

### CE short circuit current gain using hybrid- $\pi$ model:

Figure 4.6.1 shows the Hybrid-  $\pi$  model for a single transistor with a resistive load  $R_L$ .

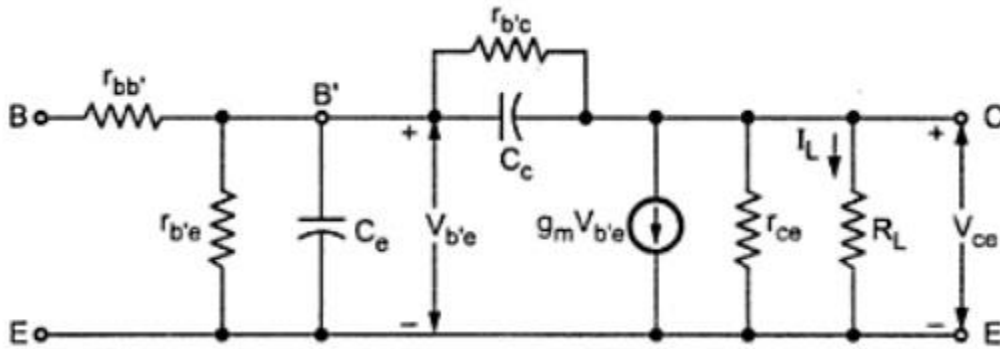


Figure 4.6.1 Hybrid-  $\pi$  model for a single transistor with a resistive load  $R_L$

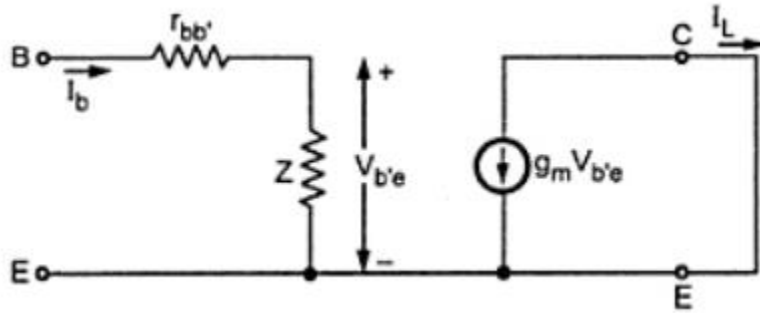
Miller capacitance is  $C_M = C_{b'c} (1 + g_m R_L)$

Here,  $R_L = 0$

$$\therefore C_M = C_{b'c} (C_e)$$

Parallel combination of  $r_{b'e}$ , and  $(C_e + C_c)$  is given as

$$\begin{aligned} Z &= \frac{r_{b'c} \times \frac{1}{j\omega(C_e + C_c)}}{r_{b'e} + \frac{1}{j\omega(C_e + C_c)}} \\ &= \frac{r_{b'e}}{1 + j\omega r_{b'e} (C_e + C_c)} \end{aligned}$$



**Figure 4.6.2 Simplified Hybrid pi model**

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$$V_{b'e} = I_b Z$$

$$Z = V_{b'e} / I_b$$

The current gain for the circuit figure 4.6.2 is,

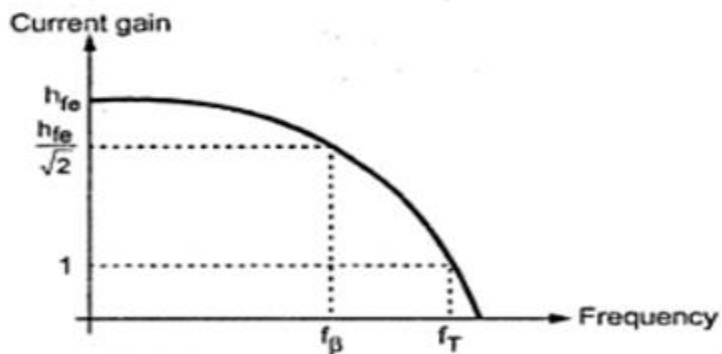
$$A_i = \frac{I_L}{I_b} = \frac{-g_m V_{b'e}}{I_b} \quad \because I_L = -g_m V_{b'e}$$

$$A_i = -g_m Z$$

$$= \frac{-g_m r_{b'e}}{1 + j\omega r_{b'e} (C_e + C_c)}$$

$$A_i = \frac{-h_{fe}}{1 + j\omega r_{b'e} (C_e + C_c)}$$

Figure 4.6.3 shows the Frequency Vs Current Gain



**Figure 4.6.3 Frequency Vs Current Gain**

$$f_{\beta} = \frac{1}{2 \pi r_{b'e} (C_e + C_c)}$$

$$A_i = \frac{-h_{fe}}{1 + j \frac{f}{f_{\beta}}}$$

$$|A_i| = \frac{h_{fe}}{\sqrt{1 + \left(\frac{f}{f_{\beta}}\right)^2}}$$

### $f_{\beta}$ (Cutoff frequency):

It is the frequency at which the transistor short circuit CE current gain drops by 3dB or  $1/\sqrt{2}$  times from its value at low frequency. It is given as,

$$f_{\beta} = \frac{1}{2 \pi r_{b'e} (C_e + C_c)}$$

or

$$= \frac{g_{b'e}}{2 \pi (C_e + C_c)}$$

or

$$= \frac{1}{h_{fe}} \frac{g_m}{2 \pi (C_e + C_c)} \quad \because g_{b'e} = \frac{1}{r_{b'e}} = \frac{g_m}{h_{fe}}$$

### $f_{\alpha}$ (Cut-off frequency):

It is the frequency at which the transistor short circuit CB current gain drops by 3dB or  $1/\sqrt{2}$  times from its value at low frequency.

