



from half wave dipole and quarter wave Radiation monopole Imsink(H-2) Im Sm (H-Z) + 4 RITIONO H dz 2=0 - perfect reflecting L=2H Image Im Sm k (H+2) < Im 8m /3 (H+2) (b, corresponding monopole (a) centre-fed dipole with assumed sinusoidal current Figure car shourd a centre-fed dipole with distibution sinusoidal cuerent distribution & (6) shows corresponding a "A dipele antenne" is a strenight rediator, usually fed in the center and producing a maximum of hadiation in the plane normal to the asure. The length specified in T. length specified is the overall length. Radiation from a cuaster-wave monopole ce halfware dipole It will be assumed that the current is smuloidally distributed as shown in figure. I = Im Sink(H-2), 270 Then, $E = Im Sm \beta (H+Z) , Z < 0$ Im > The value of current at the current loop (22) current maximum.





The expression for the vector potentral at point P due to the current element Idz is $dA_2 = \mu I e^{-JBR} dZ \longrightarrow O$ R -> distance from The current element to point P. The total vector potential at p due to all the current elements will be, $A_2 = \frac{H}{4\pi} \int_{-H}^{0} \frac{\Gamma_m sm \beta (H+2)e^{-j\beta R} dz}{\pi}$ + $\frac{\mu}{4\pi} \int \frac{\sum m \sin \beta (H-z) e^{-i\beta R}}{R} dz \rightarrow \textcircled{D}$) REAR [Ray] -> (in denominate) NO -> R in the phase facture, so the difference between R and V is important. R= 8-2 Cord. Then the expression for Az becomes A2: MIme Br Sm B (H+2) e jkzcus Q H + $\int_{a}^{H} smh(H-2) e^{jhz(\omega)\theta} dz \rightarrow 3$ [if H=>14. $sm \beta (H+2) = sm \beta (H-2) \qquad x = x + 2$ · sin (11/2+ 132) = Sm (172-132)

 $flen eq (9) becomes, = cor \beta 2.] + cor \beta 2.$ $H cor \beta 2. + \int shr \beta (Hz)$ $H z = \mu Im e^{-\int \beta r} \left[\int_{-H}^{0} cor \beta 2 e^{-\int \beta 2} d2 + \int shr \beta (Hz) e^{\int \beta 2} cer \delta d2 \right]$



$$= \frac{\mu \operatorname{Im} e^{-\frac{1}{2} \operatorname{Im} 2}}{4 \operatorname{Im} 2} \left[\int_{0}^{1} \operatorname{cu} ||_{22} e^{-\frac{1}{2} \operatorname{cu} S} \frac{d^{2}}{d^{2}} \int_{0}^{1} \operatorname{cu} ||_{22} \operatorname{cu} ||_{22} \operatorname{cu} S} \frac{d^{2}}{d^{2}} \int_{0}^{1} \operatorname{cu} ||_{22} \operatorname{cu} S} \frac{d^{2}$$





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$$= \frac{f}{p} \left[\int_{-\infty}^{\infty} \frac{e^{-\beta RY}}{2\eta \sqrt{k}} \frac{dd}{s\eta^{-2}\theta} \int_{-\infty}^{\infty} \frac{1}{2\theta} \int_{-\infty}^{0} \frac{1}{2\theta} \int_$$



$$\frac{P_{av}}{\pi r^2} \frac{30 \operatorname{I}_{\mathrm{ym}_{1}}}{(\pi r^2)} \left[\frac{(\omega^2 (\pi_1 \cos))}{\sin^2 0} \right] w/m^2,$$

Power Radiation by a Half wave dipole and its Radiation resistance Poynting Vectors Method Elemental area of the spherical shell $ds = 2\pi r^2 \sin \theta \, d\theta \rightarrow 0$ power tated W = plands = J = 30 Ims (car2 (0)2 (as 0) ? gradiated W = s Pav ds = J = Ims (car2 (0)2 (as 0) ? $= 60 \text{ frms} \int_{0}^{\infty} \left(\frac{\cos^2(\overline{\eta}_2 \cos \theta)}{\sin \theta} + \frac{1}{2} \cos \theta \right) d\theta$ = $bo Ims \int Y_2 \left\{ \frac{(1+cos(Tcos0))}{Smp} \right\}$ (2 cm 2= 1+ cas 2 = 60 I mai × I I -> numerical Entegestion method (or) graphics method cord Simpon's cord trep. e Zoidal eules, I = 1.219 $W = 60 I_{rmJ} \times 1.219$ W = 73.140 LymsW = Inno Rr Ry = 73-14 = 732

quarter-wave Rr = 73.14 = 36.57 pc.