## UNIT - 4

## TORSION

## PART-A

1. Write torsional equation
(AU April/May 2017)
$T / J=C \theta / L=q / R$
T-Torque
J- Polar moment of inertia
C-Modulus of rigidity
L- Length
q- Shear stress R-Radius
2. Define torsional rigidity. (AU Nov/Dec 2016)
The torque required to introduce unit angle of twist in unit length is called torsional rigidity or stiffness of shaft.
3. State any two functions of springs.
(AU Nov/Dec 2015)
4. To measure forces in spring balance, meters and engine indicators.
5. To store energy.
6. Write down the expression for power transmitted by a shaft.
(AU Nov/Dec 2014)
$\mathrm{P}=2 \pi \mathrm{NT} / 60$
Where, N -speed in rpm
T-torque
7. Write down the expression for torque transmitted by hollow shaft $\mathrm{T}=/ 16) * \mathrm{Fs} *((\mathrm{D} 4-\mathrm{d} 4) / \mathrm{d} 4$ Where, T -torque
q- Shear stress D-outer diameter d- Inner diameter
8. Write down the equation for maximum shear stress of a solid circular section in diameter ' $D$ ' when subjected to torque ' $T$ ' in a solid shaft.
$\mathrm{T}=\pi / 16$ * Fs*D3 where, T-torque
q- Shear stress D - diameter
9. What is composite shaft?

Sometimes a shaft is made up of composite section i.e. one type of shaft is sleeved over other types of shaft. At the time of sleeving, the two shafts are joined together, that the composite shaft behaves like a single shaft.

## 8. What is a spring?

A spring is an elastic member, which deflects, or distorts under the action of load and regains its original shape after the load is removed.
9. What are the various types of springs?
i. Helical springs ii. Spiral springs
iii. Leaf springs iv. Disc spring or Belleville springs
10. Classify the helical springs.

Close - coiled or tension helical spring.
Open -coiled or compression helical spring.
11. What is spring index ( C )?

The ratio of mean or pitch diameter to the diameter of wire for the spring is called the spring index.

## 12. What are the assumptions made in Torsion equation

The material of the shaft is homogeneous, perfectly elastic and obeys Hooke"s law.

Twist is uniform along the length of the shaft
The stress does not exceed the limit of proportionality
The shaft circular in section remains circular after loading o Strain and deformations are small.

## 13. What is solid length?

The length of a spring under the maximum compression is called its solid length. It is the product of total number of coils and the diameter of wire.

Ls $=n t \mathrm{xd}$
Where, $n t=$ total number of coils.

## 14. Define spring rate (stiffness).

The spring stiffness or spring constant is defined as the load required per unit deflection of the spring.
$\mathrm{K}=\mathrm{W} / \mathrm{y}$ Where, W-load
y- Deflection.

## 15. Define pitch.

Pitch of the spring is defined as the axial distance between the adjacent coils in uncompressed state. Mathematically

Pitch=free length n -1

## 16. Define helical springs..

The helical springs are made up of a wire coiled in the form of a helix and are primarily intended for compressive or tensile load.
17. What are the differences between closed coil \& open coil helical springs? Closed coil spring
The spring wires are coiled very closely, each turn is nearly at right angles to the axis of helix. Helix angle is less ( $7^{0}$ to $10^{\circ}$ )

## Open coil spring

The wires are coiled such that there is a gap between the two consecutive turns. Helix angle is large ( $>10 \mathrm{o}$ )
18. Write the assumptions in the theory of pure torsion.

1. The material is homogenous and isotropic.
2. The stresses are within elastic limit
3. $\mathrm{C} / \mathrm{S}$ which are plane before applying twisting moment remain plane even after the application of twisting moment.
4. Radial lines remain radial even after applying torsional moment.
5. The twist along the shaft is uniform

## 19. Define : Polar Modulus

Polar modulus is defined as the ratio of polar moment of inertia to extreme radial distance of the fibre from the centre.
20. Write the equation for the polar modulus for solid circular section

$$
\mathrm{Z}_{\mathrm{p}}=\frac{\pi \mathrm{d}^{3}}{16}
$$

## 21. Define Torsion

When a pair of forces of equal magnitude but opposite directions acting on body, it tends to twist the body. It is known as twisting moment or torsion moment or simply as torque.

Torque is equal to the product of the force applied and the distance between the point of application of the force and the axis of the shaft.

## 22. Define polar modulus

It is the ratio between polar moment of inertia and radius of the shaft. $£=$ polar moment of inertia $=\mathrm{J} / \mathrm{R}$
23. Why hollow circular shafts are preferred when compared to solid circular shafts?

* The torque transmitted by the hollow shaft is greater than the solid shaft.
* For same material, length and given torque, the weight of the hollow shaft will be less compared to solid shaft.


