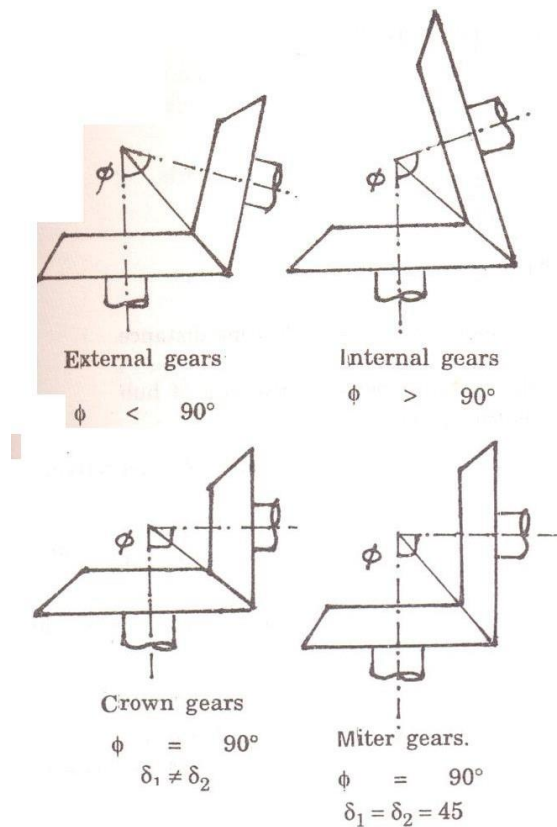


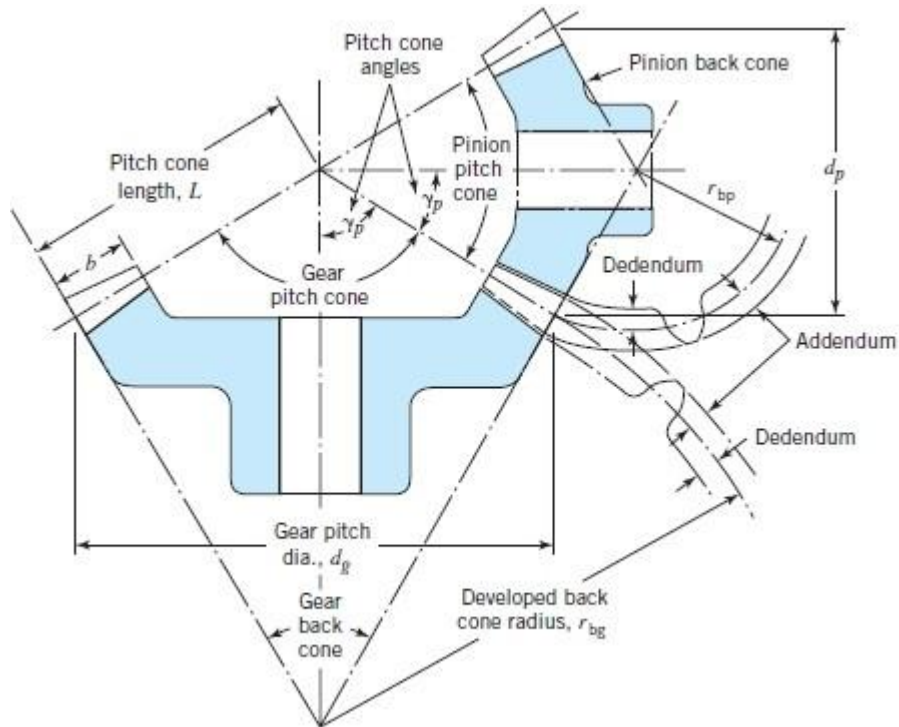
3 BEVEL, WORM AND CROSS HELICAL GEARS

3.1 BEVEL GEAR

Bevel gears are used to transmit power between the shafts whose axes are intersecting at an angle. In bevel gears, teeth are cut on conical surface in contrast with spur and helical gears, for which the teeth are cut on a cylindrical surfaces. The structure of the helical gear is similarly to an uniformly serrated frustum of a cone.



3.1.1 BEVEL GEAR TERMINOLOGY



CLASSIFICATION

1. Based on the shape of teeth such as
 - a. Straight teeth bevel gears
 - b. Curved teeth bevel gears
2. Based on the angle between the shafts
 - a. External gear drive ,if shaft angle $<90^\circ$
 - b. Internal gear drive ,if shaft angle $>90^\circ$
 - c. Mitre gear, if shaft angle = 90°

Example.Design a bevel gear drive to transmit 7 kW at 1600 rpm for the following data

Gear ratio = 3

Material for pinion and gear = C45 Steel

Life = 10,000 hours

Since the pinion and gear are made of same material, pinion is weaker than gear and its teeth are subjected to more number of cycles.

