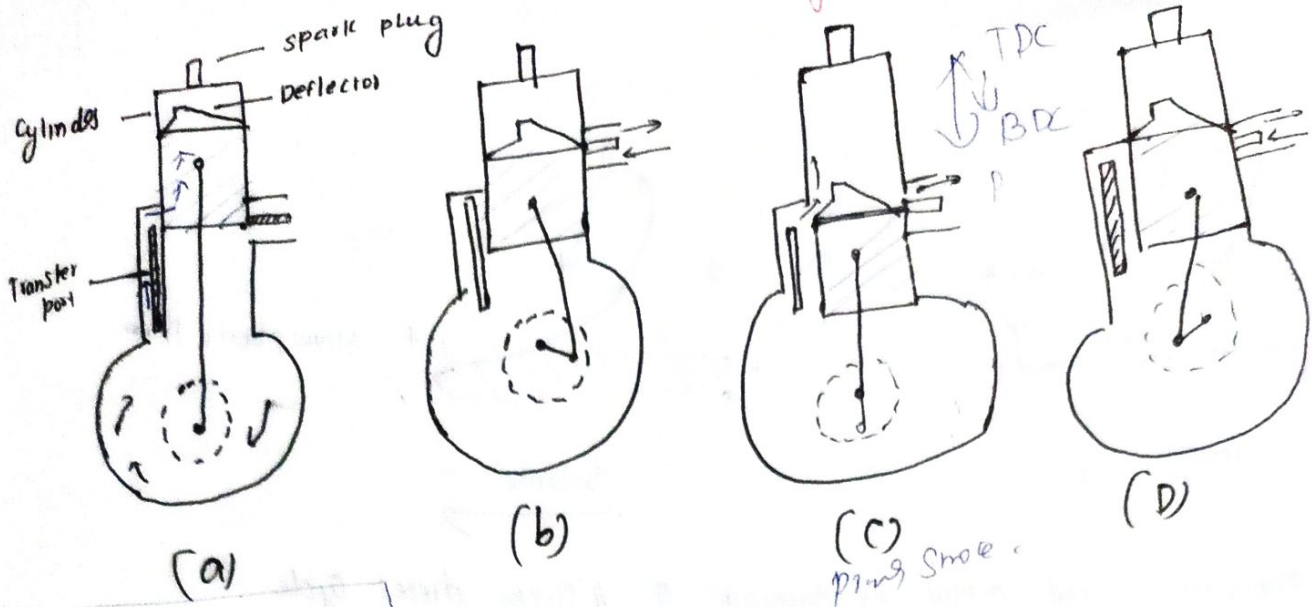


Theoretical and actual P.V diagram of 4 stroke diesel cycle

Valve timing diagram of four stroke diesel engine



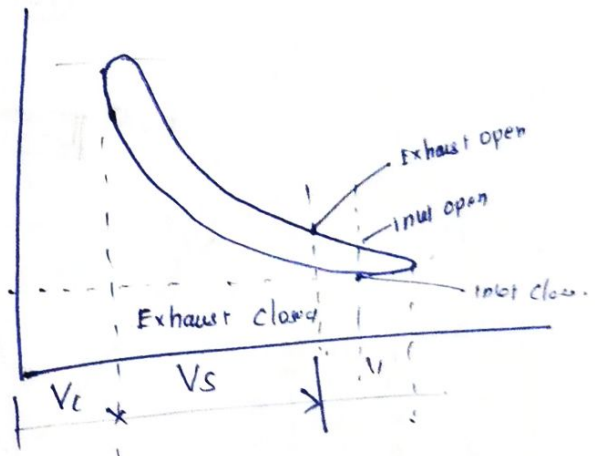
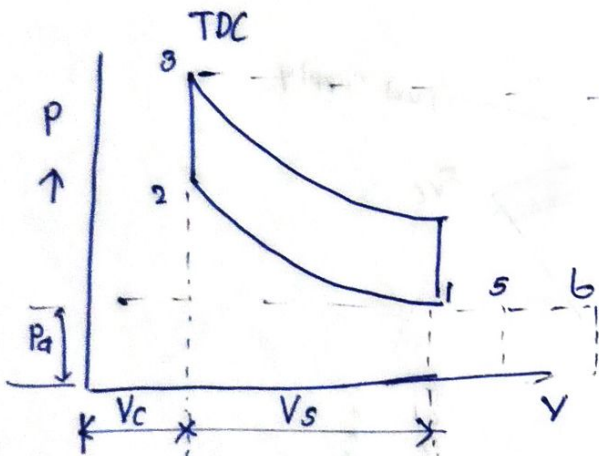
## Two stroke petrol engine



