

SNS COLLEGE OF TECHNOLOGY COIMBATORE - 641 035. (An Autonomous Institution)



DEPARTMENT OF MECHANICAL ENGINEERING

19MEB201 - Fluid Mechanics and Machinery
UNIT -2 FLOW OVER FLAT PLATE AND FLOW THROUGH CIRCULAR CONDUITS

Therefore the head loss of the Letter Case is four times of the former comes due to doubled mean velocity. ii) Various Minos Lossen -The loss of energy due to frection in a pipe is known as mojor losses while the loss of energy caused on account of the change in relocity of flowing flind is called minos losses are usually quite small as Compared to the loss of energy due to friction and hence, they are Called minor losses. Some times it may be reglected without Serious covers. But in Case of short pipes these losses are comparable with the loss of energy, every due to friction. Some of the losses of energy, which may cause due to the change of velocity, are as follows. 1. Loss of energy due to Sudden enlargement 2. Loss of acres head due to Sudden Contraction 3. Loss of energy at the entrance to the prin 4. hors of energy at the exit from the pipe 5. Loss of energy due to gradual Contraction

- 6. Loss of energy due to an obstruction in a
- 7. Loss of energy in bends
- 8. Loss of energy in varieus pipes fillings.
- Two temps of fluid (P= 998 kg/m³ and $\mu = 0.001$ kg at 20°C are Connected by a Capillary tube 4 m, in diameter, and 3.5 m long. The Surface of temps. 30 cm higher than the Surface of temps 2.

 Estimate the flow rate in m³/n. Is the flow land. For what tube diameter will Reynolds number be 500; (NOV 2013)

Given data: $P = 998 \text{ kg/m}^{3} \quad \mu = 0.001 \text{ kg/ms} = 0.001 \frac{\text{N}}{\text{m}}$ $D = 4mm = 0.004m, \quad L = 3.5m$ $Z_{1} - Z_{2} = H = 30 \text{ cm} = 0.3 \text{ m}$

Solution:

Exit velocity of flow in the Capillary tube $V = \sqrt{2gH} = \sqrt{2 \times 9.81 \times 0.3} = 2.4\frac{1}{2}$

From Continuty equation $flow rate = AV = \frac{\pi}{4}D^{2}V.$ $= \frac{\pi}{4}(0.004)^{2} \times 2.426$ $= 3.05 \text{ m}^{3}/\text{s}$ Reynolds number $Re = \frac{PVD}{I}$

= 9684.59 75000

Therefore, the flow is lumbered as flow through pipes through lube is Considered as flow through pipes and Reynolds number of the flow is more than 5000. For the Reynolds number 500, the diameters of the tube is given by $D = \frac{\text{Re } \mu}{\text{PV}} = \frac{500 \times 0.001}{998 \times 2.426} = 0.206 \, \text{mm}$

3) A 150mm diameter pipe reduces in diameter absorptly to 100mm diameter. If the pipe Cavenes water at 30 litres per Second, Calculate the Pressure loss across the Contraction. Take 6 efficient of Contraction as 0.6 (Nov 2012)

Giron Data:

di= 150mm = 0.15m, d2= 100mm = 0.1m.

8 = 30 hz/s = 0.03 m3/s

Co-efficient of Contraction Cc = 0.6

Solution:

Asea $A_1 = \frac{x}{4} d_1^2 = \frac{x}{4} (0.15)^2 = 0.01767 m^2$ $A_2 = \frac{x}{4} d_2^2 = \frac{x}{4} (0.1)^2 = 7.85 \times 10^{-3} m^2$ From Continuity equation

$$V_1 = \frac{\alpha}{A_1} = \frac{0.03}{0.01767} = 1.697 \text{ m/s}$$

Head loss due to Sudden Contraction.

$$h_{c} = \frac{V_{2}^{2}}{2g} \left[\frac{1}{C_{c}} - 1 \right]^{2}$$

$$= \frac{3 \cdot Q_{2}^{2}}{2 \times 9 \cdot 81} \left[\frac{1}{0.6} - 1 \right]^{2}$$

- a A plate of boomm length and 400mm wide is immersed in a flord of specific gravity 0.9 and Kinemertic visiosity of (2) =10-4 m 2/s The flird is moving with the velocity of m/s Determine
 - (1) Boundary Layer thickness.
 - (2) Shear stress at the end of the Plante
 - (3) sing force on one side of the plate

