## Problems

Let us consider a solid shaft being subjected to a torque of 1.6 $\mathrm{k} \mathbf{N m}$. Find the necessary diameter of the shaft, if the allowable shear stress is 50 MPa . The allowable twist is $1^{\circ}$ for every 20 diameters length of the shaft. Take C $=80 \mathrm{GPa}$.

## Given:

$\mathrm{T}=1.6 \mathrm{kNm}, \mathrm{f}_{\mathrm{s}}=50 \mathrm{~N} / \mathrm{mm}^{2}, \theta=1^{\circ}$,
$\mathrm{I}=20 \mathrm{~d}, \mathrm{C}=80 \mathrm{~N} / \mathrm{mm}^{2}$
i)Diameter of shaft considering strength of shaft.
(i.e., Taking the consideration that the shear stress should not exceed the permissible limit)

For a solid circular shaft,

$$
T=\frac{\pi}{16} f_{s} D^{3}
$$

$1.6 \times 10^{6}=\frac{\pi}{16} \times 50 \times D^{3}$
$\operatorname{orD}=\sqrt[3]{\frac{16 \times 1.6 \times 10^{6}}{\pi \times 50}}=54.63 \mathrm{mmSay} 55 \mathrm{~mm}$
ii)Diameter of shaft considering stiffness of shaft.
(i.e., Taking the consideration that the angle of twist should not exceed the permissible limit)

Using the Torsional equation,

$$
\frac{\mathrm{T}}{\mathrm{~J}}=\frac{\mathrm{C} \theta}{\ell} \quad\left(\because \mathrm{~J}=\frac{\pi}{32} \mathrm{D}^{4} \text { for soild shaft }\right)
$$

$$
\frac{T}{\frac{\pi}{20} D^{4}}=\frac{C \theta}{20 D}
$$

Or

$$
(\because 1=20 D)
$$

Or $\frac{32 \mathrm{~T}}{\pi \mathrm{D}^{3}}=\frac{\mathrm{C} \theta}{20} \quad \theta=1^{\circ}=^{\frac{\pi}{180}} \mathrm{rad}$

$$
\begin{aligned}
\mathrm{D} & =\sqrt[3]{\frac{32 \mathrm{~T} \times 20}{\pi \mathrm{C} \theta}} \\
& =\sqrt[3]{\frac{32 \times 1.6 \times 10^{6} \times 20 \times 180}{\pi \times 80 \times 10^{3} \times \pi}}
\end{aligned}
$$

$=61.59 \mathrm{~mm}$ say 62 mm
$\therefore$ Necessary diameter of shaft is the maximum value of (i) and (ii) i.e., 62 mm .

A solid cylindrical shaft is to transmit 300 KW power at 100 rpm . If the shear stress is not to exceed $\mathbf{6 0 ~ N} / \mathrm{mm}^{2}$, find its diameter. What percent saving in weight would be obtained it this shaft is replaced by a hollow one whose internal diameter equals to 0.6 of the external diameter, the length, the material and the maximum shear stress being the same.

Given

| Solid shaft | Hollow shaft |
| :--- | :--- |
| speed, $\mathrm{N}=100 \mathrm{rpm}$ |  |
| $\mathrm{P}_{\mathrm{s}}=300 \mathrm{KW}$ | $\mathrm{P}_{\mathrm{h}}=300 \mathrm{KW}$ |
| $\mathrm{f}_{\mathrm{s}}=60 \mathrm{~N} / \mathrm{mm}^{2}$ | $\mathrm{~d}=0.6 \mathrm{D}_{\mathrm{h}}$ |
| $\mathrm{D}=?$ |  |

Length is same, i.e., $1_{s}=1_{h}$
Material is same, i.e., $C_{s}=C_{h}$;
Max shear stress is same, i.e., $\left(f_{s}\right)_{s}=\left(f_{s}\right)_{h}$
For a solid shaft,
using the equation, $\mathrm{P}=\frac{2 \pi \mathrm{NT}}{60}$
$\operatorname{cr} 300 \times 10^{3}=\frac{2 \pi \times 100 \times T}{60}$

$$
\frac{300 \times 10^{3} \times 60}{2 \pi \times 100}
$$

$\therefore$ Torque, $\mathrm{T}=$
$=28647.8 \mathrm{Nm}$
$=28647800 \mathrm{Nmm}$