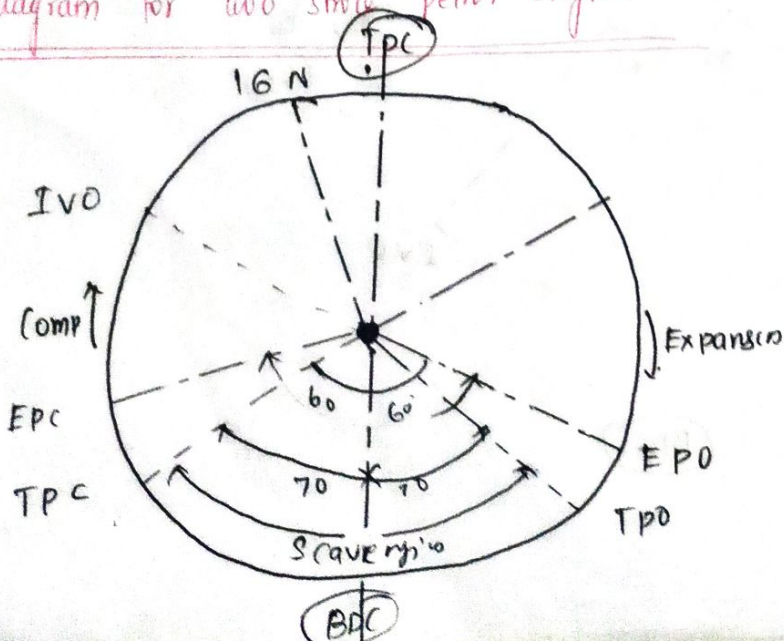
1/2 rotation of Crank & compress - completed.

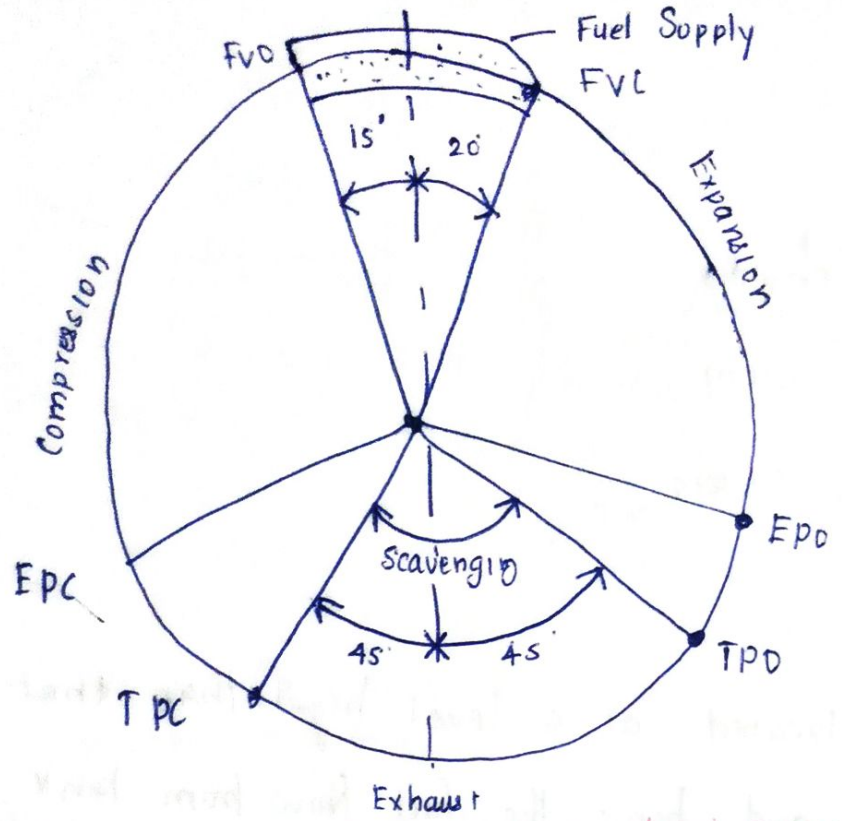
Working of two stroke petrol engine.

Theoretical and actual P-v diagram:



Port diagram for two stroke petrol engine





Port timing diagram for two stroke diesel Engine

Two Stroke	Four stroke
Thermodynamic cycle completed in two stroke of the piston or in one revolution of the crank	two revolution of the crank
Turning moment is more uniform and hence light flywheel can be used	non uniform and hence heavier flywheel is needed
Engine is easier to start	Engine is difficult to start
High rate of wear & tear	Low rate of wear & tear
Low Volumetric efficiency	High Volumetric efficiency
Initial cost is low	High
Maintenance is simple	difficult