Given data:

 $L = 600 \, \text{mm} = 0.6 \, \text{m}$, S = 0.9 $V = 6 \, \text{m/s}$ $b = 400 \, \text{mm} = 0.4 \, \text{m}$ $V = 10^{-4} \, \text{m}^2/\text{s}$

Solution

Boundary Layer thickness Re = $\frac{UL}{V} = \frac{6 \times 0^{-6}}{10^{-4}} = 36000$ Reynolds number Re = $\frac{UL}{V} = \frac{6 \times 0^{-6}}{10^{-4}} = 36000$ Sine Re $< 5 \times 10^{5}$ the flew is Lerminar , therefore, the thickness of boundary layer and shear stress for thickness of boundary layer and shear stress for leminar flow are obtained as follows.

The empirical relation for thickness of boundary Louyer for Laminar flow is given by

Prandel -Bzassino as

$$G_{tam} = \frac{5x}{\sqrt{Re}} = \frac{5 \times 0.6}{\sqrt{3600}} = 0.0158$$

(ii) Shear Stress at the end of the Plate

Shear Stress $I_0 = \frac{\mu \ U \pi}{2 f} = \frac{0.9 \times (1 \times 10^{-4}) \times b \times \pi}{2 \times 0.0158}$

= 0.0536 N/m2

(iii) Drag forse on the Side of the plate

(8) A pipe of 12cm diameter is Carrying an oil (h= 2.2 pa.5 and P=1250 kg/m³) with a velocity of 4,5 m/s. Determine the shear stress at the wall surface of the pipe, head loss, if the length of the pipe is 25 m and the power lost.

(Nov 2011)

Given Data:

D= 12cm = 0.12m

L= 25m, h= 2.2 Pa.S = 2.2 N.S/m2

P= 1250 kg/m3, V= 4.5 m/s.

Solution:

$$G = AU = \frac{\pi}{4} D^2 U = \frac{\pi}{4} \times 0.12^2 \times 4.5$$

 $G = 0.051 \,\text{m}^3/\text{s}$.

From Hagen-possessible's equation $P_{1}-P_{2} = \frac{128 \, \mu \, \text{GpL}}{\times \, \text{D4}}$ $P_{1}-P_{2} = \frac{128 \, \text{X} \, \text{Z} \cdot \text{Z} \, \text{X} \, \text{D} \cdot \text{D51} \, \text{X} \, \text{25}}{\times \, \text{X} \, \text{D} \cdot \text{124}}$ $P_{1}-P_{2} = \frac{551}{147}, \frac{147}{67}, \frac{67}{67}, \frac{7}{64}$

Shear stress at the pipe will

$$T_{max} = \left(-\frac{dP}{dx}\right) \frac{R}{2}$$

$$= \frac{P_1 - P_2}{L} \times \frac{R}{2}$$

$$= \frac{55 \cdot 1147}{25} \times \frac{0.12}{242}$$

$$= \frac{661.38 \cdot N/m^2}{242}$$

$$= \frac{32 \cdot \mu UL}{WD^2}$$

$$= \frac{32 \cdot \mu UL}{Pg \cdot D^2}$$

$$= \frac{32 \cdot \chi 2.2 \times 4.5 \times 25}{(1250 \times 9.81) \times (0.12)^2}$$

$$= 44.85 \cdot m$$

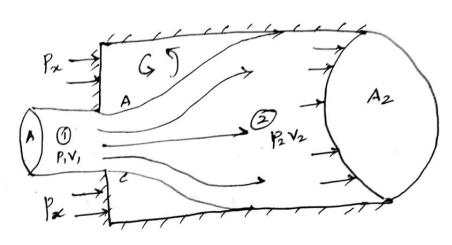
Power Lost
$$P = WGhL$$

$$P = (1250 \times 9.81) \times 0.051 \times 44585$$

$$P = 28.05 \text{ kW}$$

Minor Head Losses

The local or minor head losses are Coursed by certain local features or disturbances. The disturbances may se Carried by changes in the Size or shape of a pipe; this would affect the velocity distribution and may result in eddy formation.



