

Design a S.S.B of span 5m to carry a factored UDL of 47 kN/m. Use ISMB section & take beam as laterally supported. The depth of the beam shouldn't exceed 350 mm.

S.S.B,  $l = 5\text{m}$

Factored load = 47 kN/m

ISMB, laterally supported beam  
depth  $\nless 350\text{mm}$ .

Step 1: Load Calculation;

$w$  (given) = 47 kN/m  
(if not assume)

Step 2: B.M Calculation

---

$$\begin{aligned} \text{Max B.M (S.S.B)} &= \frac{wl^2}{8} = \frac{47 \times 5^2}{8} \\ &= 146.875 \text{ kNm} = 146.875 \times 10^6 \end{aligned}$$

Step 3: S.F. Calculation (V):

$$V \text{ (S.S.B)} = \frac{wL}{2} = \frac{47 \times 5}{2} = 115 \text{ kN}$$

Step 4: Calculation of section Modulus ( $Z_p$ ):

$$\begin{aligned} Z_p &= \frac{M \gamma_{mo}}{f_y} \\ &= \frac{146.875 \times 10^6 \times 1.1}{250} \end{aligned}$$

$Z_p \text{ (required)} = 646250 \text{ mm}^2$

Step 5: Selection I-section:

In given problem, depth of section shouldn't exceed 350 mm  $\leftarrow$  ISMB section.

ISMB 350 (Pg. no. 2  $\rightarrow$  steel table)

$$Z_e = 778.9 \times 10^3 \text{ mm}^3$$

$$Z_p = 1.12 \times Z_e = 884.8 \times 10^3 \text{ mm}^3$$

$$h = 350 \text{ mm}$$

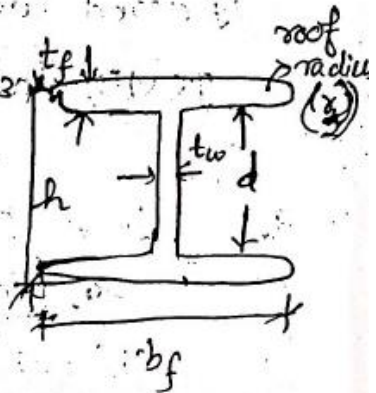
$$b_f = 140 \text{ mm}$$

$$t_f = 14.2 \text{ mm}$$

$$r_1 = 14 \text{ mm}$$

$$t_w = 8.1 \text{ mm}$$

$$b = \frac{b_f}{2}$$



$$I_z = 136503 \times 10^4 \text{ mm}^4$$

Where,  $b \rightarrow$  outstand of flange (in compression flange).

$$b = \frac{140}{2} = 70 \text{ mm}$$

Pg. no. - 18

$\downarrow$  Table 2

Step 6: Classification of section:

Rolled steel section

	$b/b_f$	$d/t_w$
$\rightarrow$ Plastic	$9.4 \leq$	$84 \leq$
$\rightarrow$ Compact	$10.5 \leq$	$105 \leq$
$\rightarrow$ Semi-compact	$15.7 \leq$	$126 \leq$

neutral axis @ mid-depth.

$$i) \quad b = 70 \text{ mm} \Rightarrow \frac{b}{t_f} = \frac{70}{14.2} = 4.92 < 9.4$$

$$ii) \quad d = h - 2(t_f + r_1) = 350 - 2(14.2 + 14) = 293.6 \text{ mm}$$

$d$

Step 7: Check for shear.

The given problem is laterally supported beam

$$\text{So, } V \leq V_d$$

pg. no. 59  
8.4

$$V_d = \frac{f_y \times h \times t_w}{\gamma_{m0} \times \sqrt{3}} = \frac{250 \times 350 \times 8.1}{1.1 \times \sqrt{3}}$$

$$= 372.99 \text{ kN}$$

$$V = 117.5 \text{ kN (from step 1)}$$

$V < V_d \Rightarrow \text{So, check for shear is satisfied.}$

Step 8: Check for Moment carrying capacity.

The given section is plastic & laterally supported

$$V = 117.5 \times 10^3 \text{ N} \quad \text{① } (V \leq 0.6 V_d)$$

$$0.6 \times V_d = 0.6 \times (372.99)$$

$$= 223.794$$

$(V < V_d)$ . Hence safe.

②  $M_d$  (8.2.112 - pg no 53)

$$M_d = \frac{\beta_b Z_p f_y}{\gamma_{m0}} \leq \frac{1.2 Z_e f_y}{\gamma_{m0}} \quad ($$

$\beta_b = 1$  (plastic section)

$$\rightarrow M_d = \frac{1 \times 884.8 \times 10^3 \times 250}{1.1}$$

$$= 201.0909 \times 10^6 \text{ Nmm}$$

$$\rightarrow \frac{1.2 Z_e f_y}{\gamma_{m0}} = \frac{1.2 \times 771.9 \times 10^5 \times 250}{1.1}$$

$$= 21242.7 \text{ kNm}$$

Step 9: Check for Deflection:

$$\delta < \frac{l}{300}$$

$$\rightarrow \delta_{(S.S.B)} = \frac{5wl^4}{384EI} = \frac{5 \times 47 \times (5000)^4}{384 \times 2 \times 10^5 \times 13130.9 \times 10^6}$$

$$\delta = 14.03 \text{ mm} \quad \text{from steel table.}$$

$$\rightarrow \frac{l}{300} = \frac{5000}{300} = 16.67 \text{ mm}$$

$14.03 < 16.67$ , Hence, check for deflection is satisfied.