Using the equation, $\mathrm{T}=$

$$
\frac{\pi}{16} f_{s} D^{3}
$$

$28647800=\frac{\pi}{16} \times 60 \times D^{3}$
orD $=\sqrt[3]{\frac{28647800 \times 16}{\pi \times 60}}$
SolvingD $=134.49$ say 135 mm .

## For hollow shaft

Givend $=0.6 D_{h}$
Since length, material and maximum shear stress values are the same, the torque transmitted by a solid shaft is equal to the torque transmitted by a hollow shaft, i.e., $T_{h}=28647800 \mathrm{~N} \mathrm{~mm}$

But Torque transmitted by a hollow shaft

$$
\left.\begin{array}{c}
T_{h}=\frac{\pi}{16} f_{s} \frac{\left(D_{h}^{4}-d^{4}\right)}{D_{h}} \\
\therefore 28647800= \\
=\frac{\pi}{16} \times 60 \times\left(\frac{D_{h}^{4}-\left(0.6 D_{h}\right)^{4}}{D_{h}}\right) \\
=\frac{60 \pi}{16} \times\left(\frac{D_{h}^{4}-0.1296 D_{h}^{4}}{D_{h}}\right) \\
D_{h}
\end{array}\right)
$$

$28647800=\frac{60 \pi}{16} \times 0.8704 \mathrm{D}_{\mathrm{h}}^{3}$
$\therefore \mathrm{D}_{\mathrm{h}}=\sqrt[3]{\frac{16 \times 28647800}{60 \pi \times 0.8704}}$
$=140.86 \mathrm{~mm}$ say 141 mm
$\therefore$ Internal dia, $\mathrm{d}=0.6 \mathrm{D}_{\mathrm{h}}$
$=0.6 \times 141$
$=84.6 \mathrm{~mm}$

## \% Saving in weight

Weight of shaft $=\left(\begin{array}{lcc}\begin{array}{l}\text { weight } \\ \text { density }\end{array} & \times \begin{array}{c}\text { Cross } \\ \text { of shaft }\end{array} & \begin{array}{c}\text { Length } \\ \text { of shaft }\end{array}\end{array} \begin{array}{c}\text { of } \\ \text { shaft }\end{array}\right)$
$\therefore$ Weight of solid shaft

$$
w_{s}=\rho \frac{\pi}{4} D^{2} 1
$$

Weight of hollow shaft

$$
W_{h}=\rho \frac{\pi}{4}\left(D_{h}^{2}-d^{2}\right) 1
$$

Both shafts are of same length and same material. Therefore, density and length are the same. And also weight of solid shaft is more than weight of hollow shaft for the same length.
$\therefore$ Percentage saving in weight

$$
\begin{gathered}
=\frac{w_{s}-W_{h}}{w_{s}} \times 100 \\
=\frac{\left(\frac{\pi}{4} D^{2} \rho l\right)-\left(\frac{\pi}{4}\left(D_{h}^{2}-d^{2}\right) \rho l\right)}{\frac{\pi}{4} D^{2} \rho l} \times 100 \\
=\frac{D^{2}-\left(D_{h}^{2}-d^{2}\right)}{D^{2}} \times 100 \quad\left(\because D=135 \mathrm{~mm} D_{h}=141 \mathrm{mn}\right) \\
=\frac{135^{2}-\left(141^{2}-84.6^{2}\right)}{135^{2}} \times 100 \quad\left(d_{h}=84.6 \mathrm{~mm}\right) \\
=\frac{18225-12723}{18225} \times 100
\end{gathered}
$$

= 30.18\%
Here we see an example of a solid aluminium shaft 1 m long and 100 mm diameter is replaced by a hollow steel shaft of the same length and same external diameter. The angle of twist per unit torsional moment over total length is same for both the shafts. If modulus of rigidity of steel is thrice that of aluminium, find the inner diameter of steel shaft.