## PART-B

1. A solid shaft is to transmit 300 kW at 100 rpm if the shear stress is not exceed $80 \mathrm{~N} / \mathrm{mm}^{2}$. Find the diameter of the shaft. If this shaft were to be replaced by hollow shaft of same material and length with an internal diameter of 0.6 times the external diameter, what percentage saving in weight is possible.
[Madras Univ., Oct 96] (AU April/May 2017)
Given Data: $\quad \mathrm{P}=300 \mathrm{~kW}$

$$
\begin{aligned}
& \mathrm{N}=100 \mathrm{rpm} \\
& \tau=80 \mathrm{~N} / \mathrm{mm}^{2} \\
& \mathrm{~d}=0.6 \mathrm{D}_{1}
\end{aligned}
$$

[ $d_{1}$ - Inner diameter of hollow shaft $D_{1}$ - Outer diameter of hollow shaft] To find:

1. Diameter of the solid shaft(D)
2. \% of saving in weight

## @ Solution:

We know that,
Power,

$$
\begin{align*}
& \text { Power, } \mathrm{P}=\frac{2 \pi \mathrm{~N} \mathrm{~T}}{60} \\
& 300=\frac{2 \times \pi \times 100 \times \mathrm{T}}{60} \\
& \mathrm{~T}=28.6 \mathrm{kN}-\mathrm{m}=28.6 \times 10^{3} \mathrm{~N}-\mathrm{m} \\
& \mathrm{~T}=28.6 \times 10^{6} \mathrm{~N}-\mathrm{mm} \quad \ldots \ldots . .(1) \tag{1}
\end{align*}
$$

Torque for solid shaft (considering shear stress)

$$
\begin{aligned}
& \mathrm{T}=\frac{\pi}{16} \times \tau \times \mathrm{D}^{3} \\
& 28.6 \times 10^{6}=\frac{\pi}{16} \times 80 \times \mathrm{D}^{3}
\end{aligned}
$$

$$
\text { Solid shaft diameter, } \mathrm{D}=122.1 \mathrm{~mm}
$$

Solid shaft is replaced by hollow shaft
In hollow shaft, Inner diameter, d
Outer diameter, $\mathrm{D}_{1}$

Torque transmitted by hollow shaft

$$
\mathrm{T}=\frac{\pi}{16} \times \tau\left[\frac{\mathrm{D}_{1}^{4}-\mathrm{d}^{4}}{\mathrm{D}_{1}}\right]
$$

Where, $\mathrm{d}=0.6 \mathrm{D}_{1}$ (Given)

$$
\begin{align*}
\Rightarrow \quad & \mathrm{T}
\end{aligned} \begin{aligned}
16 & \frac{\pi}{16} \\
& \left.=\frac{\pi}{16} \times 80 \times \frac{\left(\mathrm{D}_{1}\right)^{4}-\left(0.6 \mathrm{D}_{1}\right)^{4}}{\mathrm{D}_{1}}\right] \\
& =\frac{\pi}{16} \times 80 \times \mathrm{D}_{1}^{3}[0.8704] \tag{2}
\end{align*}
$$

We know that,
Torque transmitted by hollow shaft is equal to torque transmitted by solid shaft when the solid shaft is replaced by hollow shaft.

Equating (1) and (2),

$$
\Rightarrow \quad 28.6 \times 10^{6}=\frac{\pi}{16} \times 80 \times \mathrm{D}_{1}^{3}[0.8704]
$$

$$
\text { External diameter, } \mathrm{D}_{1}=127.8 \mathrm{~mm}
$$

We know that,

$$
\mathrm{d}=0.6 \mathrm{D}_{1}=0.6 \times 127.8
$$

Internal Diameter, $\mathrm{d}=76.68 \mathrm{~mm}$
\% of saving in weight

$$
\begin{equation*}
=\frac{\text { Weight of solid shaft }- \text { Weight of hollow shaft }}{\text { weight of solid shaft }} \times 100 \tag{3}
\end{equation*}
$$

Weight of solid shaft
$=$ Area of solid shaft $\times$ Density $\times$ Length

$$
\begin{aligned}
& =\frac{\pi}{4}\left(\mathrm{D}_{1}^{2}-\mathrm{d}^{2}\right) \times \mathrm{p} \times \mathrm{L} \\
& =\frac{\pi}{4} \times\left[(127.8)^{2}-(76.68)^{2}\right] \times \mathrm{p} \times \mathrm{L}
\end{aligned}
$$

Weight of hollow Shaft $=8209.7 \times \mathrm{p} \times \mathrm{L}$
$(3) \Rightarrow$
$\%$ of saving in weight $=\frac{11709.03 \mathrm{pL}-8209.7 \mathrm{pL}}{11709.03 \mathrm{pL}} \times 100$
$\%$ of Saving in weight $=29.8 \%$
Result: Percentage of saving in weight $=29.8 \%$
2. A hollow shaft is to transmit 200 kW at 80 rpm . If the shear stress is not to exceed $70 \mathrm{MN} / \mathrm{m}^{2}$ and internal diameter is 0.5 of the external diameter. Find the external and internal diameters assuming that maximum torque is $\mathbf{1 . 6}$ times the mean. (AU April/May 2016)
Given Data:

$$
\begin{aligned}
& \mathrm{P}=200 \mathrm{~kW} \\
& \mathrm{~N}=80 \mathrm{rpm} \\
& \mathrm{~T}=70 \mathrm{MN} / \mathrm{m}^{2} \\
& =70 \times 10^{6} \mathrm{~N} / \mathrm{m}^{2}=70 \mathrm{~N} / \mathrm{mm}^{2} \\
& \mathrm{D}=0.5 \mathrm{D} \\
& \mathrm{~T}_{\max }=1.6 \mathrm{~T}_{\text {mean }}
\end{aligned}
$$