## Fuel Supply System

### Fuel System in SI Engines:

- (i) Gravity system
- (ii) Pressure system

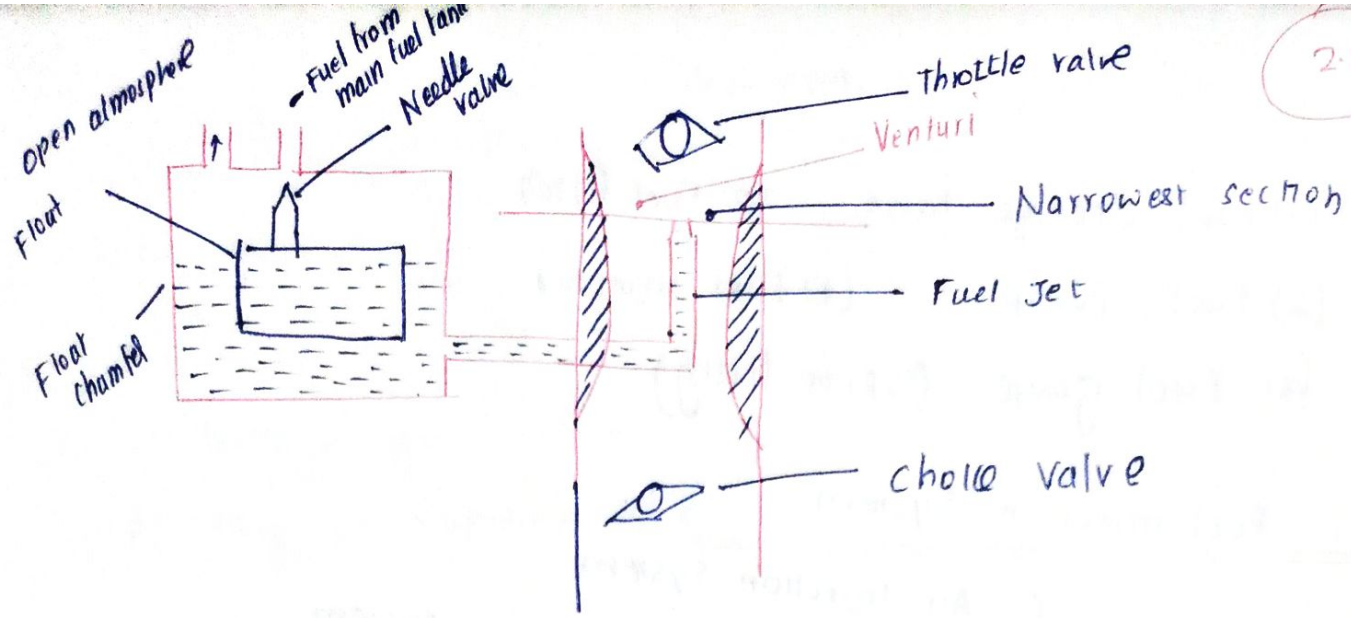
#### Gravity System:-

• fuel tank is located at a level higher than that of the engine cylinder and hence the fuel flow from tank to engine cylinder under gravitational force.

#### Pressure System:-

tank is located below the engine cylinder and hence, the fuel is forced or pumped from tank to engine cylinder by means of external source such as feed pump

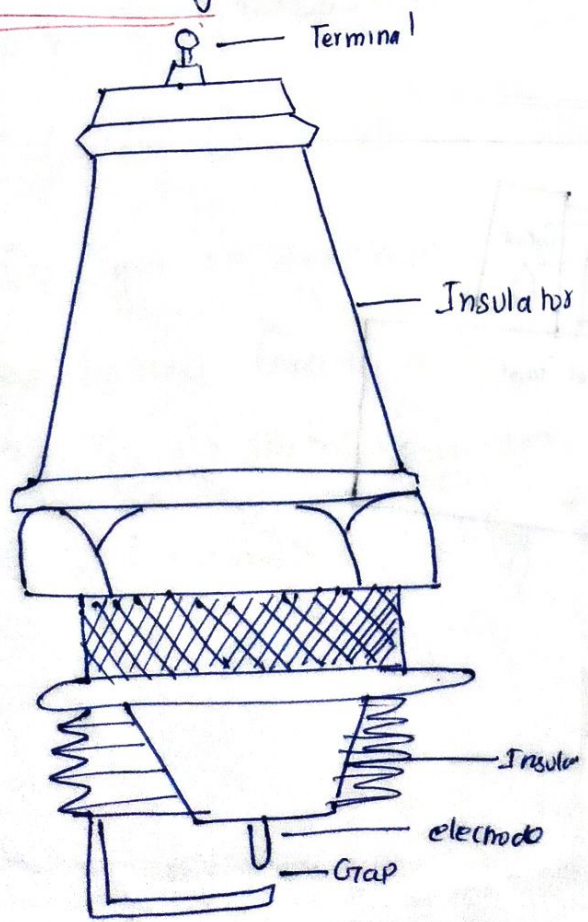
- |                       |                     |
|-----------------------|---------------------|
| (a) Fuel storage tank | (d) Carburettor     |
| (b) Fuel Pump         | (e) inlet Manifold. |
| (c) Fuel filter       |                     |



Simple Carburettor

- (1) Float and Float chamber
- (2) Venturi
- (3) Throttle Valve
- (4) choke Valve
- (5) Fuel Nozzle

Spark plug:

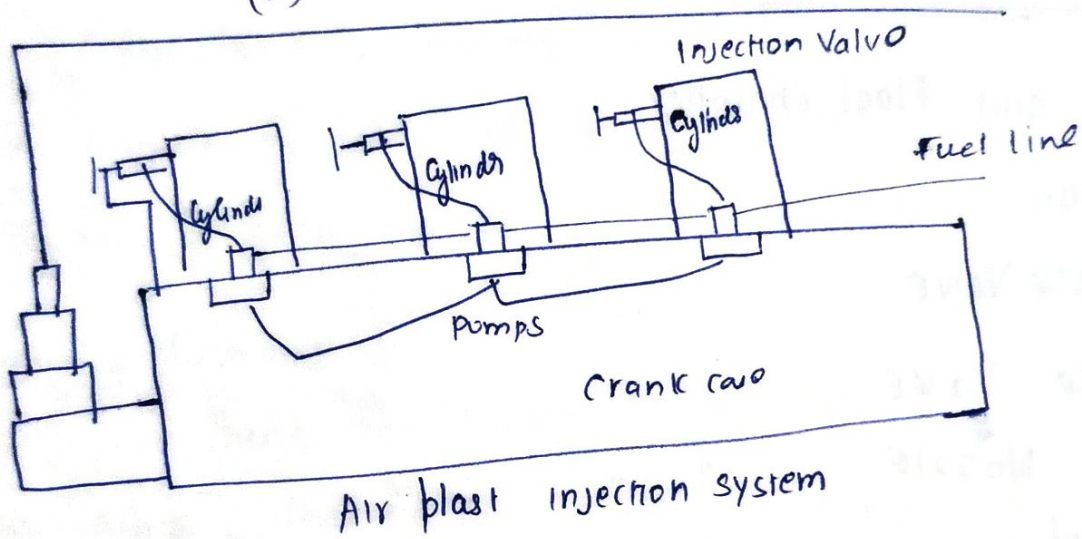


## Fuel Supply in C.I engines:

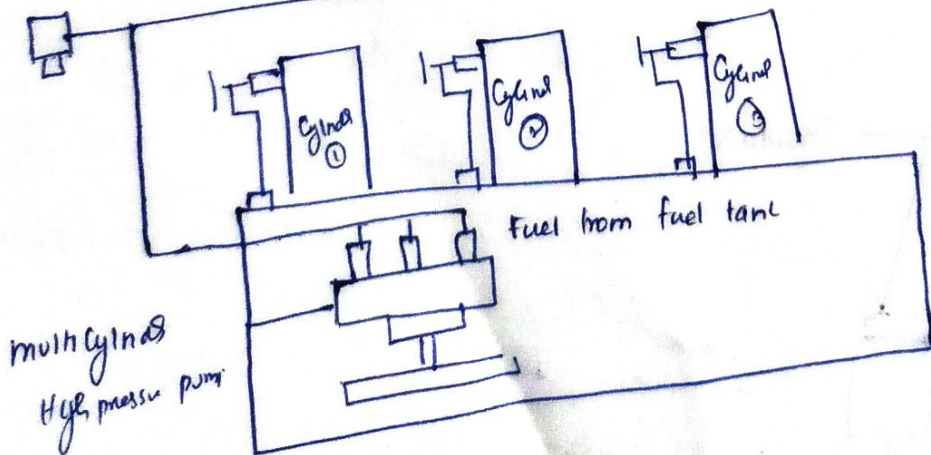
- (1) Fuel Storage tank
- (2) Fuel filter
- (3) Fuel Pump
- (4) Fuel injector
- (5) Fuel gauge
- (6) Pipe fitting

## Fuel Injection System

- (1) Air Injection System
- (2) Airless or solid injection system



## Common rail system



## Component of Solid fuel Injection System:-

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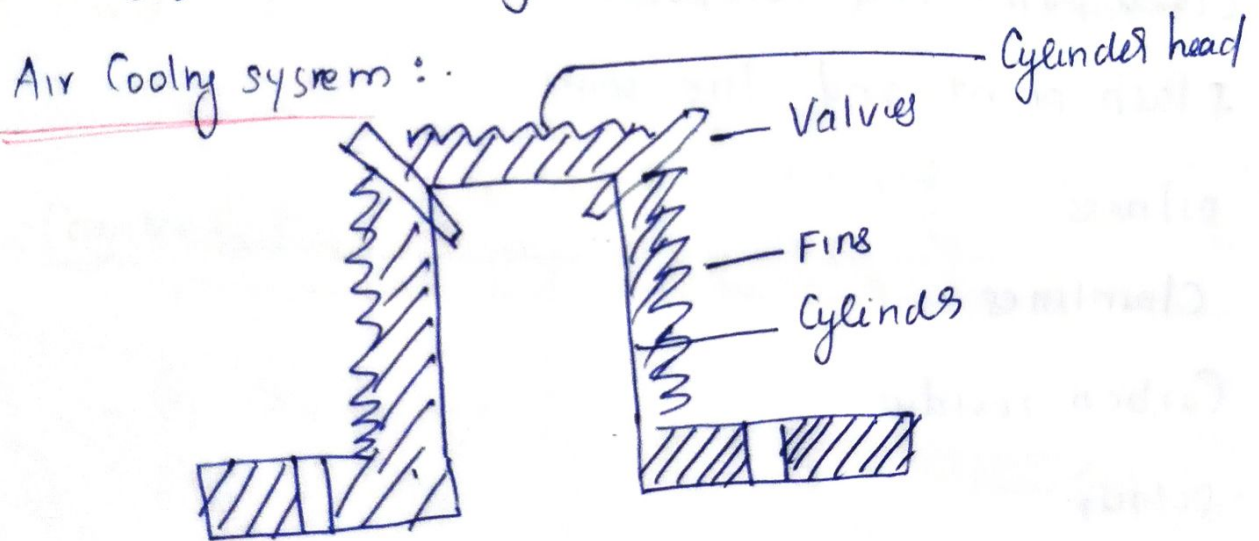
- (i) Fuel pump
- (ii) Fuel atomiser or injector

## Ignition System:

- (i) Battery Ignition System
- (ii) Magneto Ignition System

## Cooling system:-

- (i) Air Cooling system
- (ii) Water Cooling system



## Water Cooling system:-

- (1) Thermo siphon System
- (2) Forced Circulation
- (3) Thermo static regulator system
- (4) Evaporative cooling system

## Lubricating System :-

- Lubrication is the admittance of oil b/w two surfaces having relative motion.
- Lubrication is required to reduce the wear of the parts earlier and to carry out the part of the heat generated inside the engine.