## Given


$1_{a}=1000 \mathrm{~mm}_{\mathrm{s}}=1000 \mathrm{~mm}$
$D_{a}=100 \mathrm{mmD}_{\mathrm{s}}=\mathrm{D}_{\mathrm{a}}=100 \mathrm{~mm}$
$C_{s}=3 C_{a}$
It is given

$$
\left(\frac{\theta}{T}\right)_{\text {Solid }}=\left(\frac{\theta}{T}\right)_{\text {hollow }}
$$

## $C_{\text {steel }}=3 \mathbf{C}_{\text {aluminium }}$

Find the diameter of shaft.

Using the torsional equation,

$$
\frac{\mathrm{T}}{\mathrm{~J}}=\frac{\mathrm{C} \theta}{\ell}
$$

orTl $=\mathrm{C} \theta \mathrm{J}$
or

$$
\frac{\theta}{T}=\frac{\ell}{C J}
$$

$$
\left(\frac{\theta}{T}\right)_{\text {solid }}=\left(\frac{\theta}{T}\right)_{\text {hollow }}
$$

It is given
or $\quad\left(\frac{\ell}{\mathrm{CJ}}\right)_{\text {soild }}=\left(\frac{\ell}{\mathrm{CJ}}\right)_{\text {hollow }}$
or

$$
\frac{\ell_{\mathrm{a}}}{\mathrm{C}_{\mathrm{a}} \mathrm{~J}_{\mathrm{a}}}=\frac{\ell_{\mathrm{s}}}{\mathrm{C}_{\mathrm{s}} \mathrm{~J}_{\mathrm{s}}}
$$

or $\quad \frac{1000}{C_{a} \times \frac{\pi}{32} D_{a}^{4}}=\frac{1000}{3 C_{a} \times \frac{\pi}{32}\left(D_{s}^{4}-d^{4}\right)}$
$\left(\mathrm{C}_{\mathrm{s}}=3 \mathrm{C}_{\mathrm{a}}\right)$
or
or

$$
\begin{aligned}
\frac{1}{\mathrm{D}_{\mathrm{a}}^{4}} & =\frac{1}{3 \times\left(\mathrm{D}_{\mathrm{s}}^{4}-\mathrm{d}^{4}\right)} \\
\frac{1}{100^{4}} & =\frac{1}{3 \times\left(100^{4}-\mathrm{d}^{4}\right)}
\end{aligned}
$$

or100 ${ }^{4}=\left(3 \times 100^{4}\right)-3 d^{4}$
or3d $d^{4}=\left(3 \times 10^{8}\right)-10^{8}$
$3 d^{4}=2 \times 10^{8}$
Solving $d=\sqrt[4]{\frac{2 \times 10^{8}}{3}}$
$=90.36 \mathrm{mmsay} 91 \mathrm{~mm}$.
Let us consider a solid circular shaft transmits 75 KW power at 200 rpm. Calculate the shaft diameter, if the twist in the shaft is not to exceed $1^{\circ}$ in 2 m length of shaft and shear stress is
limited to $50 \mathrm{~N} / \mathrm{mm}^{2}$. Take modulus of rigidity, $\mathrm{C}=1 \times 105$ $\mathrm{N} / \mathrm{mm}^{2}$.

Given:
$\mathrm{P}=75 \mathrm{KW}, \mathrm{N}=200 \mathrm{rpm}$,
$\theta=1^{\circ}, \mathrm{I}=2000 \mathrm{~mm}$
$\mathrm{f}_{\mathrm{s}}=50 \mathrm{~N} / \mathrm{mm}^{2}, C=1 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$. Solid shaft dia?