To find: External diameter (D)
Internal diameter (d)
Solution: We know that,
Power, P
$=\frac{2 \pi \mathrm{NT}}{60}$
$200=\frac{2 \times \pi \times 80 \times \mathrm{T}}{60}$
$\Rightarrow \quad$ Torque, $\mathrm{T}=23.87 \mathrm{kN} . \mathrm{m}$

$$
\begin{aligned}
\mathrm{T} & =23.87 \times 10^{3} \mathrm{~N}-\mathrm{m} \\
& =23.87 \times 10^{6} \mathrm{~N}-\mathrm{mm} \\
\mathrm{~T} & =\mathrm{T}_{\text {mean }}=23.87 \times 10^{6} \mathrm{~N}-\mathrm{mm}
\end{aligned}
$$

We know that,

$$
\begin{aligned}
& \mathrm{T}_{\max }=1.6 \mathrm{~T}_{\text {mean }} \\
& \mathrm{T}_{\max }=1.6 \times 23.87 \times 10^{6} \mathrm{~N}-\mathrm{mm} \\
& \mathrm{~T}_{\max }=38.19 \times 10^{6} \mathrm{~N}-\mathrm{mm}
\end{aligned}
$$

We know that,
$\mathrm{T}_{\max }=\frac{\pi}{16} \times \tau\left[\frac{\mathrm{D}^{4}-\mathrm{d}^{4}}{\mathrm{D}}\right]$
Substituted $=0.5 \mathrm{D}$

$$
\begin{array}{ll}
\Rightarrow & T_{\max }=\frac{\pi}{16} \times \tau\left[\frac{D^{4}-(0.5 \mathrm{D})^{4}}{\mathrm{D}}\right] \\
& 38.19 \times 10^{6}=\frac{\pi}{16} \times 70 \times \mathrm{D}^{4}\left[\frac{1-(0.5)^{4}}{\mathrm{D}}\right] \\
\Rightarrow & \mathrm{D}=143.6 \mathrm{~mm} \\
\Rightarrow \quad & \mathrm{~d}=0.5 \mathrm{D}=71.82 \mathrm{~mm}
\end{array}
$$

Result: Outer diameter, $\mathrm{D}=143.6 \mathrm{~mm}$
Inner diameter, $\mathrm{d}=71.82 \mathrm{~mm}$
3. A shaft is required to transmit a power of 210 kW at 200 rpm . The maximum torque may be 1.5 times the mean torque. The shear stress in the shaft should not exceed $45 \mathrm{~N} / \mathrm{mm}^{2}$ and the twist $1^{\circ}$ per metre length. Determine the diameter required if
(i) The shaft is solid
(ii) The shaft is hollow with external diameter twice the internal diameter. Take modulus of rigidity $=80 \mathrm{~N} / \mathrm{mm}^{2}$
(AU Nov/Dec 2015)
Solution:

$$
\begin{aligned}
& \text { Power }(\mathrm{P})=\frac{2 \pi \mathrm{NT}}{60} \\
& \begin{aligned}
& \mathrm{T}=\frac{\mathrm{P} \times 60}{2 \pi \mathrm{~N}}=\frac{210 \times 60}{2 \times \pi \times 200} \\
& \mathrm{~T}=\mathrm{T}_{\text {mean }}=10.02 \mathrm{KNm} \\
& \quad= 10.02 \times 10^{6} \mathrm{Nmm}
\end{aligned}
\end{aligned}
$$

$$
\begin{aligned}
& \text { WKT } \mathrm{T}_{\max } \\
&=1.5 \mathrm{~T}_{\text {mean }} \\
& \mathrm{T}_{\max }=15.03 \times 10^{6} \mathrm{Nmm}
\end{aligned}
$$

## For solid shaft

$$
\begin{aligned}
& \mathrm{T}=\frac{\pi}{16} \tau \mathrm{D}^{3} \\
& 15.03 \times 10^{6}=\frac{\pi}{16} \times 45 \times \mathrm{D}^{3} \\
& \mathrm{D}=119.37 \mathrm{~mm}
\end{aligned}
$$

For Hollow shaft $\quad[d=D / 2]$

$$
\begin{aligned}
& T_{\max }=\frac{\pi}{16} \tau\left[\frac{\mathrm{D}^{4}-\mathrm{d}^{4}}{\mathrm{D}}\right] \\
& 15.03 \times 10^{6}=\frac{\pi}{16} \times 45 \times\left[\frac{\mathrm{D}^{4}-\left(\frac{\mathrm{D}^{4}}{16}\right)}{\mathrm{D}}\right] \\
& 15.03 \times 10^{6}=8.835 \times \frac{15}{16} \mathrm{D}^{3} \\
& D=12.197 \mathrm{~mm} \\
& d=\frac{D}{2}=60.98 \mathrm{~mm}
\end{aligned}
$$

4. A close coiled helical spring is to carry a load of 100 N and the mean coil diameter is to be 8times that of the wire diameter. Calculate these diameters, if the maximum stress is to be $10 \mathrm{~N} / \mathrm{mm}^{2}$
(AU Nov/Dec 2014)
Given : Load (W) = 100N
Mean coil dia $(\mathrm{D})=8 \mathrm{~d}$
Max Shear stress $(\tau)=10 \mathrm{~N} / \mathrm{mm}^{2}$
WKT

$$
\begin{aligned}
& \tau=\frac{8 \mathrm{WD}}{\pi \mathrm{~d}^{3}} \\
& 10=\frac{8 \times 100 \times 8 \mathrm{~d}}{\pi \mathrm{~d}^{3}} \\
& \mathrm{~d}^{2}=\frac{8 \times 100 \times 8}{\pi \times 10} \\
& \mathrm{~d}=14.27 \mathrm{~mm} \\
& \mathrm{D}=8 \mathrm{~d}=114.18 \mathrm{~mm}
\end{aligned}
$$