## Properties of lubrication oil :

1. Viscosity
2. Viscosity index
3. Cloud point and Pour point
4. Flash point and fire point
5. Oiliness
6. Cleanliness
7. Carbon residue
8. Colour

## Types of lubrication System :

- (1) Wet sump lubrication
- (2) Dry sump lubrication
- (3) Mist lubrication

## Fuels :-

The Performance of an I.C engine is satisfactory only when the properties of fuel used is good and hence the fundamental knowledge of type of fuel and their characteristics is essential.



## Requirements of fuel:

2.8

1. High energy density
2. Easy to handle and store
3. High thermal stability
4. Low toxicity
5. Easy Availability
6. Low deposit forming tendency
7. Good Combustion Quality

## Types of fuel:

- (i) Gaseous fuel
- (ii) Liquid fuel

## Knocking and detonation:

### Combustion stages in S.I engine

- (1) Delay period
- (2) Combustion
- (3) burning

### Factors affecting the ignition lag:

- (1) ~~ignition~~ initial pressure & temp
- (2) Compression ratio
- (3) Speed or turbulence of the engine
- (4) Chemical nature of fuel A:F ratio

### Combustion stage in C.I engine:

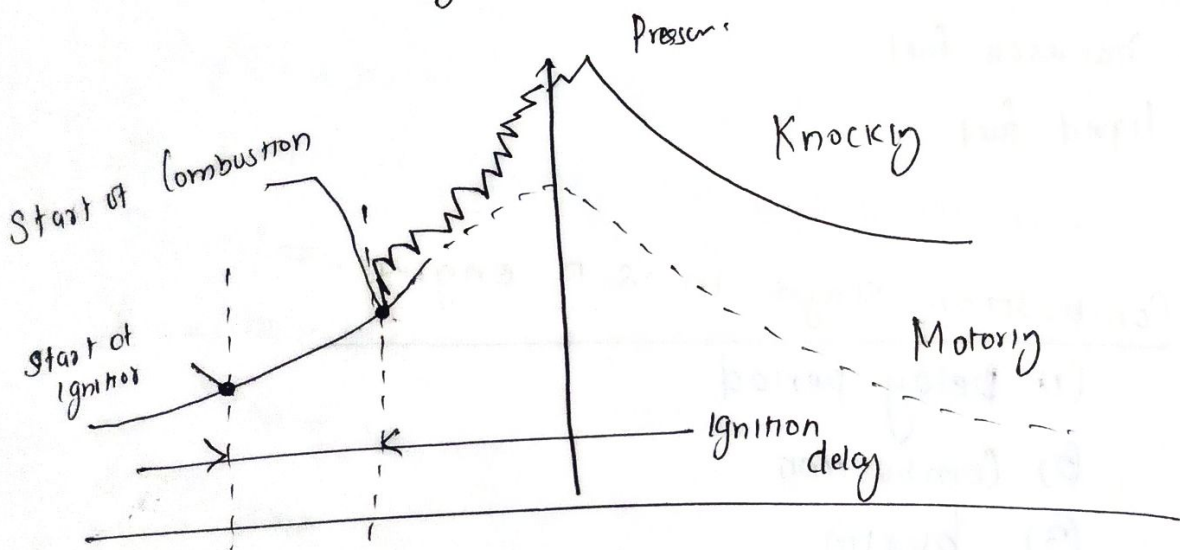
- (i) Ignition delay period
- (ii) Rapid or uncontrolled Combustion period
- (iii) Controlled Combustion period
- (iv) burn

## Diesel knock:

In Compression ignition engine Compression Combustion Process leads to Smooth Pressure rise.

• For abnormal Combustion, the ignition delay Period of the fuel is quite long.

• When ignition begins, the fuel start burning and can cause high rapid rate of Pressure rise.



## Air fuel ratio Calculations:

$$u_1 + P_1 V_1 + \frac{C_1^2}{2} + Q = u_2 + P_2 V_2 + \frac{C_2^2}{2} + W + u_2 - (1)$$

$$h = u + PV \quad (2)$$

From (1) & (2)

$$h_1 + \frac{C_1^2}{2} + Q = h_2 + \frac{C_2^2}{2} + W$$

Assuming adiabatic flow, we have

$Q=0$  and initial velocity at the Nozzle  $h_1 P C_1=0$

$$\therefore C_2^2 = 2 (h_1 - h_2) \quad \text{--- (3)}$$

$$C_2 = \sqrt{2 (h_1 - h_2)}$$

We know that

$$h = C_p T$$

$$\therefore h_1 - h_2 = C_p (T_1 - T_2) \quad \text{--- (4)}$$

For isentropic flow

$$\frac{T_2}{T_1} = \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}}$$

$$T_2 = T_1 \left[ \frac{P_2}{P_1} \right]^{\gamma-1/\gamma}$$

Sub (5) in (4) we get

$$h_1 - h_2 = C_p T_1 \left[ 1 - \left[ \frac{P_2}{P_1} \right]^{\frac{\gamma-1}{\gamma}} \right] \quad \text{--- (6)}$$

Sub (6) in (3) we get

$$C_2 = \sqrt{2 C_p T_1 \left[ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \right]}$$

Hence the above equation becomes

$$C_2 = \sqrt{\frac{2\gamma}{\gamma-1} R T_1 \left[ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \right]} \quad \left[ \because C_p = \frac{\gamma R}{\gamma-1} \right]$$