Using the equation, $\mathrm{P}=\frac{2 \pi \mathrm{NT}}{60}$

$$
\begin{aligned}
T & =\frac{60 \mathrm{P}}{2 \pi \mathrm{~N}} \\
& =\frac{60 \times 75 \times 10^{3}}{2 \pi \times 200}
\end{aligned}
$$

$=3582.8 \mathrm{Nm}$
$=3582.8 \times 10^{3} \mathrm{~N} \mathrm{~mm}$
ii)Diameter of shaft considering the strength of shaft.

Using the equation, $T=\frac{\pi}{16} f_{s} D^{3}$

Diameter,

$$
D=\sqrt[3]{\frac{16 \mathrm{~T}}{\pi \mathrm{f}_{\mathrm{s}}}}
$$

$$
=\sqrt[3]{\frac{16 \times 3582.8 \times 10^{3}}{\pi \times 50}}
$$

## $=71.47$ say 72 mm

ii)Diameter of shaft considering the stiffness of shaft.

Using the equation, $\left.\frac{T}{J}=\frac{C \theta}{\ell}_{\left(0=1^{\circ}=\right.}^{\frac{\pi}{180}} \mathrm{rad}\right)$

$$
\frac{\mathrm{T}}{\frac{\pi}{32} D^{4}}=\frac{\mathrm{C} \theta}{\ell}
$$

Substituting the values,

$$
\frac{32 \times 3582.8 \times 10^{3}}{\pi \times \mathrm{D}^{4}}=\frac{1 \times 10^{5} \times \pi}{2000 \times 180}
$$

or $\frac{32 \times 3582.8 \times 10^{3} \times 2000 \times 180}{1 \times 10^{5} \times \pi^{2}}=\mathrm{D}^{4}$
$\operatorname{orD}=\sqrt[4]{\frac{32 \times 3582.8 \times 10^{3} \times 2000 \times 180}{1 \times 10^{5} \times \pi^{2}}}$
$=80.43$ mmsay 81 mm
$\therefore$ Diameter of the shaft is the larger value of (i) and (ii) i.e., 81 mm.

A hollow shaft of diameter ratio $3 / 8$ (internal dia to outer dia) is to transmit 375 kW power at 100 rpm . The maximum torque being $\mathbf{2 0} \%$ greater than the mean torque. The shear stress is not to exceed $60 \mathrm{~N} / \mathrm{mm}^{2}$ and twist in a length of 4 m not to exceed $2^{\circ}$. Calculate the external and internal diameters which would satisfy both the above conditions. Assume modulus of rigidity, $\mathrm{C}=0.85 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$.

Given:

$$
\frac{d}{D}=3 / 8, P=375 \mathrm{~kW}=375 \times 10^{3} \mathrm{w},
$$

$\mathrm{N}=100 \mathrm{rpm}_{\text {max }}=20 \%$ greater than $\mathrm{T}_{\text {mean }}=1.2 \mathrm{~T}_{\text {mean }}$

$$
\begin{aligned}
& \mathrm{f}_{\mathrm{s}}=60 \mathrm{~N} / \mathrm{mm}^{2} . \theta=2^{\circ}=2 \times \frac{\pi}{180} \mathrm{rad} \\
& \mathrm{I}=4 \mathrm{~m}=4000 \mathrm{~mm} ; \mathrm{C}=0.85 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

Find d ? D?
$2 \pi \mathrm{NT}$
Using the relation, $\mathrm{P}=$ 60

$$
T=\frac{60 P}{2 \pi N}=\frac{60 \times 375 \times 10^{3}}{2 \pi \times 100}=35810 \mathrm{Nm}
$$

$\mathrm{T}_{\text {max }}=1.2 \mathrm{~T}_{\text {max }}$
$\therefore \mathrm{T}_{\text {max }}=1.2 \times 35810 \mathrm{Nm}$
$=42972 \mathrm{Nm}$
$=42972 \times 10^{3} \mathrm{~N} \mathrm{~mm}$
i)Diameter of the shaft considering the strength of shaft (i.e., shear stress not to exceed $60 \mathrm{~N} / \mathrm{mm}^{2}$ )