5. A circular shaft of 100 mm diameter is required to transmit torque. Find the safe torque if the shear stress is not to exceed $\mathbf{1 0 0 M p a}$.
Given:-
Dia, $\mathrm{D}=100 \mathrm{~mm}$,
Shear stress, $\tau=100 \mathrm{Mpa}$

$$
\begin{aligned}
& =100 \mathrm{MN} / \mathrm{m}^{2}=100 \times 10^{6} \mathrm{~N} / 10^{4} \mathrm{~mm}^{2} \\
\tau & =100 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

## Required:-

Tonque, $\mathrm{T}=$ ?

## Solution:

Considering shear stress

$$
\begin{aligned}
\mathrm{T} & =\frac{\pi}{4} \times \tau \times \mathrm{D}^{3} \\
& =\frac{\pi}{4} \times 100 \times(100)^{3} \\
\mathrm{~T} & =19.635 \times 10^{4} \mathrm{~N} / \mathrm{mm}
\end{aligned}
$$

## Result:-

The sate torque, $T=19.635 \times 10^{6} \mathrm{~N} / \mathrm{mm}$.
6. A solid shaft of diameter 100 mm is required to transmit 150 kW at 120 rpm . If the length of the shaft is $\mathbf{4 m}$ and modulus of rigidity for the shaft is 75 Gpa . Find the angle of twist.

## Given:

$\mathrm{D}=100 \mathrm{~mm} ; \quad \mathrm{P}=150 \mathrm{KN} ; \quad \mathrm{N}=120 \mathrm{Kpm} ; \quad \lambda=4 \mathrm{~m}=4000 \mathrm{~mm} ;$
$\mathrm{c}=75 \mathrm{Gpa}=75 \times 10^{8} \mathrm{Gpa}$
$\mathrm{C}=75 \times 10^{9} \mathrm{~N} / \mathrm{m}^{2}=75 \times 10^{3} \mathrm{~N} / \mathrm{mm}^{2}$.

## Solution:

For solid shaft, (considering angle of twist)

$$
\begin{aligned}
& \frac{\mathrm{T}}{\mathrm{~J}}=\frac{\mathrm{C} \theta}{\ell} . \quad \mathrm{J}=\frac{\pi}{32}(\mathrm{D})^{4} . \\
& \mathrm{J}=9.81 \times 10^{6} \mathrm{~mm}^{4} \\
& \text { Power, } \mathrm{P}=\frac{2 \pi \mathrm{NT}}{60} \\
& \mathrm{~T}=11.93 \times 10^{6} \mathrm{~N} . \mathrm{mm}
\end{aligned}
$$

All values applied in equation (i)
$\frac{11.93 \times 10^{6}}{9.81 \times 10^{6}}=\frac{75 \times 10^{3} \times \theta}{4000}$
$\theta=0.06$ radians
$\theta=3.7^{\circ}$.
7. A hollow circular shaft of external diameter 40 mm and internal diameter 20 mm transmits a torque of 15 kNm . Find the maximum shear stress induced in the shaft.

## Given:

$$
\begin{aligned}
& \mathrm{D}=40 \mathrm{~mm} \\
& \mathrm{~d}=20 \mathrm{~mm} \\
& \mathrm{~T}=15 \mathrm{kN} \cdot \mathrm{~m}
\end{aligned}
$$

## Required:

$$
\mathrm{T}=?
$$

## Solution:

Consider shear stress,
For hollow section,

$$
\begin{aligned}
& \mathrm{T}=\frac{\pi}{16} \times \tau\left[\frac{\mathrm{D}^{4}-\mathrm{d}^{4}}{\mathrm{D}}\right] \\
& 15 \times 10^{6}=\frac{\pi}{16} \times \tau\left[\frac{(40)^{4}-(20)^{4}}{40}\right] \\
& 15 \times 10^{6}=11780.97 \tau \\
& \tau=1273.24 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

8. A hollow Shaft of external diameter 100 mm and internal diameter 50 mm is required to transist torque from one end to shaft can transmit, if the shear stress is not to exceed 50 Mpa.

Given:-

$$
\begin{aligned}
& \mathrm{D}=100 \mathrm{~mm} \\
& \mathrm{~d}=50 \mathrm{~mm} \\
& \tau=50 \mathrm{Mpa}=50 \times 10^{6} \mathrm{~N} / \mathrm{m}^{2} . \\
& \tau=50 \mathrm{~N} / \mathrm{mm}^{2} .
\end{aligned}
$$

## Solution:

Torque,

$$
\begin{aligned}
\mathrm{T} & =\frac{\pi}{16} \times \tau\left[\frac{\mathrm{D}^{4}-\mathrm{d}^{4}}{\mathrm{D}}\right] \\
& =\frac{\pi}{16} \times 50\left[\frac{(100)^{4}-(50)^{4}}{100}\right] \\
\mathrm{T} & =9.2 \times 10^{6} \mathrm{~N} . \mathrm{mm} \\
\mathrm{~T} & =9.2 \mathrm{KN} . \mathrm{m}
\end{aligned}
$$