STEP-1-MINIMUM CONE DISTANCE

Minimum cone distance based on surface compressive strength

$$\geq \sqrt[3]{\sqrt{2+1} \left\{ \frac{0.72}{((-0.5) [])} \right\}^2 \frac{[]}{3}} \quad \text{(PSG 8.13)}$$

Design torque $[M_t]=M_t.k.k_d$ (PSG 8.15)

$$[M_t] = 97420 \times \frac{7}{1600} \times 1.5 = 640 \text{ kgf-cm ; } k.k_d = 1.5 \text{ (assumed)}$$

Equivalent young's modulus = $2.15 \times 10^6 \text{ kgf/cm}^2$ (PSG 8.14)

$$[\sigma_c] = 5000 \text{ kgf/cm}^2 \quad \text{(PSG 8.5)}$$

 $\psi_y = R/b = 3$ (for $i=3$) (PSG 8.15)

$$\geq 3 \sqrt[3]{\sqrt{2+1} \left\{ \frac{0.72}{(3-0.5)5000} \right\}^2 \frac{2.1510^6 640}{3}} \geq 10.95 \text{ cm}$$

STEP-2-AVERAGE MODULE

$$\geq 1.26 \sqrt[3]{\frac{[]}{[]}} \quad \text{(PSG 8.15)}$$

 $\sigma_b = 1400 \text{ kgf/cm}^2$ (PSG 8.5) $\Psi_m = \text{---} = 10$ (initially assumed) $y_v =$ form factor $z_v = z_1 / \cos \delta_1$ for pinion (PSG 8.39)

$$\tan \delta_2 = i = 3 ; \delta_2 = \tan^{-1} i = \tan^{-1} 3 = 71.66$$

$$\delta_1 = 90 - 71.56 = 18.43^\circ$$

$$z_v = z_1 / \cos \delta_1 = 20 / \cos 18.43 = 21$$

 $y_v = 0.396$ (PSG 8.18)

$$\geq 1.26 \sqrt[3]{\frac{640}{0.39614001020}} = 0.226 \text{ cm} = 2.3 \text{ mm}$$

STEP-3-TRANSVERSE MODULE

$$m_t = m_{av} \frac{3}{(3-0.5)} = 2.3 \times \frac{3}{(3-0.5)} = 2.76 \text{ mm}$$

next standard module = 3 mm = 0.3cm

STEP-4-CORRECTED CONE DISTANCE

$$= 0.51 \sqrt{(2+1)} \quad \text{(PSG 8.38)}$$

$$10.95 = 0.5 \times 0.3 \times z_1 \times \sqrt{(3^2+1)}; z_1 = 23.08 \approx 24$$

$$z_1 = 24 \text{ and } z_2 = i \times z_1 = 3 \times 24 = 72$$

$$\text{Final cone distance } R = 0.50.324 \sqrt{(3^2+1)} = 11.4 \text{ cm}$$

Since the final cone distance is greater than initial distance our design is safe.

STEP-5-FACE WIDTH

$$b = \frac{11.4}{3} = 3.8 \text{ cm} \approx 4 \text{ cm}$$

STEP-6-CHECKING THE INDUCED STRESSES

$$= \frac{0.72}{(-0.5)} \sqrt{\frac{(2+1)^3}{[]}} \quad \text{(PSG 8.13)}$$

$$= \frac{0.72}{(11.4 - 0.54)} \sqrt{\frac{(3^2+1) 3^2.1510^6 640}{34}}$$

$$= 4638 \text{ kgf/cm}^2 < [\sigma_c] = 5000 \text{ kgf/cm}^2$$

Our design is safe.

$$= \frac{\sqrt{(2+1)[]}}{(-0.5^2)} \frac{1}{o} \leq [\sigma_b] \quad \text{(PSG 8.13a)}$$

$$A = 20^\circ \text{ usually} \quad \text{(PSG 8.38)}$$

$$= \frac{11.4 \sqrt{(3^2+1)640}}{(11.4-0.54)^2 40.30.396} \frac{1}{o_{20}} = 591 \text{ kgf/cm}^2 \leq [\sigma_b] = 1400 \text{ kgf/cm}^2$$

STEP-7-PITCH CIRCLE DIAMETER

For pinion $d_1 = m_t z_1 = 3 \times 24 = 72$ mm

For gear $d_2 = m_t z_2 = 3 \times 72 = 216$ mm

STEP-8-TIP CIRCLE DIAMETER

$$d_{a1} = m_t(z_1 + 2\cos\delta_1) = 3(24 + 2\cos 18.43) = 77.7 \approx 78 \text{ mm}$$

(PSG 8.38)

$$d_{a2} = m_t(z_2 + 2\cos\delta_2) = 3(72 + 2\cos 71.56) = 218 \text{ mm}$$

STEP-9-ADDENDUM ANGLE θ_a

$$\theta_{a1} = \theta_{a2} = \tan^{-1}\left(\frac{o}{11.4}\right) = \tan^{-1}\left(\frac{0.31}{11.4}\right) = 1.5^\circ$$

STEP-10-DEDENDUM ANGLE θ_f

$$\theta_{f1} = \theta_{f2} = \tan^{-1}\left(\frac{o^+}{11.4}\right) = \tan^{-1}\left(\frac{0.3(1+0.2)}{11.4}\right) = 1.8^\circ$$

STEP-11-TIP ANGLE

For pinion $\delta_{a1} = \delta_1 + \theta_{a1} = 18.43 + 1.5 = 19.93^\circ$

For gear $\delta_{a2} = \delta_2 + \theta_{a2} = 71.56 + 1.5 = 73.06^\circ$

STEP-12-ROOT ANGLE

For pinion $\delta_{f1} = \delta_1 - \theta_{f1} = 18.43 - 1.5 = 16.63^\circ$

For gear $\delta_{f2} = \delta_2 - \theta_{f2} = 71.56 - 1.5 = 69.76^\circ$

STEP-13-OTHER PARAMETERS

Addendum $h_a = m_t = 3$ mm

Dedendum $h_f = 1.1236 \times m_t = 1.1236 \times 3 = 3.4$ mm

Tooth height $h = h_a + h_f = 3 + 3.4 = 6.4$ mm

SPECIFICATION

SL NO	SPECIFICATION	PINION	GEAR
1.	Material	C45 steel	C45 steel
2.	Cone distance	114 mm	114 mm