The current gain for CB configuration is given as,

$$A_i = \frac{-h_{fb}}{1 + j \frac{f}{f_\alpha}}$$

where

$$f_\alpha = \frac{1}{2\pi r_{b'e} (1 + h_{fb}) C_e}$$

$$= \frac{1 + h_{fe}}{2\pi r_{b'e} C_e} \approx \frac{h_{fe}}{2\pi r_{b'e} C_e}$$

$$|A_i| = \frac{h_{fb}}{\sqrt{1 + \left(\frac{f}{f_\alpha}\right)^2}}$$

At

$$f = f_\alpha$$

$$|A_i| = \frac{h_{fb}}{\sqrt{2}}$$

### Parameter $f_T$ :

It is the frequency at which short circuit CE current gain becomes unity.  
at  $f = f_T$ ,

$$1 = \frac{h_{fe}}{\sqrt{1 + \left(\frac{f_T}{f_\beta}\right)^2}}$$

The ratio of  $f_T / f_\beta$  is quite large compared to 1.

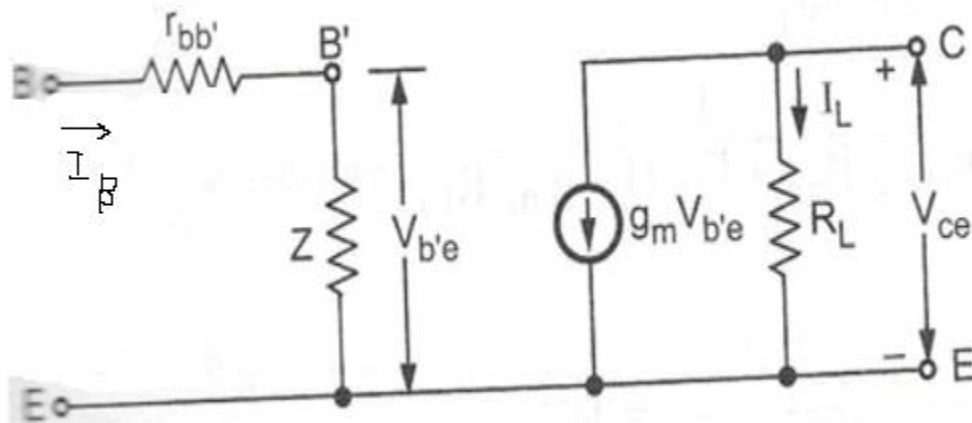
$$f_T = g_m / 2\pi C_e$$

**Current gain with resistive load:**

$$C_{eq} = C_e + C_c (1 + g_m R_L)$$

For further simplification in figure 4.6.4,

At output circuit value of  $C_c$  can be calculated as,



**Figure 4.6.4. Simplified hybrid –  $\pi$  model for CE with  $R_L$**

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$$\frac{1}{\frac{j\omega C_c}{k-1}} \approx \frac{1}{j\omega C_c}$$

$$C_c \left( \frac{k}{k-1} \right) \approx C_c$$

$$Z = \frac{V_{b'e}}{I_b}$$

$$A_i = \frac{-h_{fe}}{1 + j\left(\frac{f}{f_H}\right)}$$

$$|A_i| = \frac{h_{fe}}{\sqrt{1 + \left(\frac{f}{f_H}\right)^2}}$$

At  $f = f_H$   
 $A_i = \frac{h_{fe}}{\sqrt{2}}$

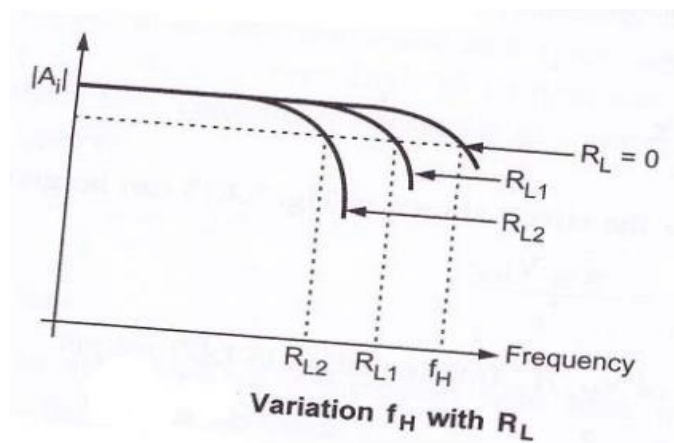
$f_H$  is the frequency at which the transistor gain drops by 3dB or  $1/\sqrt{2}$  times from its value at low frequency in figure 4.6.5. It is given as