## Result:

Torque, $\mathrm{T}=9.2 \mathrm{KN} . \mathrm{m} \ell$.
9. A hollow shaft of external diameter 120 mm transmits 300 kW power at 200rpm. Determine the maximum internal diameter if the maximum stress in the shaft is not to exceed $60 \mathrm{~N} / \mathrm{mm}^{2}$

## Given:

External Dia, $\mathrm{D}_{0}=120 \mathrm{~mm}$
Power, $\mathrm{P}=300 \mathrm{kN}$
Speed, N = 200 K.P.M
Max. Shear stress, $\tau=60 \mathrm{~N} / \mathrm{mm}^{2}$.
Solution:
Let, $\mathrm{D}_{\mathrm{i}}=$ Internal dia of shaft

$$
\begin{aligned}
& \mathrm{P}=\frac{2 \pi \mathrm{NT}}{60} \\
& \mathrm{~T}=\frac{300 \times 60}{2 \pi \times 200}=14.32 \mathrm{KN} . \mathrm{m} .
\end{aligned}
$$

We know, the equation,
$\mathrm{T}=\frac{\pi}{16} \times \tau \times \frac{\left(\mathrm{D}_{0}{ }^{4}-\mathrm{D}_{\mathrm{i}}{ }^{4}\right)}{\mathrm{D}_{0}}$
$14.32 \times 10^{6}=\frac{\pi}{10} \times 60 \times \frac{\left(120^{4}-\mathrm{D}_{\mathrm{i}}\right)}{120}$
$\left(D_{i}\right)^{4}=61.458 \times 10^{6}$
$\left(D_{0}\right)^{4}=\left(61.458 \times 10^{6}\right)^{1 / 4}$
10. Two shafts of the same material and of same lengths are subjected to the same torque, if the first shaft is of a solid circular section and the second shaft is of hollow circular section, whose internal diameter is $2 / 3$ of the outside diameter and the maximum shear stress developed in each shaft is the same, compare the weights of the shafts.

## Solution:

Let,
T - Torque transmitted by each shaft
$\tau$ - Max. shear stress developed in each shaft.
$D_{S}=$ outer diameter of solid shaft
$\mathrm{D}_{\mathrm{O}}=$ Outer diameter of hollow shaft
$D_{i}=$ Internal diameter of hollow shaft $=\frac{2}{3} D_{o}$
$\mathrm{W}_{1}=$ Weight of solid shaft
$\mathrm{W}_{\mathrm{H}}=$ weight of hollow shaft
$\mathrm{L}=$ length of each shaft
$\mathrm{W}=$ Weight density of the material each shaft.
Torque transmitted by the solid shaft,

$$
\begin{align*}
& \mathrm{T}=\frac{\pi}{16} \tau \cdot \mathrm{D}^{2} \\
& =\frac{\pi}{16} \tau\left[\frac{\mathrm{D}_{\mathrm{o}}^{4}-\frac{16}{81} \mathrm{D}_{\mathrm{o}}^{4}}{\mathrm{D}_{\mathrm{o}}}\right] \\
& =\frac{\pi}{16} \tau \times\left[\frac{\mathrm{D}_{\mathrm{o}}^{4}-0.196 \mathrm{D}_{\mathrm{o}}^{4}}{\mathrm{D}_{\mathrm{o}}}\right] \\
& \mathrm{T}=\frac{\pi}{16} \tau\left[\frac{0.804 \mathrm{D}_{\mathrm{o}}^{4}}{\mathrm{D}_{\mathrm{o}}^{4}}\right] \\
& \mathrm{T}-\frac{\pi}{16} \tau 0.804 \mathrm{D}_{\mathrm{o}}^{3} \tag{ii}
\end{align*}
$$

Equation (i) \& (ii)

$$
\begin{aligned}
& \frac{\pi}{16} \tau \mathrm{D}_{\mathrm{s}}^{3}=\frac{\pi}{16} \tau\left[0.804 \mathrm{D}_{\mathrm{o}}^{3}\right] \\
& \mathrm{D}_{\mathrm{s}}^{3}=0.804 \mathrm{D}_{\mathrm{o}}^{3} \\
& \mathrm{D}_{\mathrm{s}}=\left(0.804 \mathrm{D}_{\mathrm{o}}^{3}\right)^{1 / 3} \\
& \mathrm{D}_{\mathrm{S}}=(0.804)^{1 / 3} \cdot \mathrm{D}_{\mathrm{o}} \\
& \mathrm{D}_{\mathrm{s}}=0.93 \mathrm{D}_{\mathrm{o}}
\end{aligned}
$$

Now weight of solid shaft,

$$
\begin{align*}
& \mathrm{W}_{\mathrm{S}}=\text { weight density } \times \text { Volume of solid shaft } \\
\mathrm{W}_{\mathrm{H}}= & \omega \times \mathrm{A}_{\mathrm{H}} \times 1 \\
= & \omega \times \frac{\pi}{4}\left[\mathrm{D}_{\mathrm{o}}^{2}-\mathrm{D}_{\mathrm{i}}^{2}\right] \times \mathrm{L} \\
= & \omega \times \frac{\pi}{4}\left[\mathrm{D}_{\mathrm{o}}^{2}-\left(\frac{2}{3} \mathrm{D}_{\mathrm{o}}\right)^{2}\right] \times \mathrm{L} \\
= & \omega \times \frac{\pi}{4}\left[\mathrm{D}_{\mathrm{o}}^{2}-\frac{4}{9} \mathrm{D}_{\mathrm{o}}^{2}\right] \times \mathrm{L} \\
\mathrm{~W}_{\mathrm{H}}= & \omega \times \frac{\pi}{4} \times 0.556 \mathrm{D}_{\mathrm{o}}^{2} \times \mathrm{L} \ldots \ldots . .(\mathrm{iii}) \tag{iii}
\end{align*}
$$