For a hollow shaft, using the relation

$$
T=\frac{\pi}{16} f_{s}\left(\frac{D^{4}-d^{4}}{D}\right)
$$

$$
\operatorname{or} 42972 \times 10^{3}=
$$

(Note that $T=T_{\max }$ and $\frac{d}{D}=3 / 8 \quad$ or $d=3 / 8$ D)
or $\frac{42972 \times 10^{3} \times 16}{\pi \times 60}=\frac{D^{4}-(3 / 8 D)^{4}}{D}$

$$
=\frac{D^{4}}{D}\left\{1-\left(\frac{81}{4096}\right)\right\}
$$

$3649426=\mathrm{D}^{3} \times \frac{4015}{4096}$
orD $=\sqrt[3]{\frac{3649426 \times 4096}{4015}}$
$=154.98 \mathrm{mmsay} 155 \mathrm{~mm}$
ii)Diameter of the shaft considering the stiffness of shaft (i.e., angle of twist not to exceed $\mathbf{2}^{\circ}$ )

Using the relation, $\frac{\mathrm{T}}{\mathrm{J}}=\frac{\mathrm{C} \theta}{\ell}$
Substitute $=T_{\text {max }}=42972000 \mathrm{~N} \mathrm{~mm}$
$J=\frac{\pi}{32}\left(D^{4}-d^{4}\right)$
$\mathrm{C}=0.85 \times 10^{3}$
$\theta=2^{\circ}=\frac{2 \times \pi}{180} \mathrm{rad}=0.0349 \mathrm{rad}$
$\mathrm{I}=4 \mathrm{~m}=4000 \mathrm{~mm}$

$$
\begin{aligned}
\therefore \quad \frac{42972000 \times 32}{\pi\left(\mathrm{D}^{4}-\mathrm{d}^{4}\right)} & =\frac{0.85 \times 10^{5} \times 0.0349}{4000} \\
\text { or } & \\
\mathrm{D}^{4}-\mathrm{d}^{4} & =\frac{42972000 \times 32 \times 4000}{\pi \times 0.85 \times 10^{5} \times 0.0349} \\
&
\end{aligned}
$$

$$
\text { or } \quad D^{4}-\left(\frac{3}{8} \mathrm{D}\right)^{4}=590.2 \times 10^{6}
$$

$$
\text { or } \quad D^{4}-\left(\frac{81}{4096} D^{4}\right)=590.2 \times 10^{6}
$$

or $\quad \mathrm{D}^{4}\left(1-\frac{81}{4096}\right)=590.2 \times 10^{6}$
or $\quad \mathrm{D}^{4}\left(\frac{4015}{4096}\right)=590.2 \times 10^{6}$
or

$$
\mathrm{D}=\sqrt[4]{\frac{590.2 \times 10^{6} \times 4096}{4015}}
$$

$=156.6 \mathrm{~mm}$ say 157 mm
Ans: The diameter of the shaft to satisfy both the conditions are the greater of values (i) and (ii) i.e., 157 mm .
$\therefore$ External dia. D $=157 \mathrm{~mm}$

Internal dia, $\mathrm{d}=$

$$
3 / 8 \mathrm{D}=3 / 8 \times 157
$$

$=59 \mathrm{~mm}$

A hollow shaft is to transmit 300 KW at 80 rpm . If the shear stress is not to exceed $60 \mathrm{MN} / \mathrm{m}^{2}$ and internal diameter is 0.6 of the external diameter, find the external and internal diameters assuming that the maximum torque is $\mathbf{1 . 4}$ times the mean.

## Given:

PowerP $=300 \mathrm{KW}=300 \times 10^{3}$ Watts
Speed, $\mathrm{N}=80 \mathrm{rpm}$
Shear stress, $\mathrm{f}_{\mathrm{s}}=60 \mathrm{MN} / \mathrm{m}^{2}=\frac{60 \times 10^{6}}{10^{6}}=60 \mathrm{~N} / \mathrm{mm}^{2}$
Internal diameter $=0.6 \times$ External diameter
i.e., d $=0.6 \mathrm{D}$
$\mathrm{T}_{\text {max }}=1.4 \times \mathrm{T}_{\text {mean }}$
Find D ?d?