The above Exetch explains two pipes of Cross-Sectional area A, and Az glanged Cross-Sectional area A, and Az glanged together with a Constant density fluxl from together with a Constant density fluxl from the Smaller- diameter pipe to the Larger-

diameter pape.

The flord fails to make an adjustment with the change in direction needed for Complete with the change in direction needed for Complete filling of the Larger drimeter pipe.

The flow brokes away from the edge Magrow Section; eddies form and the resulting turbulence Canses disorpation of · If a styff lin energy. The initiation and origin of turbulance is due to fixed momenting and its inester Consider 2 Sertions 1-17through the plane of Tol Enpermeron 2-2 End of the region of extension turbulence Coursed by first Seperation From Momentum Considerations!

P, A, + Bx (A2-A,) - B2 A2 = Wt (1/2-V,) or regleiting any radial acceleration of third in the Plane of change in Section, the volority at the armular AB and CD is very small and So the pressure there Cam be assumed to be equal to the pressure of incoming

i.e. $\beta_{n} = P_{i}$ and then the momentum equation transforms to $P_{i}-P_{2}$ $A_{2}=\frac{w_{B}}{9}\left(V_{2}-V_{i}\right)$

or.
$$\frac{P_1-P_2}{W}=\frac{E_1}{A_2g}$$
 (V_2-V_1)
 $=\frac{V_1-V_2-V_1}{W}$

Invoking to Reinverdly Equation.

 $\frac{P_1}{W}+\frac{V_1^2}{2g}=\frac{P_2}{W}+\frac{V_2^2}{2g}+hearp.$

Where heap represents to head loss due to an absorpt enpansion.

 $heap=(\frac{P_1-P_2}{W})+\frac{V_1^2-V_2^2}{2g}$

Combining enquession () and (ii)

 $heap=\frac{V_2-(V_2-V_1)}{g}+(\frac{V_1^2-V_2^2}{2g})$
 $hoap=\frac{(V_1-V_2)^2}{2g}$

Endently the loss of head due to adsorpt enfancion equals the velocity head Computed enfancion equals the velocity head Computed for the velocity difference, Since by Continuity $A_1V_1=A_2V_2$
 $V_2=\frac{A_1}{A_2}$

and therefore, equation (3) may be attenuturly written as $hoap=[1-(\frac{A_1}{A_2})]^2\frac{V_1^2}{2g}=keap\frac{V_1^2}{2g}$

The head loss is a further of incoming velocity head. When area Az is very Large as Compared with A, velocity V2 Cam be assumed to be Zero,

Loss of velocity head and kinetic energy is then Complete. The flow situation Corresponds to a pipe discharging into a Large reservoir of sufficient size.

Hence, Head loss is called as pipe exit loss hout.

hexit = Kexit
$$\frac{V^2}{2g}$$

hexit = $1\frac{V^2}{2g}$
 $= \frac{1}{2g}$

V represents the average volority in the pipe

other Terms Symonyms with the loss of head due to an absorpt enlargement are

- Eddy loss because the expansion loss of head is expended exclusively on eddy formation, and Continuous Sustenance of notational motion of the flird masses.
 - Shock loss because an absorpt Engrammin Causes Sudden slowing of the flied stream.

Impostant formulas: (D) Loss of energy due to Sudden enlargement (he) $h_e = \frac{(V_1 - V_2)^2}{29}$ 1 Loss of energy due to Sudden Contraction (bc) where K = 0.375 to 0.5 If C. Value or Kis not given, then the head loss due to friction is taken Loss of energy at the entrance to a pipe(hi) Loss of energy at the exit from a pipe (ho) (3) Loes of energy due to an obstrution in a pipe $h_0 = \frac{V^2}{2g} \cdot \left(\frac{A}{C_c (A-a)} - 1 \right)^2$ Vc - Velocity of light at Vena - Contracta Ac - Area of Cross Section at Vena - Contracta oes of evergy due to gradual Contraction or Enlargement (h) h_= k (V1-V2)

The loss of energy due to Bend in pipe (his) $h_b = \frac{kV^2}{\frac{2g}{2g}}$ K - G - efficients which depends on the total angle of bend on radius of Curvalius of bend.

Loss of energy in various pipe fillings. $h_V = \frac{kV^2}{2g}$ $k \Rightarrow loefficient$, which depends on the type of

pipefitting.