Dividing Eqn (i) \& (ii)

$$
\begin{aligned}
\frac{\mathrm{W}_{\mathrm{S}}}{\mathrm{~W}_{\mathrm{H}}} & =\frac{\omega \times \frac{\pi}{4} \times \mathrm{D}_{\mathrm{S}}^{2} \times \mathrm{L}}{\omega \times \frac{\pi}{4} \times 0.556 \mathrm{D}_{\mathrm{o}}^{2} \times \mathrm{L}} \\
& =\frac{\mathrm{D}_{\mathrm{S}}^{2}}{0.556 \mathrm{D}_{\mathrm{o}}^{2}}
\end{aligned}
$$

We know, $\mathrm{D}_{\mathrm{S}}=0.93 \mathrm{D}_{\text {o }}$

$$
\begin{aligned}
& =\frac{\left(0.93 \mathrm{D}_{\mathrm{o}}\right)^{2}}{0.556 \mathrm{D}_{\mathrm{o}}{ }^{2}} \\
& =\frac{0.865 \mathrm{D}_{\mathrm{o}}{ }^{2}}{0.556 \mathrm{D}_{\mathrm{o}}{ }^{2}} \\
& =1.55
\end{aligned}
$$

11. A closely coiled helical spring is to carry a load of 500 N . Its mean diameter is to be $\mathbf{1 0}$ times that of the wire diameter calculate these diameter if the maximum shear stress in the materials of the spring is to be $80 \mathrm{~N} / \mathrm{mm}^{2}$. Also calculate the number of coils in the usually wired helical shoring if the Stiffness of the spring is $20 \mathrm{~N} / \mathrm{mm}$ deflection and modulus of rigidity $=8.6 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$.

## Given:

Load on spring, $\mathrm{W}=500 \mathrm{~N}$
Max. Shear stress, $\tau=80 \mathrm{~N} / \mathrm{mm}^{2}$.

## Required:

Diameter of wire, $\mathrm{d}=$ ?
Mean diameter of coil, $\mathrm{D}=$ ?

$$
\text { i.e., } \mathrm{D}=10 \mathrm{~d} .
$$

Solution:

$$
\begin{aligned}
& \tau=\frac{16 \mathrm{WR}}{\pi \mathrm{~d}^{3}} \\
& 80=\frac{16 \times 500 \times\left(\frac{\mathrm{D}}{2}\right)}{\pi d^{3}} \\
& 80=\frac{8000\left(10 \frac{d}{2}\right)}{\pi \mathrm{d}^{3}}
\end{aligned}
$$

$$
80 \times \pi d^{3}=8000 \times 5 \mathrm{~d}
$$

$$
\mathrm{d}^{3}=\frac{8000 \times 5}{80 \times \pi}=159.25
$$

$$
\mathrm{d}=12.6 \mathrm{~mm}
$$

Stiffness $(K)=\frac{\text { Load }}{\text { Deflection }}$
$\therefore \mathrm{K}=\frac{\mathrm{W}}{\Delta}$
$20=\frac{500}{\Delta}$
$\therefore \Delta=\frac{500}{20}$
$\Delta=25 \mathrm{~mm}$
We know, the general equation,
$\Delta=\frac{64 \mathrm{~W} \cdot \mathrm{R}^{3} \cdot \mathrm{n}}{\mathrm{C} \cdot \mathrm{d}^{4}}$
$25=\frac{64 \times 500 \times(63)^{3} \times \mathrm{n}}{8.4 \times 10^{4} \times(12.6)^{4}}$
$\mathrm{n}=6.6$
Say, 7 No 3.

## Result:-

(i) Wire diameter, $\mathrm{d}=12.6 \mathrm{~mm}$
(ii) Mean coiled diameter, $\mathrm{D}=26 \mathrm{~mm}$.
(iii) Deflection, $\Delta=25 \mathrm{~mm}$
(iv) no. of coils, $n=7$
12. A closely coiled helical spring of round wire 100 mm in diameter having 10 complete turns with a mean diameter of 120 mm is subjected to an axial load of 200N. Determine
i) The deflection of the spring
ii) Maximum shear stress in the wire
iii) Stiffness of the spring.