Theoretical Mass flow of air

$$m_a = \rho A C_2 = P_2 A_2 C_2$$

We know that

The theoretical Mass flow rate of air

$$m_a = \rho_1 A_1 C_1 = \rho_2 A_2 C_2 \quad \text{--- (8)}$$

$A_1$  &  $A_2$  - Cross sectional area of inlet & Venturi throat

For isentropic law

$$P_1 V_1^\gamma = P_2 V_2^\gamma$$

$$\frac{P_1}{\rho_1^\gamma} = \frac{P_2}{\rho_2^\gamma}$$

$$\frac{P_2}{\rho_2^\gamma} = \frac{P_1}{\rho_1^\gamma}$$

$$P_2 = P_1 \left( \frac{P_2}{P_1} \right)^{1/\gamma} \quad \text{--- (9)}$$

From equation 7 & 9

$$m_a = \rho_1 \left( \frac{P_2}{P_1} \right)^{1/\gamma} A_2 \left[ \frac{2\gamma}{\gamma-1} RT_1 \left[ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \right] \right]$$

$$= \frac{\rho_1}{RT_1} \left[ \frac{P_2}{P_1} \right]^{1/\gamma} A_2 \left[ \frac{2\gamma}{\gamma-1} RT_1 \left[ 1 - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \right] \right]$$

$$= A_2 \cdot \frac{\rho_1}{RT_1} \left[ \frac{2\gamma}{\gamma-1} P_1 \left[ \left( \frac{P_2}{P_1} \right)^{2/\gamma} - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma+1}{\gamma}} \right] \right]$$

$$m_a = A_2 \cdot \frac{\rho_1}{\sqrt{RT_1}} \left[ \frac{2\gamma}{\gamma-1} P_1 \left[ \left( \frac{P_2}{P_1} \right)^{2/\gamma} - \left( \frac{P_2}{P_1} \right)^{\frac{\gamma+1}{\gamma}} \right] \right] \quad \text{--- (10)}$$

We know that air  $\gamma = 1.4$  &  $R = 0.287 \text{ kJ/kg}^\circ\text{C}$

2.10

$$\therefore m_a = A_2 \frac{P_1}{0.287 \times 10^3 \times T_1} \left[ \frac{2 \times 1.4}{1.4 - 1} \left[ \left( \frac{P_2}{P_1} \right)^{2/1.4} - \left( \frac{P_2}{P_1} \right)^{\frac{1.4+1}{1.4}} \right] \right]$$

$$A_2 = \frac{P_1}{16.94 \sqrt{T_1}} \left[ 7 \left[ \left( \frac{P_2}{P_1} \right)^{1.43} - \left( \frac{P_2}{P_1} \right)^{1.72} \right] \right]$$

$$A_2 = \frac{7 \cdot P_1}{16.94 \sqrt{T_1}} \left[ \left( \frac{P_2}{P_1} \right)^{1.43} - \left( \frac{P_2}{P_1} \right)^{1.72} \right]$$

$$m_a = 0.1562 A_2 \frac{P_1}{\sqrt{T_1}} \left[ \left( \frac{P_2}{P_1} \right)^{1.43} - \left( \frac{P_2}{P_1} \right)^{1.72} \right]$$

$$\phi = \frac{A \cdot A}{\sqrt{T_1}} = \phi \frac{P_1}{\sqrt{T_1}} \times 0.1562 A_2 \dots (11)$$

$$\phi = \left[ \left( \frac{P_2}{P_1} \right)^{1.4} - \left( \frac{P_2}{P_1} \right)^{1.72} \right]$$

$\phi$  = Pressure in  $\text{N/m}^2$

$A$  = area in  $\text{m}^2$

$T$  = temperature in  $\text{K}$

The actual mass flow rate is

$$m_{act} = C_d \times 0.1562 A_2 \frac{P_1}{\sqrt{T_1}} \phi$$

$$m_{act} \propto \frac{P_1}{\sqrt{T_1}} \phi$$

Theoretical Mass flow rate of fuel is

$$m_f = \rho_f A_f C_f \quad \text{--- (13)}$$

Applying Bernoulli's equation for section 1-1 & 2-2

$$\frac{P_1}{\rho_f} - \frac{P_2}{\rho_f} = \frac{C_f^2}{2} + 2g$$

$\rho_f$  and  $C_f$  are the density and Velocity fuel respectively

$$\therefore C_f^2 = 2 \left[ \frac{(P_1 - P_2)}{\rho_f} - 2g \right]$$

$$C_f = \sqrt{2 \left[ \frac{(P_1 - P_2)}{\rho_f} - 2g \right]}$$

$$m_f = \rho_f A_f \sqrt{2 \left[ \frac{(P_1 - P_2)}{\rho_f} - 2g \right]} = A_f \sqrt{2 \rho_f^2 \left[ \frac{P_1 - P_2}{\rho_f} - 2g \right]}$$

