

Problem on Rigid type flange Coupling:

Design a C.I protective flange Coupling to connect two shafts in order to transmit 7.5 kw at 720 rpm. The following permissible stresses may be used.

permissible shear stress for shaft, bolt & key = 33 Mpa.

permissible crushing stress for bolt & key = 60 Mpa.

permissible shear stress for C.I Coupling = 15 Mpa.

Given:

Power $P = 7.5 \text{ kW}$.

Speed $N = 720 \text{ rpm}$.

permissible shear for shaft, bolt & key = 33 Mpa.

" crushing for bolt & key = 60 Mpa

" shear for C.I Coupling = 15 Mpa.

Design for Hub:

We know,

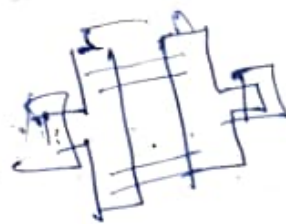
$$P = \frac{2\pi NT}{60}$$

$$\text{Torque } T = \frac{7.5 \times 10^3 \times 60}{2 \times \pi \times 720}$$

$$T = 99.47 \times 10^3 \text{ N}\cdot\text{mm}$$

To find ϕ of shaft:

$$T = \frac{\pi}{16} \times \tau_s \times d^3$$



$$d^3 = \frac{99.47 \times 10^3 \times 16}{33\pi}$$

$$d = 24.5 \text{ mm} \approx \boxed{d = 25 \text{ mm}}$$

Design of mof

∴ Inner ϕ of hub $d = 25 \text{ mm}$.

Outer ϕ of hub $D = 2d = 50 \text{ mm}$.

Length of hub $L = 1.5d = 37.5 \text{ mm}$.

checking for shear stress in Hub:

$$T = \frac{\pi}{16} \times \tau_c \times \left[\frac{D^4 - d^4}{D} \right]$$

$$99.47 \times 10^3 = \frac{\pi}{16} \times \tau_c \times \left[\frac{50^4 - 25^4}{50} \right]$$

$$\boxed{\tau_c = 4.32 \text{ Mpa}} < 15 \text{ Mpa given, Safe!}$$

Design of key:

For $\phi 25 \text{ mm}$ shaft, Take $w = 10$ & $t = 8$.

Length of key $= 1.5d = \text{Length of hub} = 37.5 \text{ mm}$.

checking for shear in key:

$$T = l \times w \times \tau_k \times d/2$$

$$99.47 \times 10^3 = 37.5 \times 10 \times \tau_k \times \frac{25}{2}$$

$$\tau_k = 21.22 \text{ Mpa} < 33 \text{ Mpa given, the design is safe}$$

Checking for Crushing Stress:

$$T = l \times \frac{b}{2} \times \sigma_{ck} \times \frac{d}{2}$$

$$99.47 \times 10^3 = 37.5 \times \frac{8}{2} \times \sigma_{ck} \times \frac{25}{2}$$

$$\sigma_{ck} = 53.05 \text{ Mpa} < 60 \text{ Mpa given, the design is safe}$$

Design of flange:

Thickness of flange = $0.5d = 0.5 \times 25 = 12.5 \text{ mm}$.
Outer ϕ of flange $D_2 = 4d = 4 \times 25 = 100 \text{ mm}$.

check for shear stress in flange:

$$T = \frac{\pi D^2}{4} \times t_f \times \tau_c \times \frac{D}{2}$$

$$99.47 \times 10^3 = \frac{\pi \times 50^2}{4} \times 12.5 \times \tau_c$$

$$\tau_c = 2.02 < 15 \text{ mpa given } \& \text{ design is safe.}$$

Design for bolt:

For $\phi 25$ mm shaft, (P.S.G 7.107).
No of bolt = 4.

Pitch \odot ϕ of bolt = $3d = 3 \times 25 = 75$ mm.

To find the size of bolt:

$$T = \frac{\pi}{4} (d_1)^2 \times \tau_b \times n \times \frac{D_1}{2}$$

$$99.47 \times 10^3 = \frac{\pi}{4} \times (d_1)^2 \times 33 \times 4 \times \frac{75}{2}$$

$$d_1^2 = 25.5 \text{ mm}$$

$$d_1 = 5.05 \text{ mm} \quad \approx \quad d_1 = 6 \text{ mm}$$

\therefore The size of bolt is M6 is selected.

2. Design a shaft and flange for a Diesel Engine in which protected type of flange coupling is to be adopted for power transmission. The following data is available for design
 power of engine = 75 kW, speed of engine = 200 rpm,
 $\tau_{max} = 40 \text{ MPa}$. Max. permissible twist in shaft = 1° in length of shaft equal to 30 times the diameter of shaft.
 $T_{max} = 1.25 T_{mean}$. pitch ϕ of bolts = $3d$. Max. stress in bolt = 20 MPa .

Find: i) Diameter of shaft, ii) Number of bolts, iii) Dia of bolt.

Given:

Power (P) = 75 kW.
 Speed (N) = 200 rpm.
 Shear stress for shaft (τ_s) = 40 MPa.
 Angle of Twist $\theta = 1^\circ = \frac{\pi}{180} = 0.0175 \text{ rad}$.
 Length $l = 30d$.
 $T_{max} = 1.25 T_{mean}$.
 pitch ϕ of bolt $D_1 = 3d$.
 Shear stress in bolt (τ_b) = 20 MPa.

Design of Hub:

We know, $P = \frac{2\pi NT}{60}$

$$T = \frac{P \times 60}{2\pi N} = \frac{75 \times 10^3 \times 60}{2 \times \pi \times 200}$$

$T_{mean} = 3580.9 \text{ N.m}$

$T_{max} = 4476.23 \text{ N.m}$

Design of flange:

Thickness of flange $t_f = 0.5d = 50\text{mm}$.
Protective circumferential flange $t_p = 0.25d = 25\text{mm}$.

Design of bolt:

For $\phi 100\text{mm}$ shaft.

No of bolts = 6.

Given pitch circle ϕ of bolt $D_1 = 3d = 300\text{mm}$.

To find the ϕ of bolt:

$$T = \frac{\pi}{4} (d_b)^2 \times C_b \times n \times D/2.$$

$$4476.23 \times 10^3 = \frac{\pi}{4} (d_b)^2 \times 20 \times 6 \times \frac{300}{2}.$$

$$d_b^2 = 316.62.$$

$$d_b = \cancel{18} 17.79\text{mm} \quad \text{Say } \boxed{d_b = M18 \text{ mm}}$$

\therefore M18 bolt is selected.

To find Diameter of shaft

$$T = \frac{\pi}{16} \times C \times d^3 \rightarrow (NA).$$

$$\frac{T}{J} = \frac{C \times \theta}{l}$$

Assume $84 \text{ kN/mm}^2 = C$.

$$\frac{4476 \cdot 23 \times 10^3}{\frac{\pi}{32} \times d^4} = \frac{10^3 \times 84 \times 0.0175}{30d}$$

$$d = 97.6 \text{ mm} \quad \boxed{\approx 100 \text{ mm} = d}$$

Inner ϕ of Hub = ϕ of shaft $\therefore d = 100 \text{ mm}$.

Outer ϕ of Hub = $D = 2d = 200 \text{ mm}$.

Length of Hub = $L = 1.5d = 150 \text{ mm}$.

Design of key:

For $\phi 100 \text{ mm}$ shaft, $W = 28 \text{ mm}$

$t = 16 \text{ mm}$.

Length of key = Length of Hub = 150 mm .