Take $\mathrm{C}=8 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$

## Given:

Dia of wire, $d=10 \mathrm{~mm}$
No. of turns, $n=10$
Mean dia of coil, $D=120 \mathrm{~mm}$
Radius of coil, $\mathrm{R}=\mathrm{D} / 2=60 \mathrm{~mm}$
Axial load, $\mathrm{W}=200 \mathrm{~N}$
Modulus of rigidity, $\mathrm{C}=8 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$

## Required:

$\Delta=$ Deflection of the spring $=$ ?
$\tau=$ maximum shear stress in the wire $=$ ?

$$
\mathrm{k}=\text { Stiffness of the spring }=?
$$

Solution:
(i) Deflection,

$$
\begin{aligned}
& \Delta=\frac{64 \mathrm{~W} \mathrm{R}^{3} \times \mathrm{n}}{\mathrm{c} \mathrm{~d}^{4}} \\
& \Delta=\frac{64 \times 200 \times(60)^{3} \times 10}{8 \times 10^{4} \times 10^{4}}=34.5 \mathrm{~mm}
\end{aligned}
$$

(ii) Shear stress,

$$
\begin{aligned}
& \tau=\frac{16 \mathrm{WR}}{\pi \mathrm{~d}^{3}} \\
& \tau=\frac{16 \times 200 \times 60}{\pi \times 10^{3}}=61.1 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

(iii) Stiffness of the spring, K
$\mathrm{K}=\mathrm{W} / \delta$
13. A close coiled helical spring of 100 mm mean diameter is made up of 10 mm diameter rod and has 20 turns. The spring carries an axial load of 200N. Determine the shearing stress taking the values of modulus of rigidity $=8.4 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$ Determine the deflection when carrying this load. Also calculate the stiffness of the spring and the frequency of free vibration for a mass hanging from it.

## Given:

Mean dia of coil, $\mathrm{D}=100 \mathrm{~mm}$
Mean radius of coil, $\mathrm{R}=\mathrm{D} / 2=100 / 2=50 \mathrm{~mm}$
Diameter of rod, $d=10 \mathrm{~mm}$
No. of turns, $n=20$
Axial load, $\mathrm{W}=200 \mathrm{~N}$
Modulus of rigidity, $\mathrm{C}=8.4 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$.
Required:

$$
\tau=? ; \quad \Delta=? ; \quad \mathrm{K}=? ; \quad \mathrm{g}=?
$$

## Solution:





$$
\mathrm{K}=5.25 \mathrm{~N} / \mathrm{mm}
$$



$$
=\frac{1}{2 \pi} \cdot \sqrt{\frac{981}{3.8095}}
$$

$$
\begin{aligned}
& \mathrm{g}=\text { centre of graduing } \\
& \Delta=\text { deflection in }
\end{aligned}
$$

Cycles/sec
14. The stiffness of a closely coiled helical spring is $1.5 \mathrm{~N} / \mathbf{m m}$ of compression under a maximum load of 60 N . The maximum shearing stress produced in the wire of the spring is $125 \mathrm{~N} / \mathrm{mm}^{2}$. The solid length of the spring (when the coils are touching) is given as 5 cm . Find (i) Diameter of wire (ii) mean diameter of the coils and (iii) number of coils required. Take $C=4.5 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$

## Given:

Stiffness of spring, $K=1.5 \mathrm{~N} / \mathrm{mm}$.
Load on spring, $W=60 \mathrm{~N}$
Max. shear stress,

$$
\tau=125 \mathrm{~N} / \mathrm{mm}^{2}
$$

Solid length of spring $=50 \mathrm{~mm}$
Modulus of rigidity, $\mathrm{C}=4.5 \times 10^{4} \mathrm{~N} / \mathrm{mm}^{2}$.

## Required:

Dia. Of wire, $d=$ ?
Mean dia of coil, $\mathrm{D}=$ ?
Mean radius of coil, $\mathrm{R}=\mathrm{D} / 2$.
No. of coils, $\mathrm{n}=$ ?

$$
\begin{align*}
& \mathrm{K}=\frac{\mathrm{Cd}^{4}}{64 \mathrm{R}^{3} \mathrm{n}} \\
& 1.5=\frac{4.5 \times 10^{4} \times \mathrm{d}^{4}}{64 \times \mathrm{R}^{3} \times \mathrm{n}} \\
& \mathrm{~d}^{4}=\frac{1.5 \times 64 \times \mathrm{R}^{3} \times \mathrm{n}}{4.5 \times 10^{4}} \\
& \mathrm{~d}^{4}=0.002133 \mathrm{R}^{3} \cdot \mathrm{n} \ldots \ldots(\mathrm{i}) \\
& \tau=\frac{16 \mathrm{~W} \times \mathrm{R}}{\pi \mathrm{~d}^{3}} \\
& 12.5=\frac{16 \times 60 \times \mathrm{R}}{\pi \mathrm{~d}^{3}} \\
& \mathrm{R}=0.40906 \mathrm{~d}^{3} \tag{ii}
\end{align*} \ldots . \text { (ii) }
$$

Substituting the value of R in equation (i), we get

$$
\begin{aligned}
\mathrm{d}^{4} & =0.02133 \times\left(0.40906 \mathrm{~d}^{3}\right) \times \mathrm{n} \\
& =0.002133 \times\left(0.40906^{3}\right) \times \mathrm{d}^{9} \times \mathrm{n}=0.00014599 \times \mathrm{d}^{9} \times \mathrm{n} \\
\frac{\mathrm{~d}^{9} . \mathrm{n}}{\mathrm{~d}^{4}} & =\frac{1}{0.00014599} \text { or }^{5} . \mathrm{n}=\frac{1}{0.00014599} \quad \rightarrow \text { (iii) }
\end{aligned}
$$

$$
\mathrm{d}^{5} . \mathrm{n}=\frac{1}{0.000146}
$$

Solid length, $=\mathrm{n} \times \mathrm{d}$

$$
\begin{aligned}
& 50=\mathrm{n} \times \mathrm{d} \\
& \mathrm{n}=\frac{50}{\mathrm{~d}} \ldots . .(\mathrm{iv})
\end{aligned}
$$