Using the relation, $\mathrm{P}=\frac{2 \pi \mathrm{NT}_{\text {mann }}}{60}$
$\therefore T_{\text {mean }}=\frac{60 \mathrm{P}}{2 \pi \mathrm{~N}}$

$$
=\frac{60 \times 300 \times 10^{3}}{2 \pi \times 80}=35809 \mathrm{Nm}
$$

$=35809 \times 10^{3} \mathrm{~N} \mathrm{~mm}$
i)Diameter of shaft based on strength of shaft.

Using the relation, $T=\frac{\pi}{16} f_{S}\left(\frac{D^{4}-d^{4}}{D}\right)$
or $1.4 \times 35809 \times 10^{3}=$

$$
\frac{\pi}{16} \times 60\left[\frac{\mathrm{D}^{4}-(0.6 \mathrm{D})^{4}}{\mathrm{D}}\right]
$$

or50132600 $=11.78\left(\frac{\mathrm{D}^{4}-0.1296 \mathrm{D}^{4}}{\mathrm{D}}\right)$
$\frac{D^{4}}{D}(1-0.1296)$
or
$=4255738$
$\operatorname{orD}^{3}(0.8704)=4255738$
$\therefore \mathrm{D}=\sqrt[3]{\frac{4255738}{0.8704}}$
$=169.72$ say 170 mm .
$\therefore$ External diameter, $\mathrm{D}=170 \mathrm{~mm}$
Internal diameter, $\mathrm{d}=0.6 \mathrm{D}$
$=0.6 \times 170=102 \mathrm{~mm}$.
A solid shaft is subjected to a torque of 45 k Nm . If angle of twist is 0.5 degree per meter length of the shaft and shear stress is not to exceed $90 \mathrm{MN} / \mathrm{m} 2$ find, i)Suitable diameter of shaft,ii)Find maximum shear stress and the angle of twist per meter length. Modulus of rigidity $=\mathbf{8 0} \mathbf{G N} / \mathrm{m2}$.

## Given:

Torque, $\mathrm{T}=45 \mathrm{kNm}=45 \times 10^{6} \mathrm{Nmm}$
Angle of twist, $\theta=0.5^{\circ}=0.5 \times \pi / 180 \mathrm{rad}=8.726 \times 10^{3} \mathrm{rad}$ Shear stress, $\mathrm{f}_{\mathrm{s}}=90 \mathrm{MN} / \mathrm{m}^{2}=90 \mathrm{~N} / \mathrm{mm}^{2}$

Shear modulus, $C=80 \mathrm{GN} / \mathrm{m}^{2}=\frac{\frac{80 \times 10^{9}}{10^{6}}}{}=80 \times 10^{3} \mathrm{~N} / \mathrm{mm}^{2}$ Length $=1 \mathrm{~m}=1000 \mathrm{~mm}$
i)Diameter of shaft based on strength of shaft

Using the relation, $T=\frac{\pi}{16} f_{S} D^{3}$
$\operatorname{or} 45 \times 10^{6}=\frac{\pi}{16} \times 90 \times D^{3}$
$\operatorname{orD}=\sqrt[3]{\frac{16 \times 45 \times 10^{6}}{\pi \times 90}}$
$=136.55$ say 137 mm
ii)Diameter of shaft based on stiffness of shaft

Using the relation $\frac{T}{J}=\frac{C \theta}{\ell}$
or

$$
\frac{T}{\frac{\pi}{32} D^{4}}=\frac{C \theta}{\ell}
$$

orD $=\sqrt[4]{\frac{32 \mathrm{~T} \times 1}{\pi \times \mathrm{C} \theta}}$

$$
=\sqrt[4]{\frac{32 \times 45 \times 10^{6} \times 1000 \times 180}{\pi \times 80 \times 10^{3} \times 0.5 \times \pi}}
$$