$$m_f = 1.414 A_f \sqrt{\rho_f^2 \left[ \frac{P_1 - P_2}{\rho_f} - 2g \right]}$$

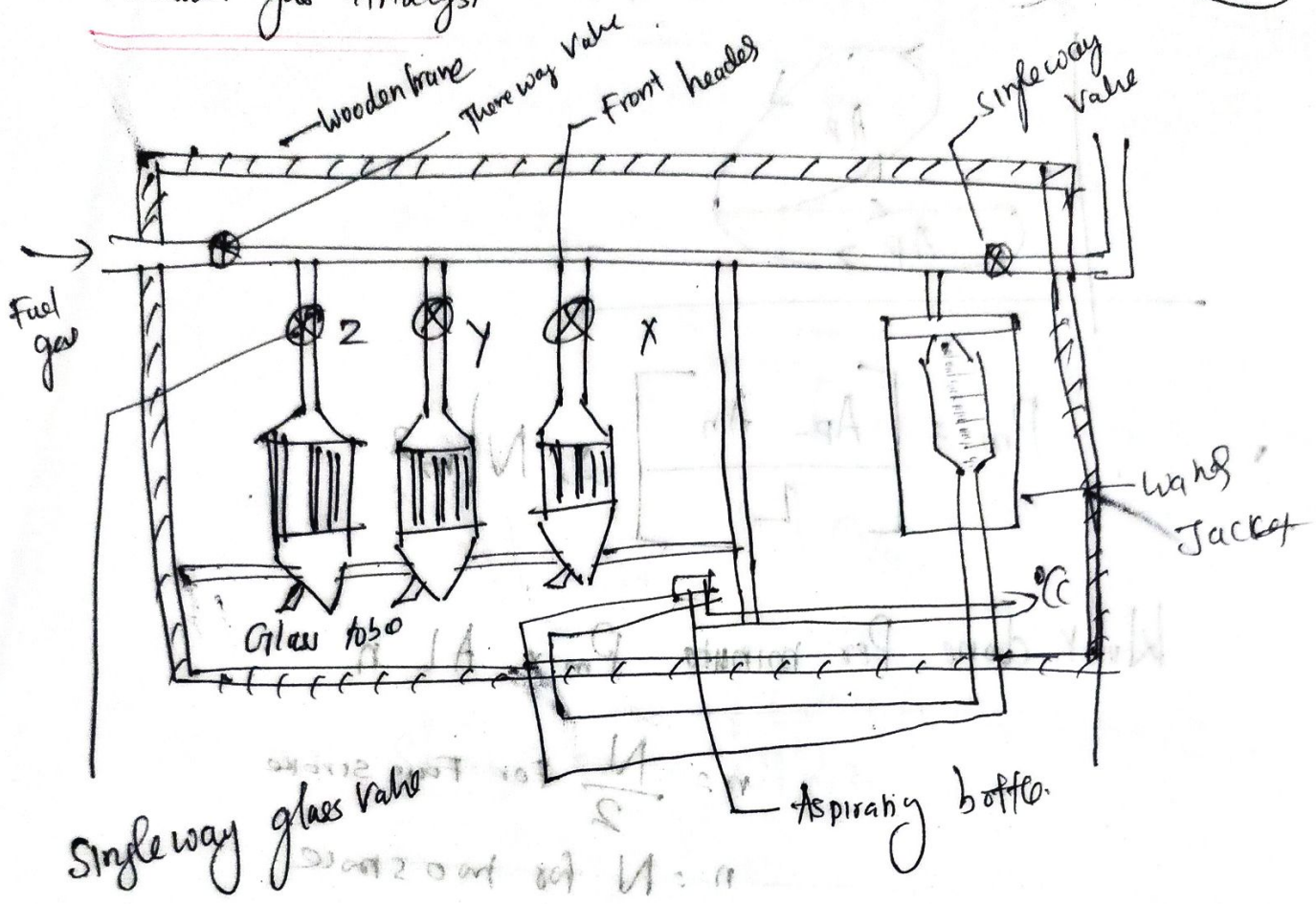
$$m_f = 1.414 A_f \sqrt{\rho_f (P_1 - P_2) - 2g \rho_f} \quad \text{--- (14)}$$

The actual Mass flow rate

$$C_d \times 1.414 A_f \sqrt{\rho_f (P_1 - P_2) - 2g \rho_f}$$

$$1.414 \frac{A_f}{\sqrt{\pi}}$$

Exhaust gas Analysis



Performance Calculation

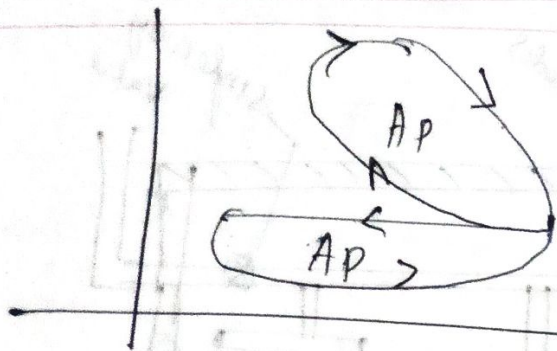
Power developed by various Method listed below

- (1) Indicated Power
- (2) Brake power
- (3) BMEP
- (4) Friction Power (F.P)

IP =

$$IP = \frac{K P_m L A n}{60} \text{ KW}$$

18/10/2017 Derivation of Indicated Power :



$$P_m = \frac{A_p - A_n}{L} \times N \text{ m}^2$$

Work done Per minute  $P_m \times A L n$

$n = \frac{N}{2}$  For Four stroke

$n = N$  for two stroke

I.P.K =  $\frac{K P_m A L N}{60}$  KW

Indicated Power (I.P.) is the power developed by the gas in the cylinder.

(1) Indicated Power (I.P.)

(2) Brake Power (B.P.)

(3) B.M.E.P.