$$f_H = \frac{1}{2\pi r_{b'e} C_{eq}}$$

$$= \frac{1}{2\pi r_{b'e} [C_e + C_c (1 + g_m R_L)]}$$

At  $R_L = 0$

$$f_H = \frac{1}{2\pi r_{b'e} [C_e + C_c]} = f_\beta$$

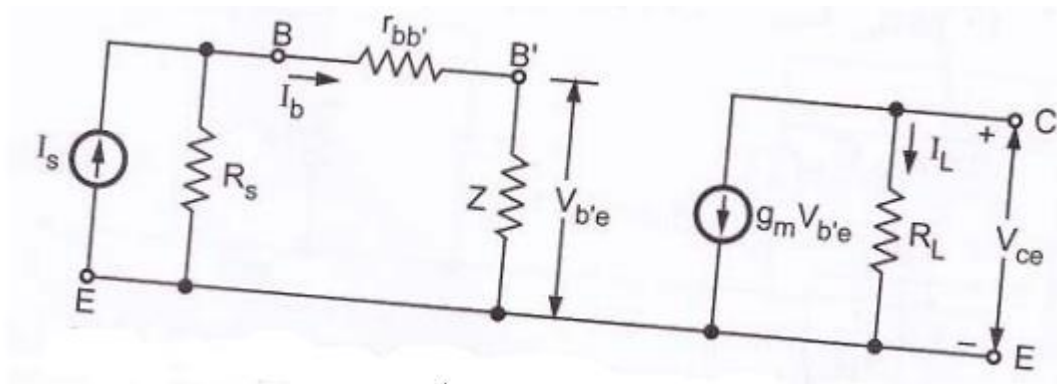


**Figure 4.6.5. Variation  $f_H$  with  $R_L$**

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**Current gain including source resistance:**

Figure 4.6.6. shows hybrid pi Equivalent circuit with current source



**Figure 4.6.6. Equivalent circuit with current source**

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$$\frac{I_L}{I_s} = \frac{-g_m r_{b'e} R_s}{R_s + r_{bb'} + r_{b'e}}$$

$$A_{is} \text{ at low frequency} = \frac{-h_{fe} R_s}{R_s + h_{ie}}$$

**Voltage gain including source resistance:**

$$A_{vs} = \frac{V_o}{V_s} = \frac{I_L}{I_s} \frac{R_L}{R_s} = \frac{-g_m Z R_s}{R_s + r_{bb'} + Z} \times \frac{R_L}{R_s}$$

$$= \frac{-g_m Z R_L}{R_s + r_{bb'} + Z}$$

$$A_{vs \text{ low}} = \frac{I_L}{I_s} \frac{R_L}{R_s} = \frac{-h_{fe} R_s}{R_s + h_{ie}} \times \frac{R_L}{R_s}$$

$$= \frac{-h_{fe} R_L}{R_s + h_{ie}}$$

Cutoff frequency including source resistance:

$$A_{is \text{ high}} = \frac{A_{is}}{1 + j \left( \frac{f}{f_H} \right)}$$

$$A_{vs \text{ high}} = \frac{A_{vs}}{1 + j \left( \frac{f}{f_H} \right)}$$

where,  $f_H = \frac{1}{2\pi R_{eq} C_{eq}}$

where,  $R_{eq} = r_{b'e} \parallel (r_{bb'} + R_s)$

and  $C_{eq} = C_e + C_c [1 + g_m R_L]$

For  $R_L = 0$ ,

$$f_H = \frac{1}{2\pi R(C_e + C_c)}$$

$$= \frac{f_T}{g_m R} \quad \because f_T = \frac{g_m}{2\pi(C_e + C_c)}$$

$$= \frac{h_{fe} f_\beta}{g_m R} \quad \because f_T = h_{fe} f_\beta$$

$$= \frac{f_\beta}{g_{b'e} R} \quad \because g_{b'e} = \frac{g_m}{h_{fe}}$$



## Gain Bandwidth Product:

### i. Gain Bandwidth Product for Voltage:

$$\begin{aligned} |A_{vs \text{ low } f_H}| &= |A_{vso} f_H| = \frac{-h_{fe} R_L}{R_s + h_{ie}} \times \frac{1}{2\pi R_{eq} C_{eq}} \\ &= \frac{R_L}{R_s + r_{bb'}} * \frac{f_T}{1 + 2\pi f_T C_C R_L} \end{aligned}$$

### ii. Gain Bandwidth Product for current:

$$\begin{aligned} |A_{iso} \times f_H| &= \frac{g_m R_s}{2\pi C(R_s + r_{bb'})} \\ &= \frac{f_T}{1 + 2\pi f_T C_c R_L} \cdot \frac{R_s}{R_s + r_{bb'}} \end{aligned}$$