$=160 \mathrm{~mm}$.
$\therefore$ Diameter of the shaft is the greater of values (i) and (ii) i.e., 160 mm
iii)Find maximum shear stress

Using the relation $\frac{T}{J}=\frac{f_{s}}{R}$

$$
\begin{aligned}
& \quad \frac{45 \times 10^{6}}{\frac{\pi}{32} \times 160^{4}}=\frac{\mathrm{f}_{8}}{\left[\frac{160}{2}\right]} \quad \text { (Substitute } D=160 \mathrm{~mm} \text { ) } \\
& \therefore \mathrm{f}_{\mathrm{s}}=55.95 \mathrm{~N} / \mathrm{mm}^{2}
\end{aligned}
$$

iv)Find angle of twist per meter length
(Substitute D = 160 mm)

Using the relation,

$$
\frac{\mathrm{T}}{\mathrm{~J}}=\frac{\mathrm{C} \theta}{\ell}
$$

$$
\frac{45 \times 10^{6}}{\frac{\pi}{32} \times 160^{4}}=\frac{80 \times 10^{3} \times \theta}{1000}
$$

or
Solving, $\theta=8.742 \times 10^{-3} \mathrm{rad}$
$=8.742 \times 10^{-3} \times\left(\frac{180}{\pi}\right)$
degrees
$=0.5^{\circ}$.
Let us consider the diameter of a sold shaft to transmit 90 KW at 160 rpm such that the shear stress is limited to $60 \mathrm{~N} / \mathrm{mm}^{2}$. The maximum torque is likely to exceed the mean torque by $20 \%$. Also find the permissible length of the shaft, if the twist is not to exceed 1 degree over the entire length. Take rigidity modulus as $0.8 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$.

Given:
$P=90 K W=90 \times 10^{3}$ Watts,
$\mathrm{N}=160 \mathrm{rpm}, \mathrm{f}_{\mathrm{s}}=60 \mathrm{~N} / \mathrm{mm}^{2}$,
$\mathrm{T}_{\text {max }}=1.2 \mathrm{~T}_{\text {mean }}$
$\theta=1^{\circ}={ }^{\frac{1 \times \pi}{180}} \mathrm{rad} ;$
$\mathrm{C}=0.8 \times 10^{5} \mathrm{~N} / \mathrm{mm}^{2}$.
Find I?

Using the relation, $\mathrm{P}=\frac{2 \pi \mathrm{NT}_{\text {mean }}}{60}$

$$
\therefore T_{\text {mean }}=\frac{60 \mathrm{P}}{2 \pi \mathrm{~N}}=\frac{60 \times 90 \times 10^{3}}{2 \pi \times 160}
$$

$=5374.2 \mathrm{Nm}$
$=5374.2 \times 10^{3} \mathrm{~N} \mathrm{~mm}$.
i)Diameter of shaft

Using the relation, $T=\frac{\pi}{16} f_{s} D^{3}$
$\operatorname{orD}=\sqrt[3]{\frac{16 \mathrm{~T}}{\pi \times \mathrm{f}_{\mathrm{S}}}}$

$$
=\sqrt[3]{\frac{16 \times 5374.2 \times 10^{3} \times 1.2}{\pi \times 60}}
$$

$=81.80$ say 82 mm
ii)Permissible length, I

Using the relation, $\frac{\mathrm{T}}{\mathrm{J}}=\frac{\mathrm{C} \theta}{l}$
$\frac{\mathrm{T}}{\frac{\pi}{32} \mathrm{D}^{4}}=\frac{\mathrm{C} \theta}{l}$
Substituting the values,

$$
\frac{1.2 \times 5374.2 \times 10^{3}}{\frac{\pi}{32} \times 82^{4}}=\frac{0.8 \times 10^{5} \times \pi}{180 \times l}
$$

$$
l=\frac{0.8 \times 10^{5} \times \pi \times 82^{4} \times \pi}{32 \times 5374.2 \times 10^{3} \times 180 \times 1.2}
$$

$=961 \mathrm{~mm}$