$I.P. = \frac{K P_m A L N}{60}$  KW



$$A:F = \frac{m_{act}}{m_{theor}} = 0.1562 A_2 C_{d2} \frac{P_1}{\sqrt{T_1}} \sqrt{\rho_1} \quad (2.12)$$

$$1.414 A_1 C_{d1} \sqrt{P_1 (P_1 - P_2) - 2g P_1 f}$$

$$0.11 \frac{A_2}{A_1} \frac{C_{d2}}{C_{d1}} P_1 \left[ \left( \frac{P_2}{P_1} \right)^{1.43} - \left( \frac{P_2}{P_1} \right)^{1.72} \right]$$

$$\sqrt{T_1} \sqrt{P_1 (P_1 - P_2) - 2g P_1 f}$$

$$A:F = 0.11 \frac{A_2}{A_1} \frac{C_{d2}}{C_{d1}} P_1 \left[ \left( \frac{P_2}{P_1} \right)^{1.43} - \left( \frac{P_2}{P_1} \right)^{1.72} \right]$$

$$\text{Pressure should be in } \frac{N}{m^2} \sqrt{(P_1 (P_1 - P_2) - 2g P_1 f) T_1}$$

### Morse test

For all cylinders operative

$$(B.P)_n = (I.P)_n - (F.P)_n$$

When one cylinder is inoperative

$$(B.P)_{n-1} = (I.P)_{n-1} - (F.P)_{n-1}$$

$$(B.P)_n - (B.P)_{n-1} = (I.P)_n - (I.P)_{n-1} = (I.P)_n$$

B.P = Brake power

I.P = Indicated power

F.P = friction power.

## Brake Power (B.P)

$$B.P = \frac{2\pi NT}{60 \times 1000} \text{ Kw}$$

N - Engine Speed in rpm      T - Torque in N-m

## Measurement of Brake power :

- (1) Rope brake dynamometer
- (2) Prony brake dynamometer
- (3) Hydraulic dynamometer

## IMEP

$$P_m = \frac{\text{Work done per Cycle}}{\text{Stroke Volume}}$$

## IMEP

(1) Equivalent rectangular Method

Mid ordinate Method

Plain meter Measurement

## Measurement of fuel Consumption :

$$\text{Fuel Consumption} = \frac{V \times \rho_{\text{fuel}}}{t}, \text{ Kg/sec}$$

Where t - time taken, sec

# Measurement of Air Consumption:

2.13

## Head of Air

$$h_a \times \rho_a = h_w \times \rho_w$$

$$h_a = h_w \times \frac{\rho_w}{\rho_a} \quad \text{m}$$

$$h_a = \frac{1000 h_w}{\rho_a} \quad \text{in m}$$

## Velocity of Air Passing through the orifice

$$C_a = \sqrt{2gh_a} = \sqrt{2 \times 9.81 \times \frac{1000 h_w}{\rho_a}}$$

$$C_a = \sqrt{19620 \frac{h_w}{\rho_a}} \quad \text{in m/sec}$$

## Mass flow rate of air

$$m = C_d \rho_a A C_a = \rho_a \frac{\pi}{4} d^2 \times C_d \times \sqrt{19620 \frac{h_w}{\rho_a}}$$

$$m = \frac{\pi}{4} d^2 \times C_d \times \sqrt{19620 h_w \rho_a}$$

$$m = 110.026 d^2 \times C_d \times \sqrt{h_w \rho_a}$$

$$m = 6.5 \times d^2 \times C_d \times \sqrt{h_w \frac{\rho_a}{\rho_a}}$$

# Various efficiency of an engine

## 1. Mechanical efficiency

$$\eta_m = \frac{B.P}{I.P} = \frac{B.P}{B.P + F.P}$$

## 2. Over all efficiency

$$\eta_o = \frac{B.P \times 3600}{m_f \times C.V}$$

## 3. Brake thermal efficiency

$$\eta_{br} = \frac{B.P \times 3600}{m_f \times C.V}$$

## 4. Indicated thermal efficiency

$$\eta_{it} = \frac{I.P \times 3600}{m_f \times C.V}$$

## 5. Relative efficiency

$$\eta_{rel} = \frac{\eta_{it}}{\eta_{air}}$$

## 6. Volumetric efficiency

$$\eta_v = \frac{V_a}{V_s}$$

Where :-

Unit II formula

$A_p$  - Area of Positive loop,  $m^2$

$A_n$  - Area of Negative loop,  $m^2$

$L$  - Length of the Indicator diagram,  $m$

$s$  - Spring scale  $N/m^2/m$

Force on the piston  $P_m \times A$ ,  $KN$

$P_m$  - m.e.p  $KPa$  (or)  $KN/m^2$

$A$  = Cross sectional area of piston,  $m^2$

Work done per stroke =  $P_m \times A \times L$

$L$  = length of stroke

Work done per minute =  $P_m \times A \times L \times n$

$n = \frac{N}{2}$  for Four stroke engine

$n = N$  for Two stroke engine

Work done per second =  $\frac{P_m \times A \times L \times n}{60}$

Indicated Power 'K' cylinders =  $K P_m \frac{A L N}{60}$  kW

B. P' [Brake power]

Boop  $N$  = Engine rpm

$T$  = Torque  $N-m$

$D$  = Dia of flywheel

$d$  = " of rope

$S$  = Spring balance reading

$N$  = rpm of the engine

$T_f$  = frictional Torque

$W$  = Weight

$L$  = length or Stroke.