Substituting eqn (iv) in (iii)

$$
\begin{aligned}
& \mathrm{d}^{3} \times \frac{50}{\mathrm{~d}}=\frac{1}{0.00016} \\
& \mathrm{~d}^{4}=137 \\
& \mathrm{~d}=(137)^{1 / 4} \\
& \mathrm{~d}=3.42 \mathrm{~mm}
\end{aligned}
$$

Substituting, $\mathrm{d}=3.42 \mathrm{~mm}$ value in eqn (iv)

$$
\begin{aligned}
& \mathrm{n}=\frac{50}{\mathrm{~d}}=\frac{50}{3.42}=14.62 \text { say } 15 \\
& \mathrm{n}=15
\end{aligned}
$$

Substitute, $\mathrm{d}=3.42 \mathrm{~mm}$ value in eqn (ii)

$$
\begin{aligned}
& \mathrm{R}=0.40906 \mathrm{~d}^{3}=0.40906(3.42)^{2} \\
& \mathrm{R}=16.36 \mathrm{~mm}
\end{aligned}
$$

Mean dia of coil, $\mathrm{D}=2 \mathrm{R} \quad(\mathrm{R}=\mathrm{D} / 2)$

$$
\begin{aligned}
& =2 \times 16.36=32.72 \\
& D=32.72 \mathrm{~mm}
\end{aligned}
$$

15. An open coil helical spring made of 10 mm diameter wire and of mean diameter 10 cm has 12 coils, angle of helix being $15^{\circ}$. Determine the axial deflection and intensities of bending and shear stress under a load of 500 N . Take $C$ as $80 \mathrm{kN} / \mathrm{mm} 2$ and $E=200 \mathrm{kN} /$ $\mathbf{m m}^{2}$. [Nov/Dec 2014]

## Given Data:

Diameter of wire $(\mathrm{d})=10 \mathrm{~mm}=0.01 \mathrm{~m}$
Mean coil diameter $(\mathrm{D})=10 \mathrm{~cm}=0.1 \mathrm{~m}$
No.of coils $(\mathrm{n})=12$ radius $(\mathrm{R})=\frac{\mathrm{D}}{2}=0.05 \mathrm{~m}$
Angle of helix $(\propto)=15^{\circ}$
Axial load $(\mathrm{W})=500 \mathrm{~N}$
$\mathrm{C}=80 \mathrm{KN} / \mathrm{mm}^{2}=80 \times 10^{9} \mathrm{~N} / \mathrm{m}^{2}$
$\mathrm{E}=200 \mathrm{kN} / \mathrm{mm}^{2}=200 \times 10^{9} \mathrm{~N} / \mathrm{m}^{2}$

## To find:

(i) Axial Deflection ( $\delta \backslash$ )
(ii) Bending Stress $\left(\sigma_{b}\right)$
(iii) Shear stress $(\tau)$

## Solution:

(i) Axial Deflection ( $\delta$ )
$\delta=2 \mathrm{WR}^{3} \mathrm{n} \pi \sec \alpha\left[\frac{\cos ^{2} \alpha}{\mathrm{CI}_{\mathrm{P}}}+\frac{\operatorname{Sin}^{2} \alpha}{\mathrm{EI}}\right]$
$\delta=2 \times 500 \times 0.05^{3} \times 12 \times \pi \sec 15 \times$

$$
\left[\frac{\cos ^{2} 15}{80 \times 10^{9} \times \frac{\pi}{32} \times(0.01)^{4}}+\frac{\operatorname{Sin}^{2} 15}{200 \times 10^{9} \times \frac{\pi}{64} \times(0.01)^{4}}\right]
$$

$\delta=0.061 \mathrm{~mm}$
$\sigma_{\mathrm{b}}=\frac{32 \mathrm{M}}{\mathrm{Td}^{3}}$
$M=W R \sin \propto=500 \times 0.05 \times \sin 15$
$\mathrm{M}=6.47 \mathrm{Nm}$

$$
\sigma_{\mathrm{b}}=\frac{32 \times 6.47}{\pi \times 0.01^{3}}=65.90 \mathrm{~W} / \mathrm{m}^{2}
$$

(iii) Shear stress ( $\tau$ )

$$
\tau=\frac{16 \mathrm{~T}}{\pi \mathrm{~d}^{3}}
$$

$\tau=\mathrm{WR} \cos \propto=500 \times 0.05 \times \cos 15$
$\tau=24.14 \mathrm{Nm}$
$\tau=\frac{16 \times 24.14}{\left(\pi \times 0.01^{3}\right)}=122.94 \mathrm{MN} / \mathrm{m}^{2}$
$90=\sigma_{x}=\sin \theta, 30=\sigma_{x=} \cos \theta$
Thus,

$$
\begin{aligned}
& \sigma_{x}=\sqrt{90^{2}+30^{2}} \\
& =94.87 \mathrm{MN} / \mathrm{m}^{2} \quad(\text { Ans }) \\
& \frac{\sigma_{x} \sin \theta}{\sigma_{x} \cos \theta}=\frac{90}{30}=3
\end{aligned}
$$

Or, $\quad \tan \theta=3$
Or, $\quad \theta=71^{\circ} 33^{\prime}($ Ans $)$

